A simulation of an X-ray binary system. A bright yellow-white star is on the right, with a large, glowing orange and yellow accretion disk extending from it. A blue, turbulent wind or coronal outflow extends upwards from the center of the disk. The background is black with some faint stars.

Radiation Hydrodynamic
Simulations of Coronae &
Disk Winds in X-ray
Binaries

Nick Higginbottom

Daniel Proga

Christian Knigge

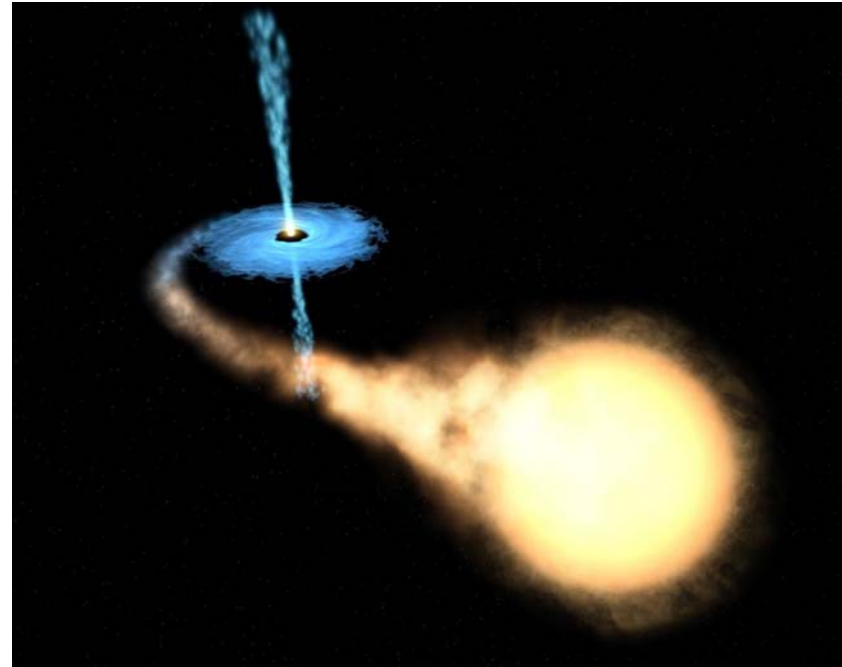
Knox Long

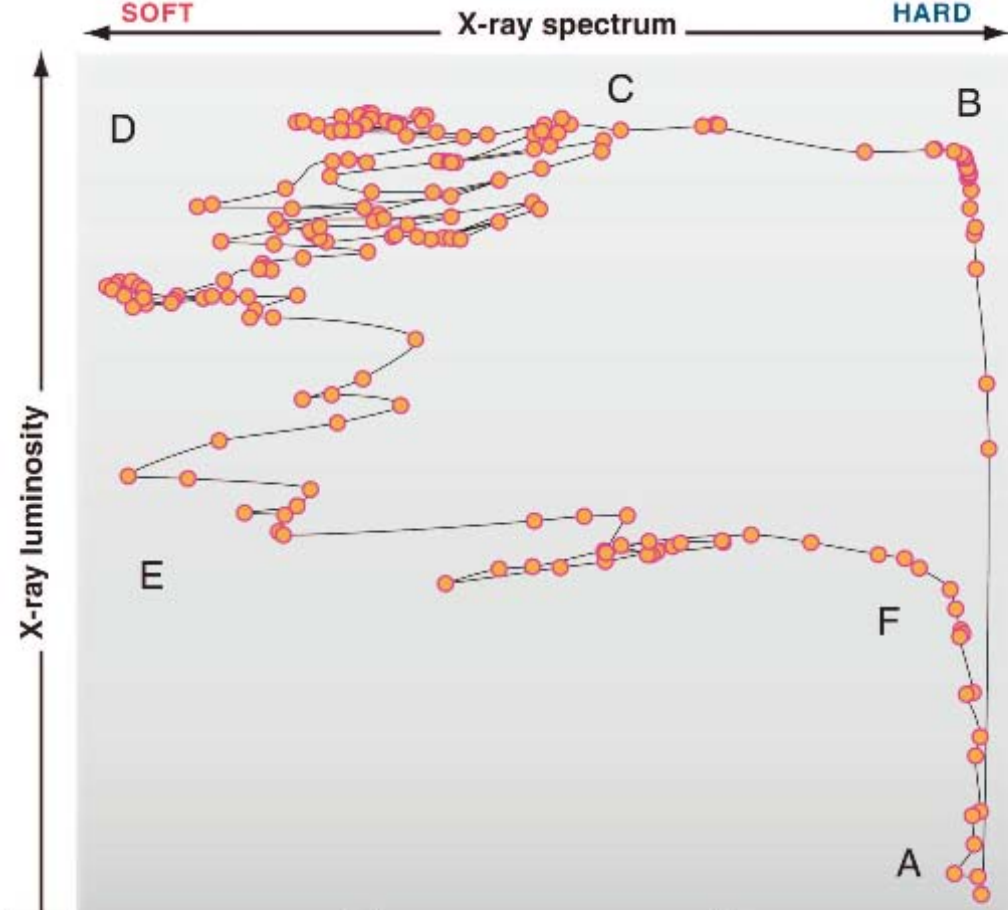
Overview

- Low Mass X-ray Binaries
 - LMXB Absorbers/Outflows
 - Possible outflow driving mechanisms
- Hydrodynamic simulations of thermally driven outflows
 - Significant mass loss rates
 - Velocities approaching those seen in observations

X-Ray binaries

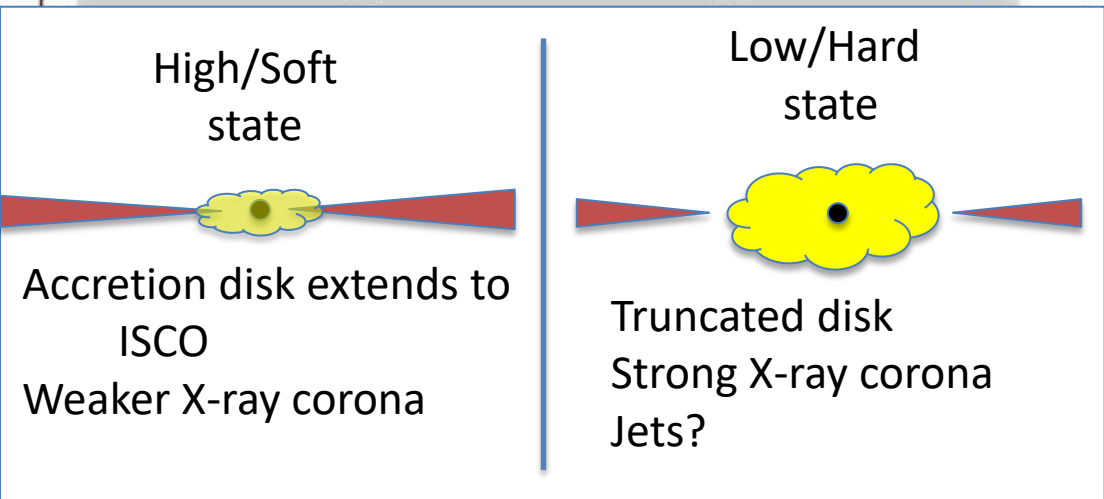
- A neutron star or black hole in orbit with a secondary
 - O/B star = High mass X-ray binary (HMXB)
 - Smaller star = Low mass X-ray binary (LMXB)
- We concentrate on LMXB
 - secondary has filled its Roche lobe, and is fuelling an accretion disk around the compact object





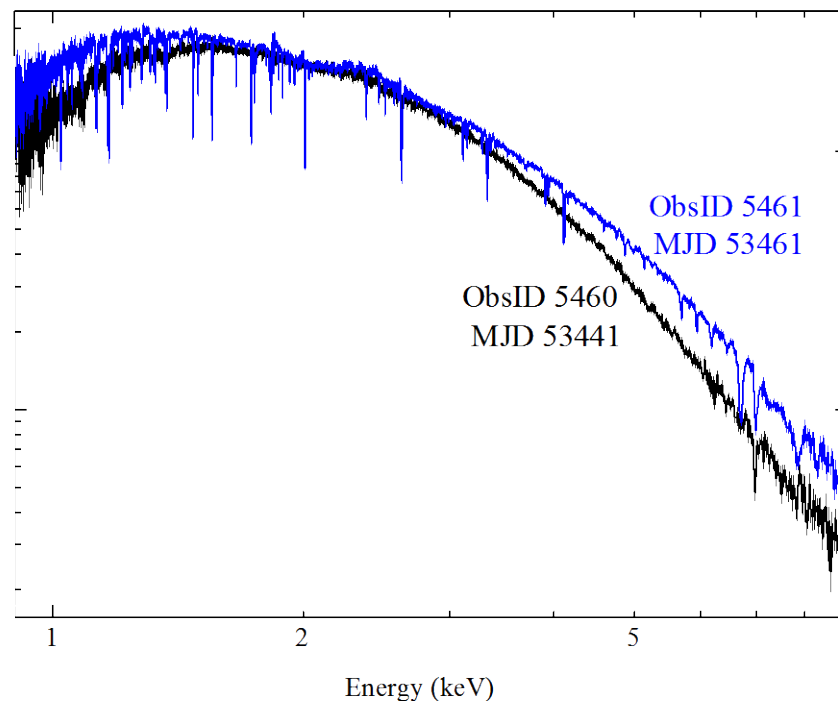
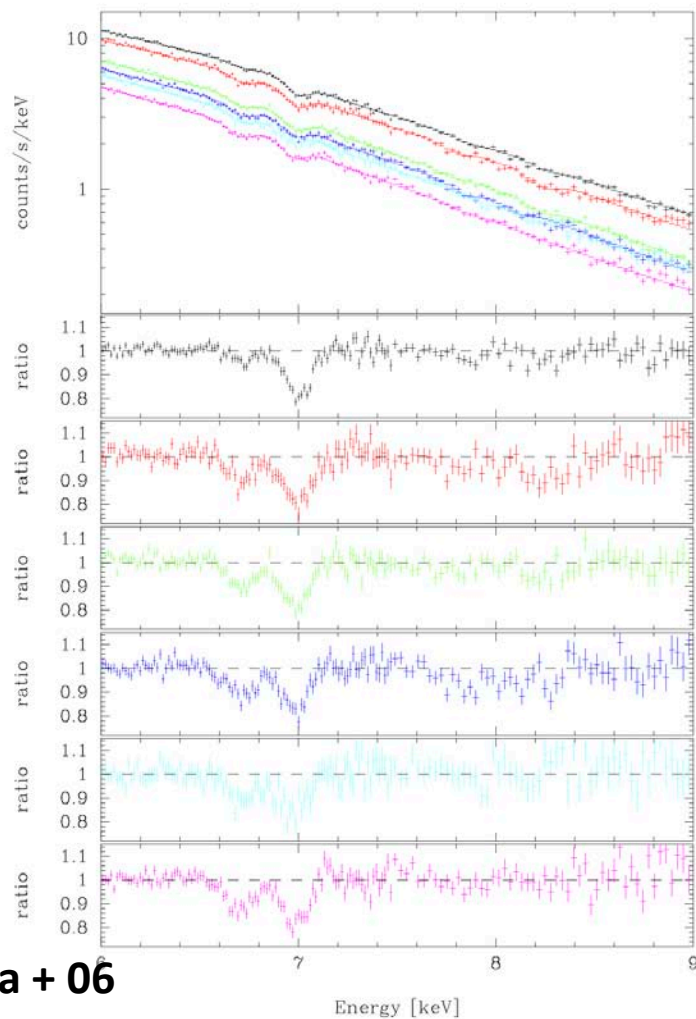
LMXB states

- Low/Hard state (A-B) truncated inner disk + hot `corona`.
- B-D – jet shuts off, spectrum softens
- D-E – high/soft state – spectrum dominated by accretion disk
- E-F– disk recedes? Jet can reappear.



X-ray binary spectra – evidence of an absorber

- 4U 1630-472



- GRO J1655-40
- Black = high state
- Blue = low state

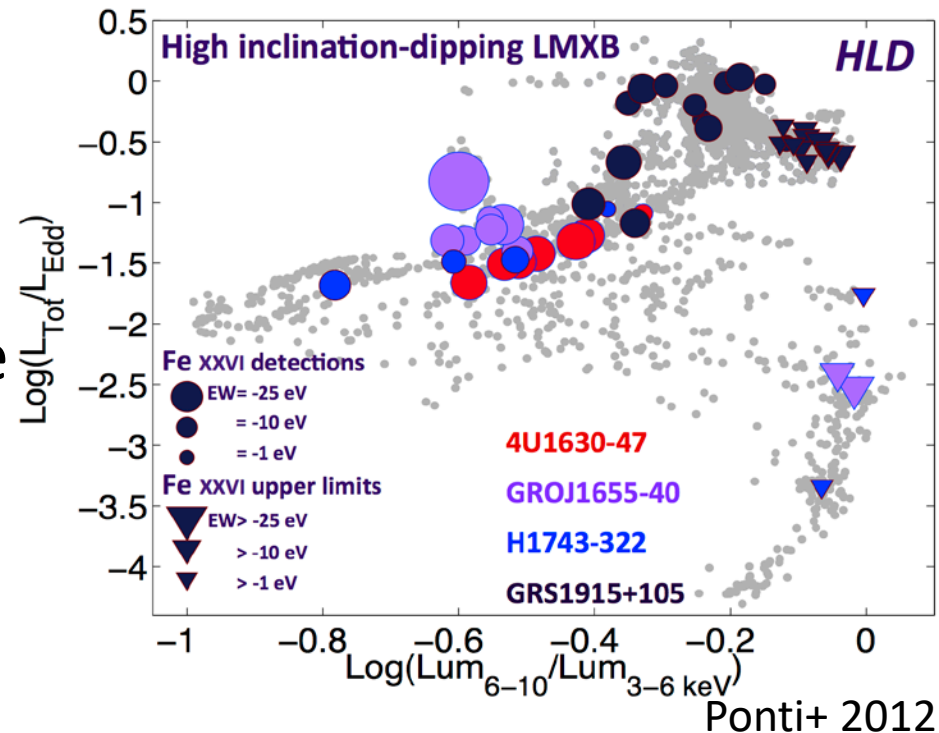
LMXB absorbers

- Mainly seen in X-ray lines of He and H like Iron
 - Highly ionized ($\xi > 10^3$)
 - $N_H \approx 10^{21} - 10^{24} \text{ cm}^{-2}$
- Ubiquitous in high inclination systems
- 8 systems show blue shifts of 400-3000 km/s
- Preferentially seen in systems with large P_{orb}
- Never seen at the same time as jets
- Seen exclusively in the high/soft state

$$\xi = \frac{L_X}{n_H r^2}$$

Motivation to study XRB disk winds

- Mass transfer - $\dot{M}_{wind} > \dot{M}_{acc}$?
- Angular momentum transfer
 - If winds are connected to the disk via magnetic field lines
- State change
- Veiling
 - If winds exist, we view the system through them



Driving mechanisms for XRB disk winds

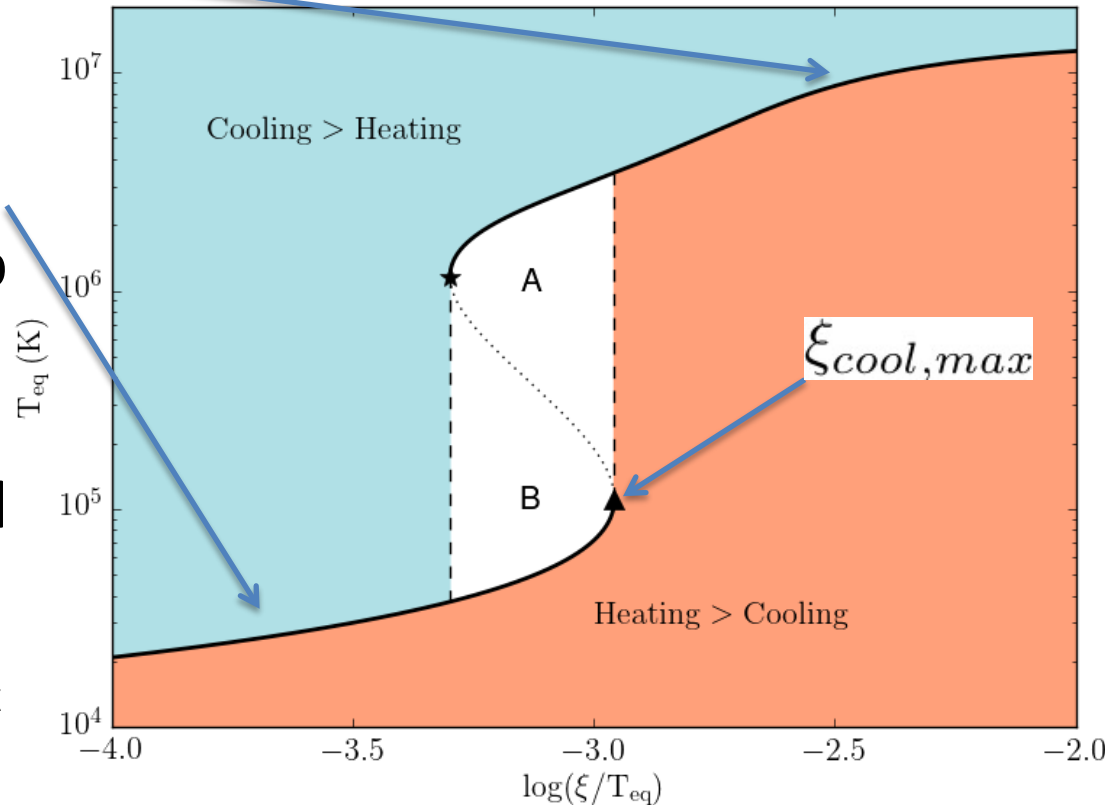
- Magnetic
 - B fields required for MRI, can also drive a wind
- Radiation
 - pressure on lines and electrons
 - Unlikely for XRBs due to high ionization state
- Thermal –
 - Thermal velocity at the surface of the disk exceeds local escape velocity
 - Radius at which gas at Compton temperature can escape given by

$$R_{IC} = \frac{GM_{BH}\mu m_H}{k_B T_{IC}}$$

- This is rather large – $10^5 R_G$

Thermal wind launching mechanism

- Upper branch, gas is at Compton temperature and can escape.
- Lower branch, PI heating balanced by Line+Recomb cooling
- At $\xi_{\text{cool,max}}$ gas heats rapidly – gains energy and accelerates
- Precise location of $\xi_{\text{cool,max}}$ and shape of curve defines energy increase and resulting flow
- Atomic physics!



$$\xi = \frac{L_X}{n_H r^2}$$

Simulating thermal disk winds

- We use ZEUS to solve the equations of hydrodynamics

Mass $\frac{D\rho}{Dt} + \rho \nabla \cdot v = 0$

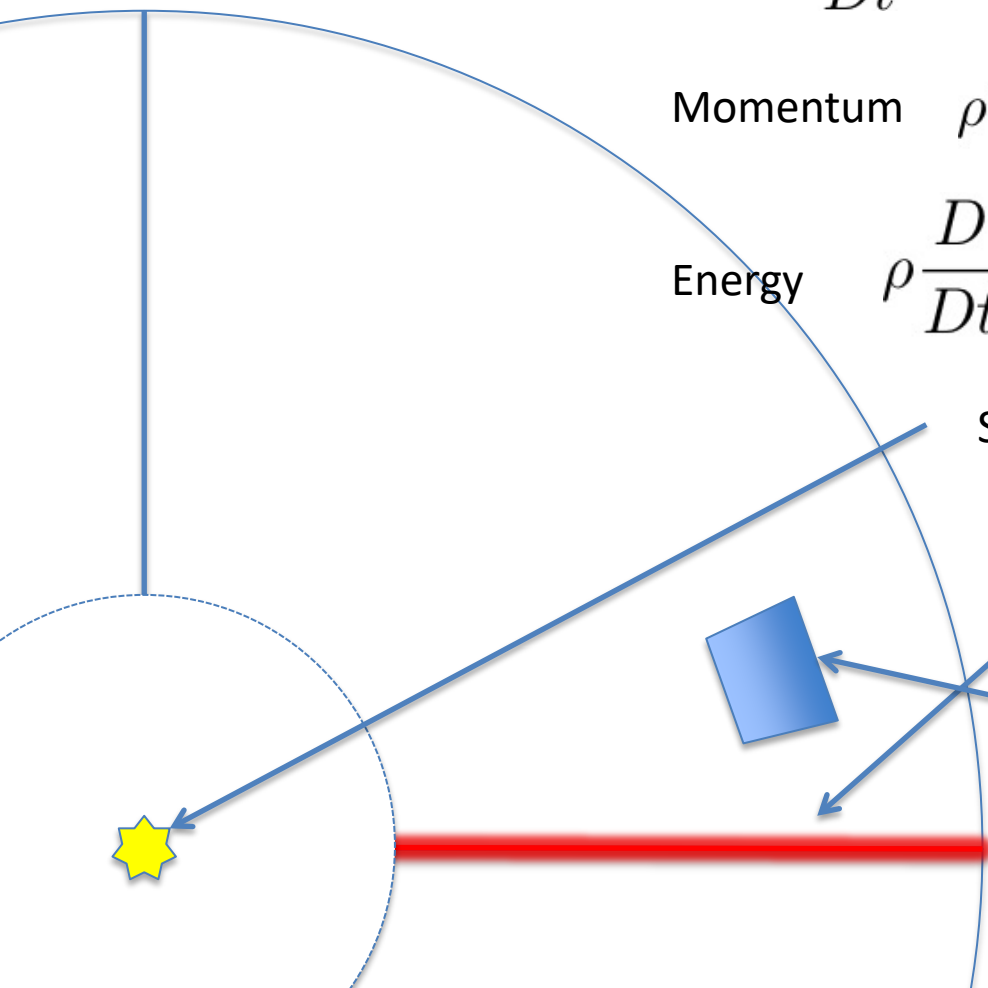
Momentum $\rho \frac{Dv}{Dt} = -\nabla P + \rho g$

Energy $\rho \frac{D}{Dt} \left(\frac{e}{\rho} \right) = -P \nabla \cdot v + \rho \mathcal{L}(\xi, T)$

Source of ionizing radiation $L_x = 3.3 \times 10^{37} \text{ erg s}^{-1}$

Fixed density boundary $\rho(r) = \rho_0 \left(\frac{r}{R_{IC}} \right)^{-2}$

For a given cell, we calculate the radiative heating/cooling rate from ionization parameter and temperature



Analytic heating and cooling rates

Initial investigations used analytic expressions for heating and cooling rates from Blondin (1994)

$$\rho\mathcal{L} = n^2(G_{Compton} + G_X - L_l - L_b)$$

Compton heating /cooling

$$G_{Compton} = 8.9 \times 10^{-36} \xi (T_X - 4T)$$

X-ray (photoionization) heating

$$G_X = 1.5 \times 10^{-21} \xi^{1/4} T^{-1/2} (1 - T/T_X)$$

Bremstrahlung cooling

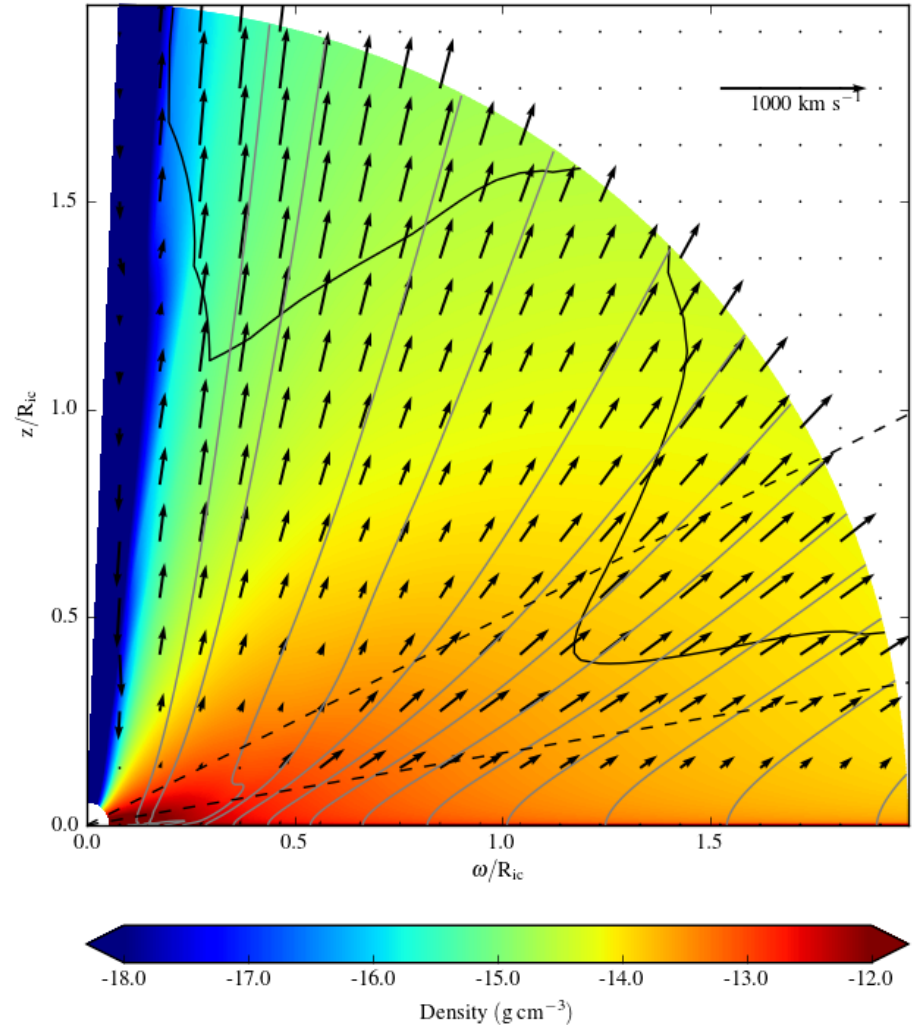
$$L_b = 3.3 \times 10^{-27} T^{1/2}$$

Line (bound-bound and free-bound) cooling

$$L_l = \left[1.7 \times 10^{-18} \exp(-T_L/T) \xi^{-1} T^{-1/2} + 10^{-24} \right] \delta$$

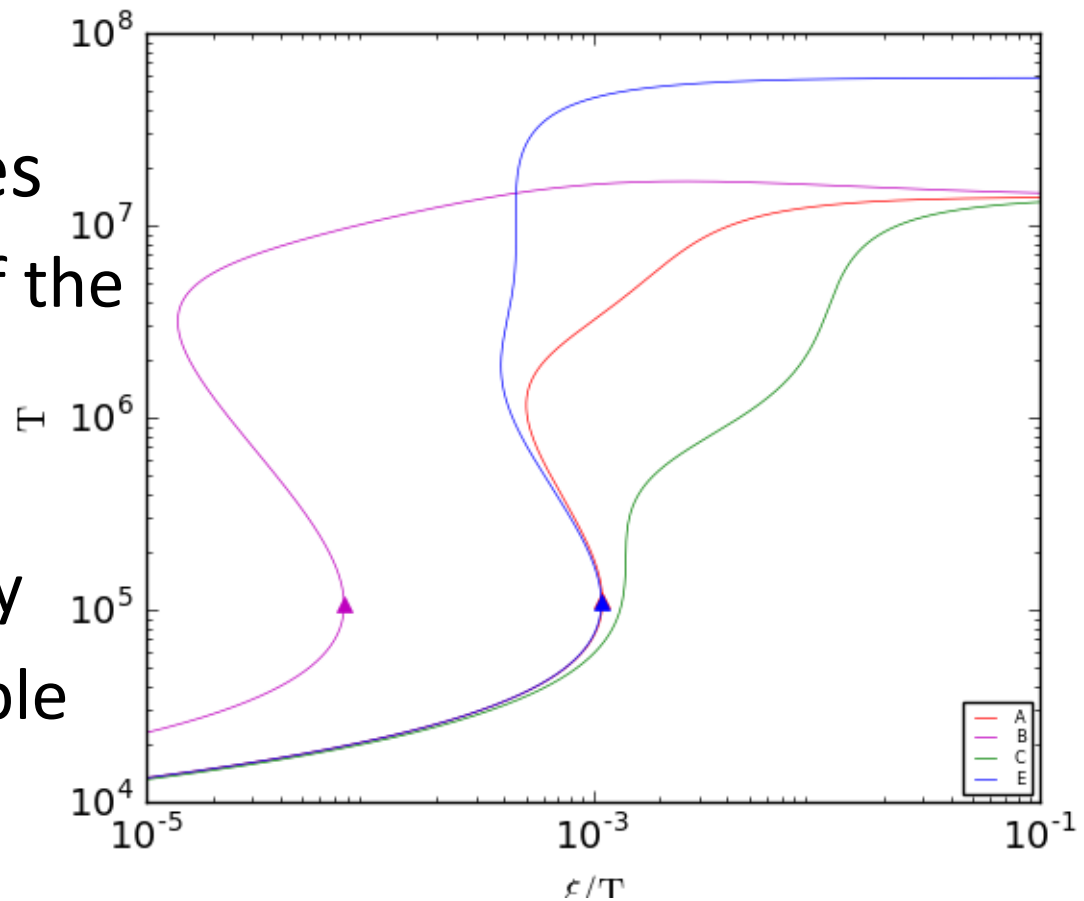
Thermal outflow 1

- High density ($n_{\text{H}} > 10^{12}$) gas is slow moving ($< 100 \text{ km s}^{-1}$)
- Failed in the stated aim to model GRO1655-50
- However - wind outflow rate approx. 7x accretion rate
- GRO1655-40 is perhaps an extreme source....



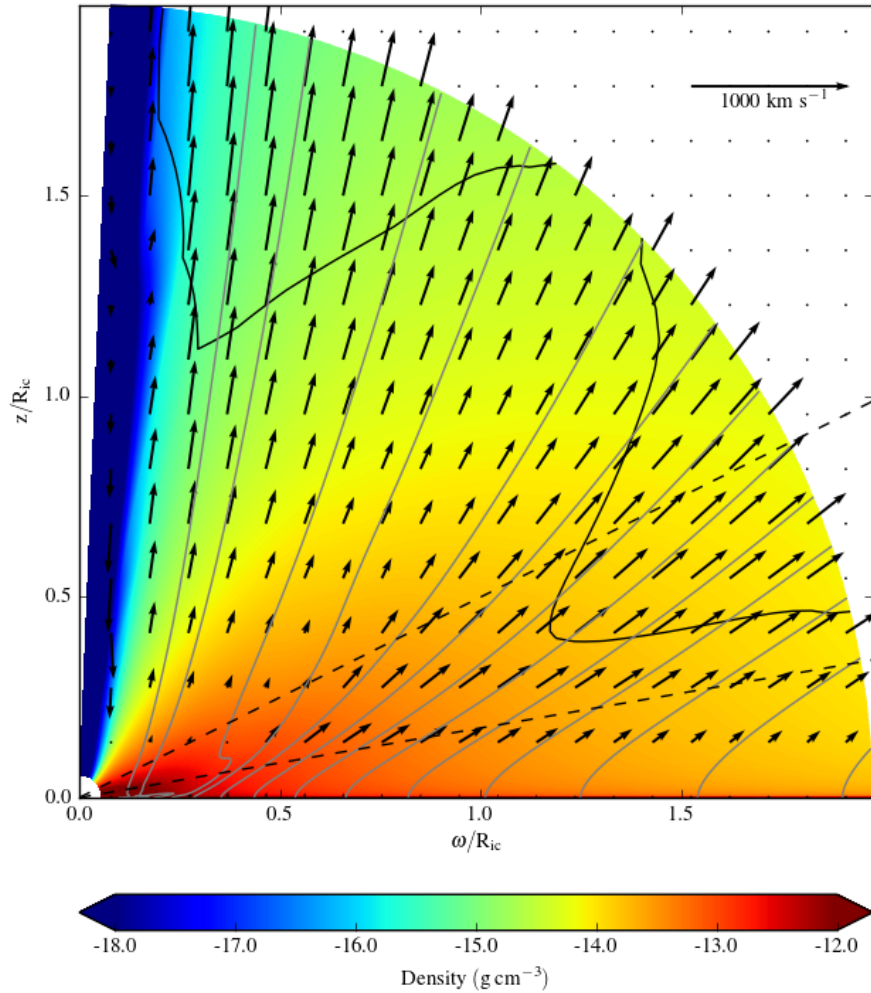
Investigating the effect of modifying the heating and cooling rates

- Physically motivated changes to heating/cooling rates
 - Changes the form of the stability curve
 - B: Change $\xi_{\text{cool,max}}$
 - C: Remove instability
 - E: Extend the unstable zone

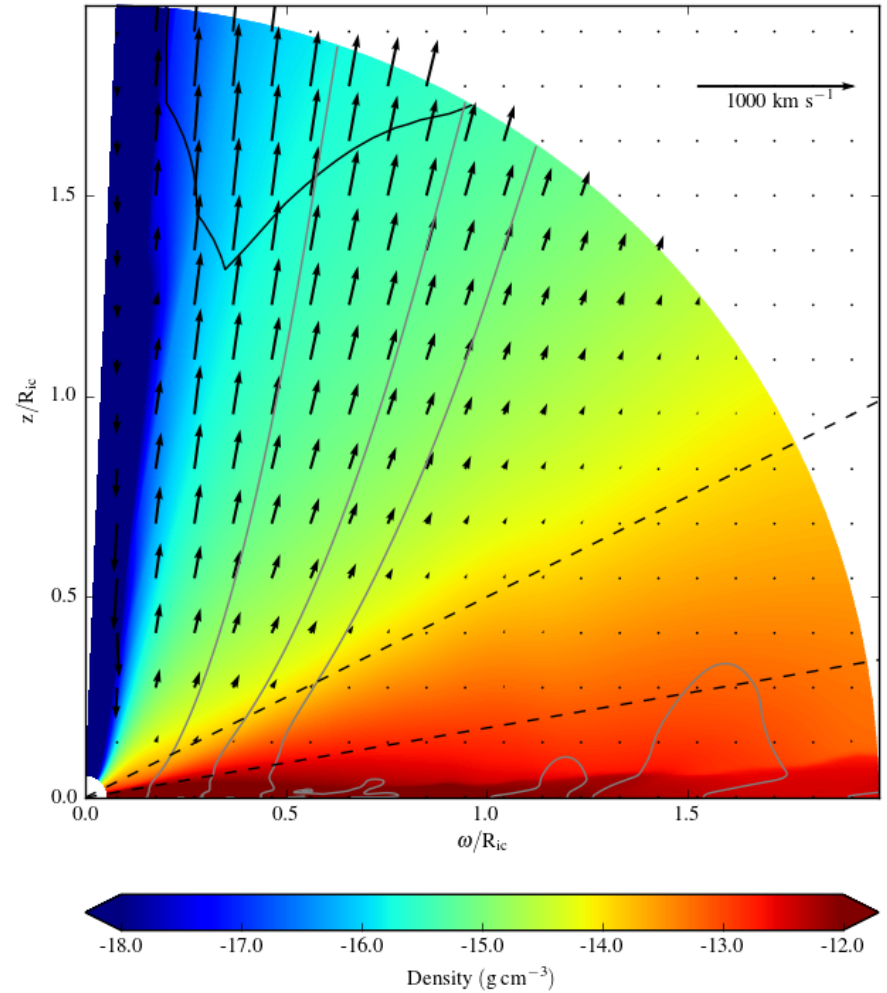


Results 1: No instability = no outflow

Standard analytic H/C rates

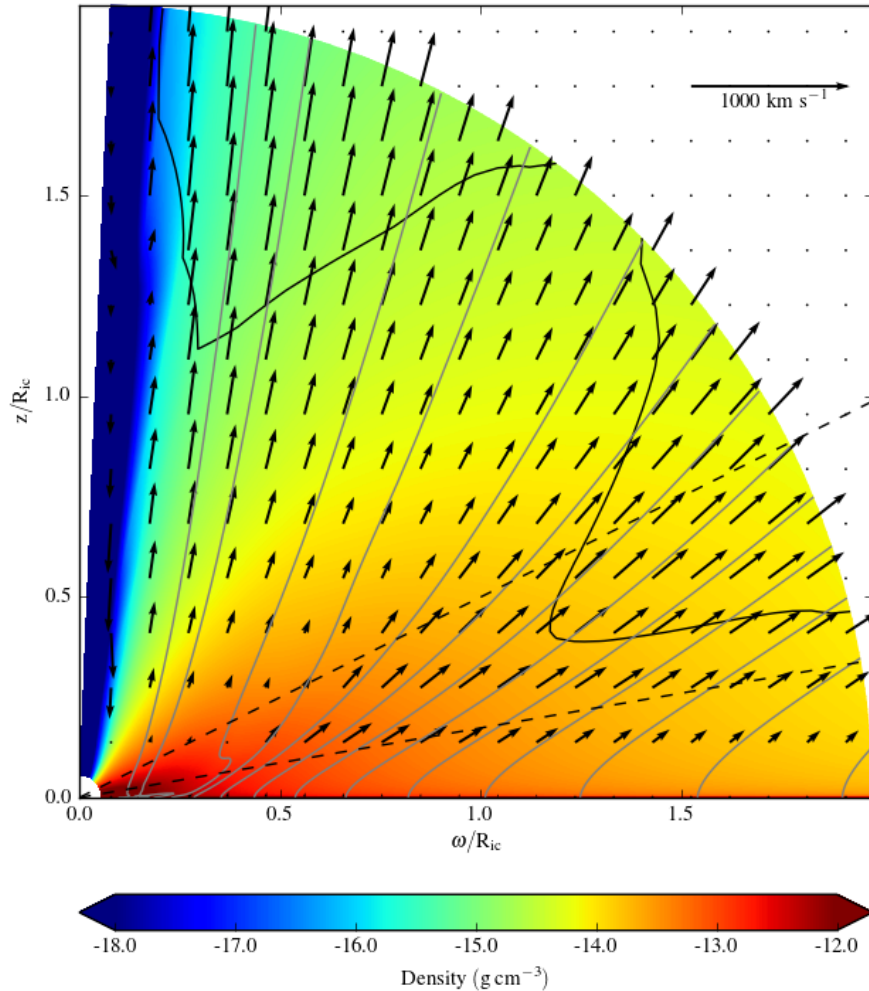


Weak heating (stable)

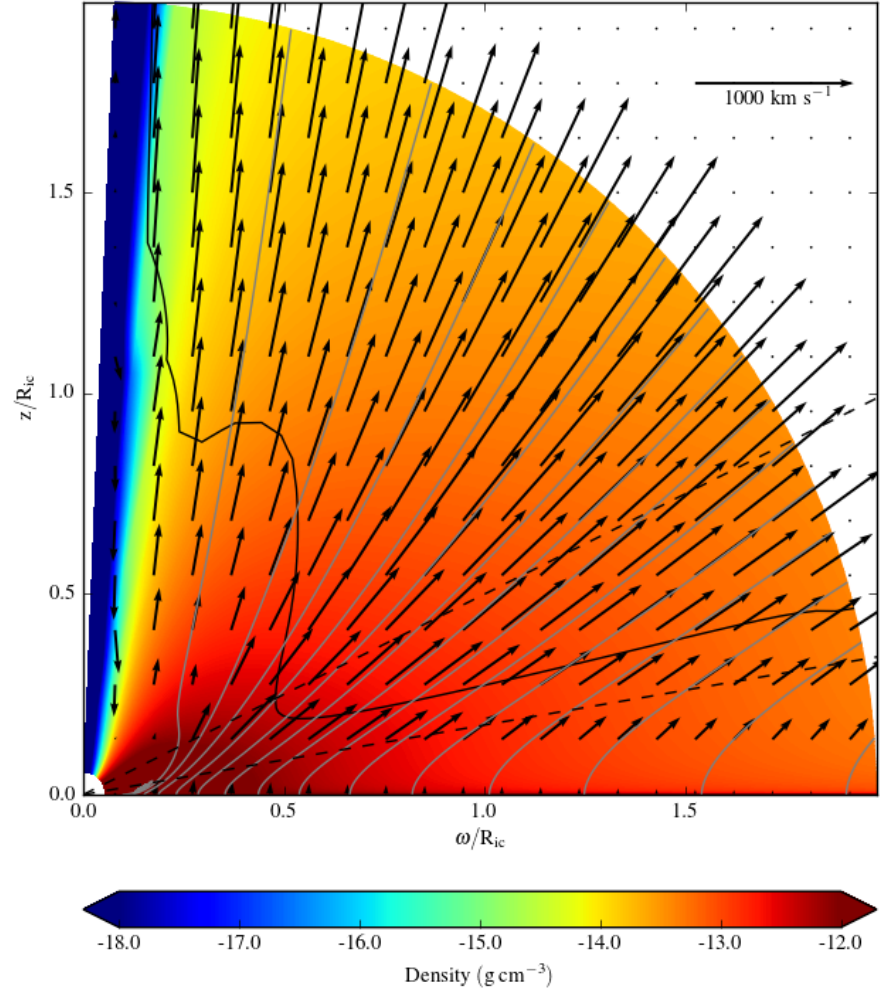


Results 2: Denser base = denser flow

Standard analytic H/C rates



Strong heating (unstable/catastrophic)



Mass loss rate = 40 x accretion rate
Much denser, and somewhat faster

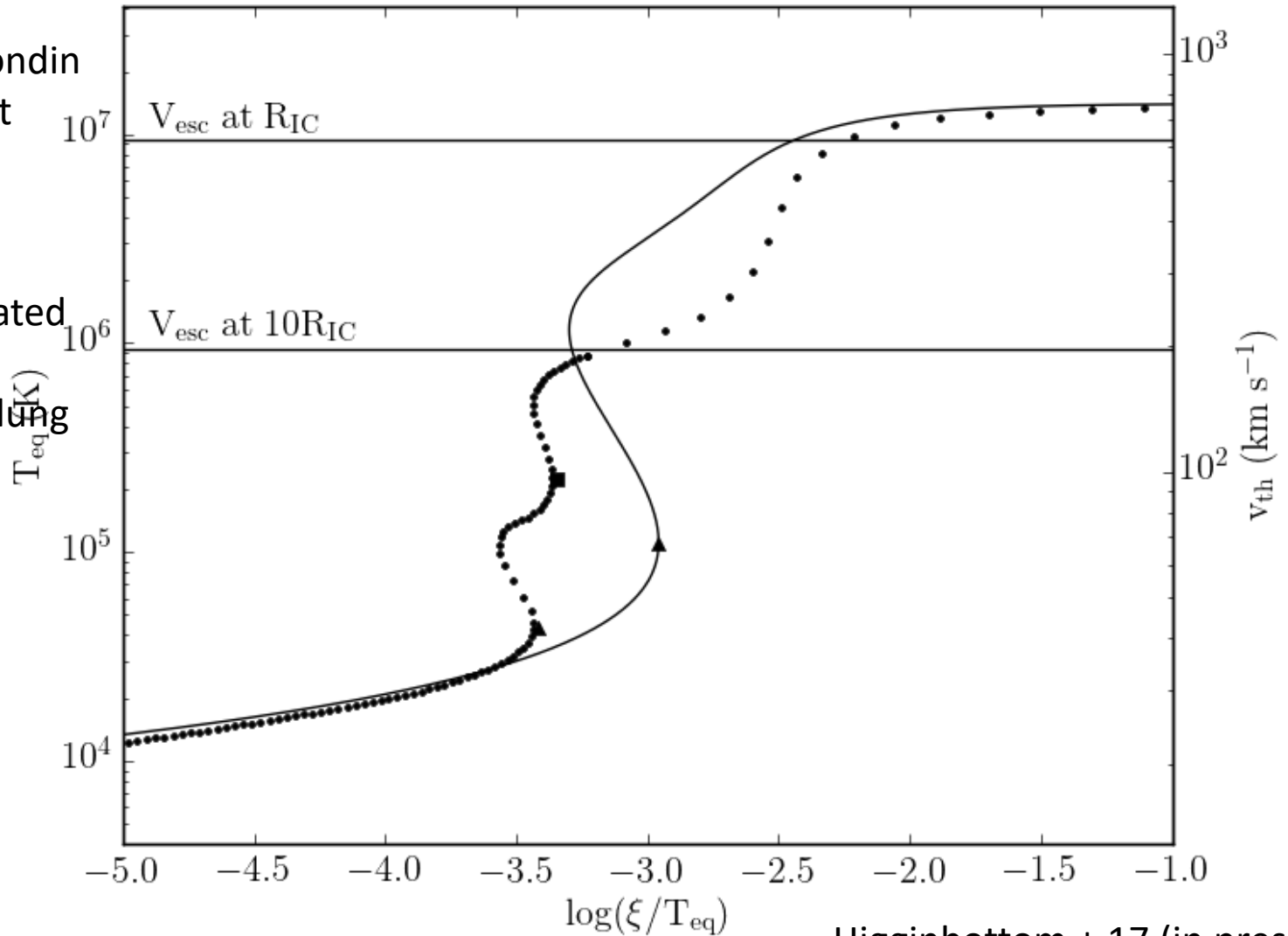
Next step

- We demonstrated that the heating and cooling rates have major effect on the outflow
- We want to test the plausibility of our modified heating and cooling rates
- Use photoionization code to compute them
 - net heating/ net cooling(ξ, T) lookup tables calculated in Cloudy (see Daniel's talk next)
 - Modify Zeus to use these tables
 - Initially still using optically thin assumption

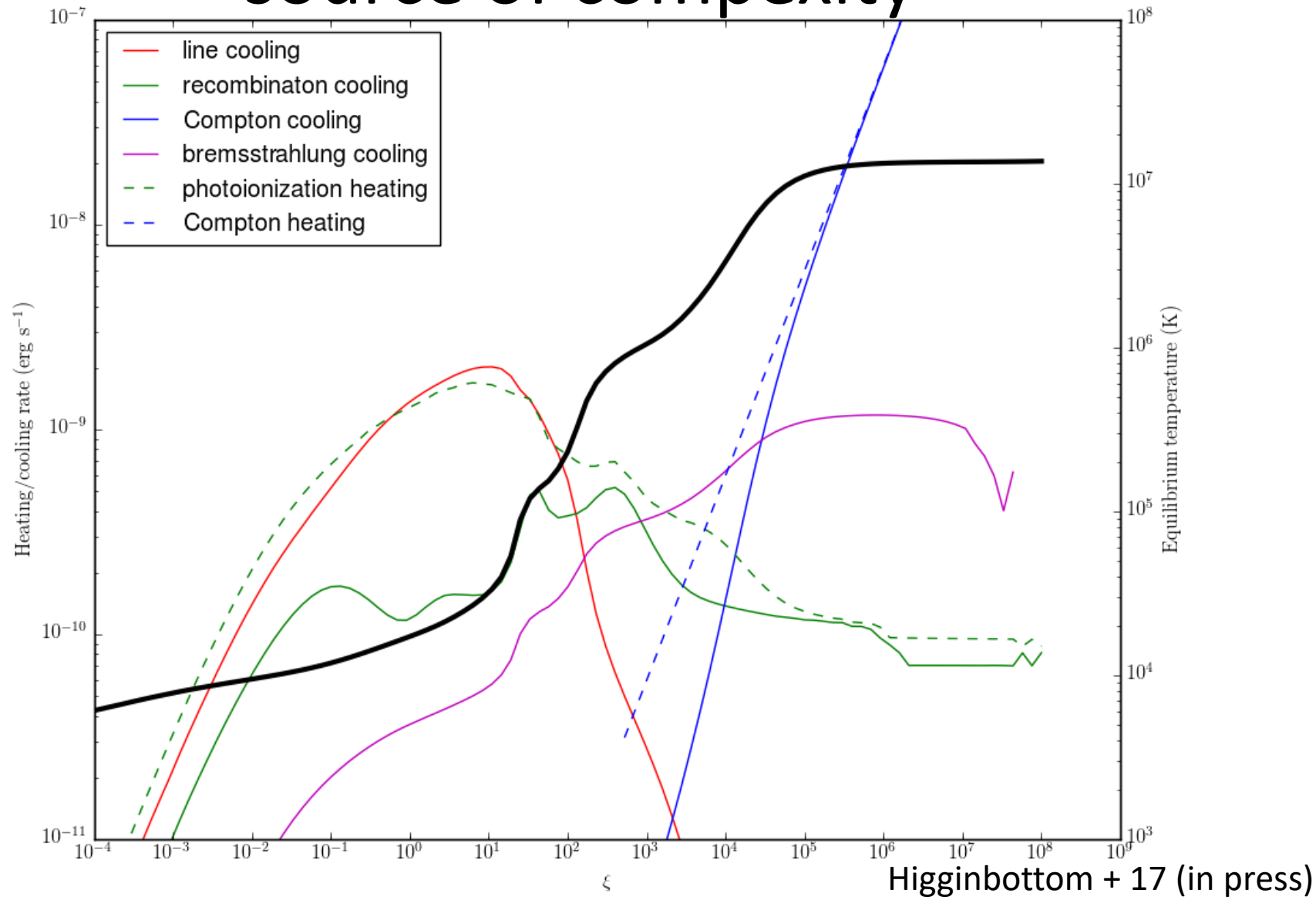
Stability curve computed in cloudy

Solid line from Blondin (1994) – different atomic data, analytical fit

Dotted line calculated from Cloudy 50keV Bremsstrahlung SED.

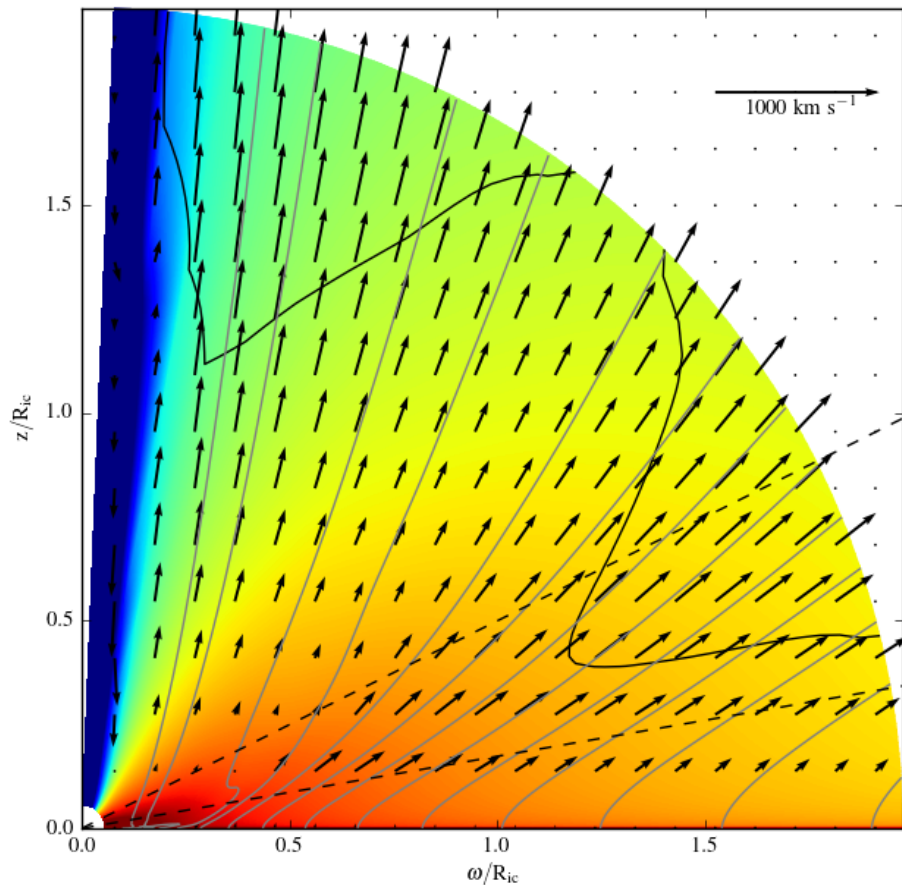


Heating and cooling mechanisms – the source of complexity



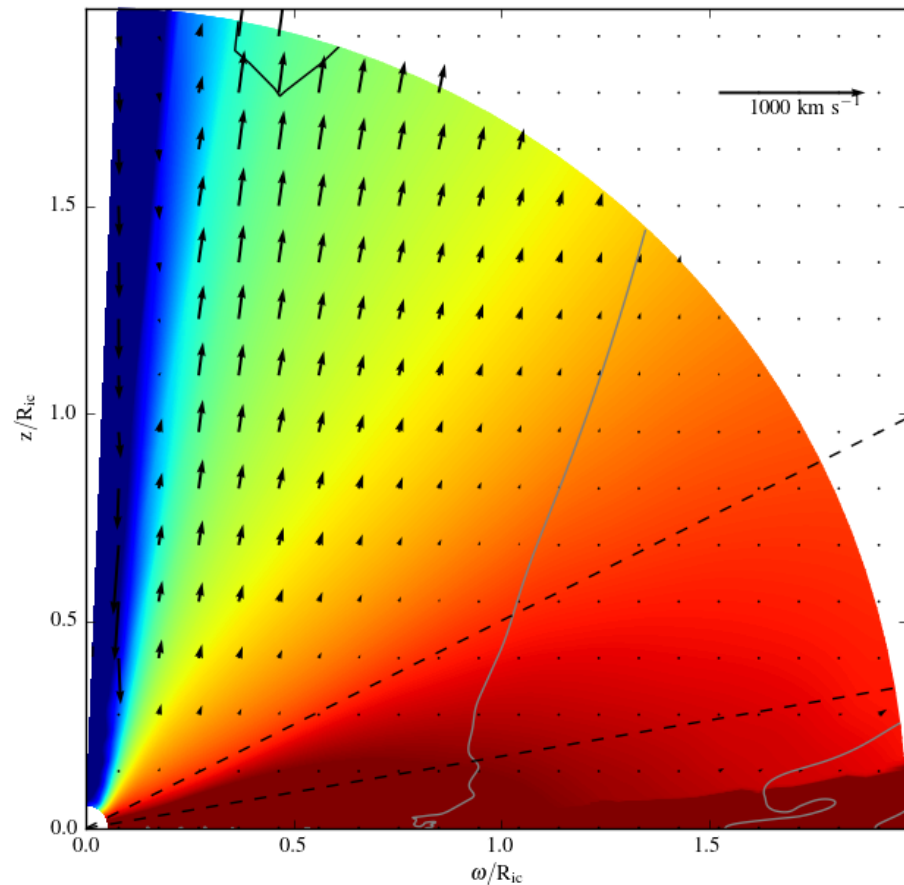
Outflow with accurate heating and cooling rates

Analytic fits to H/C rates



Density (g cm^{-3})

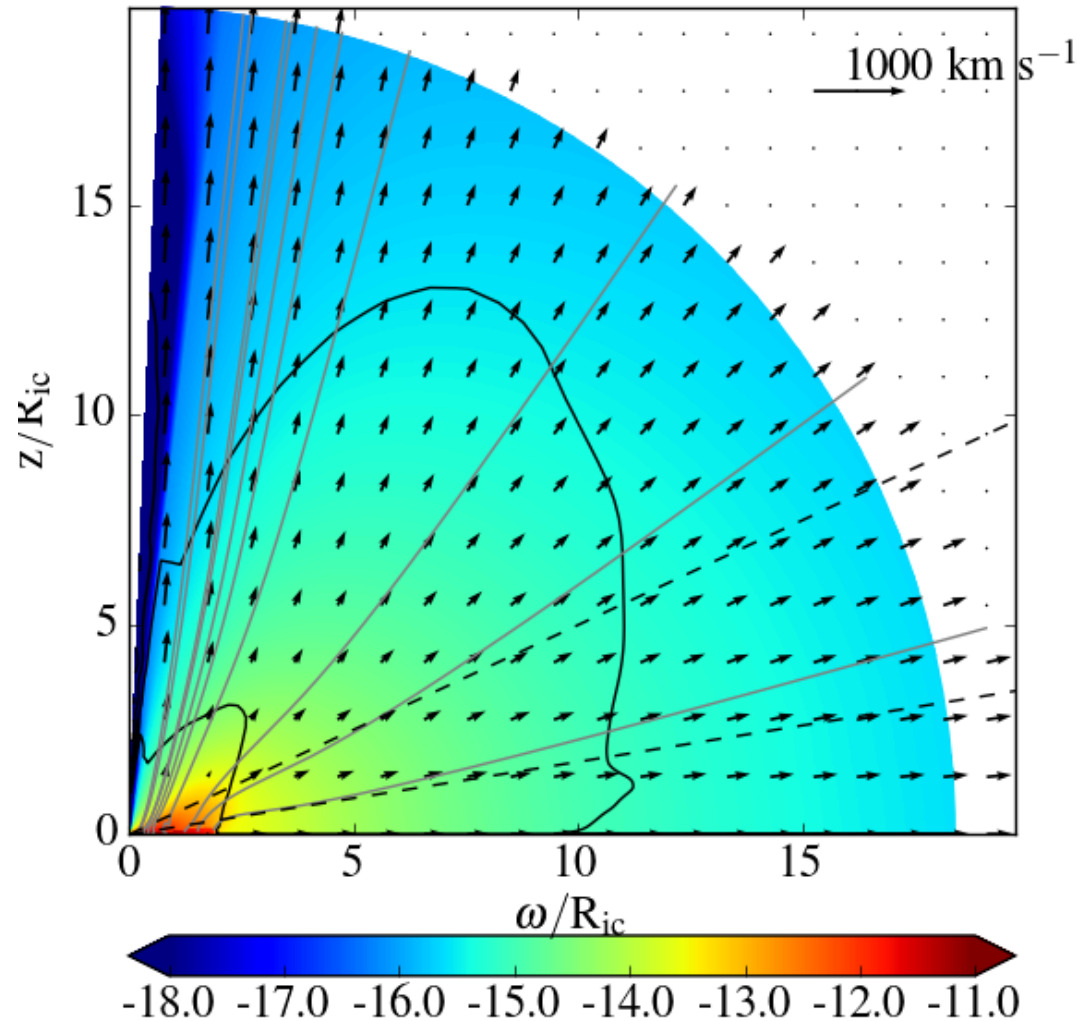
Detailed lookup H/C rates



Density (g cm^{-3})

Chasing the Mach 1 surface

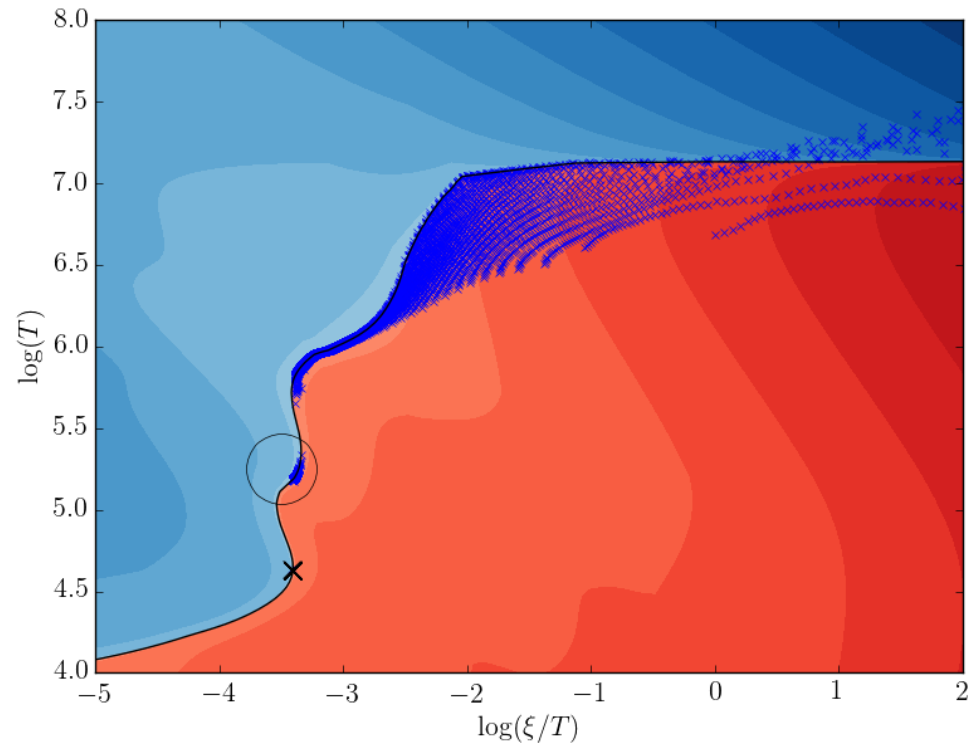
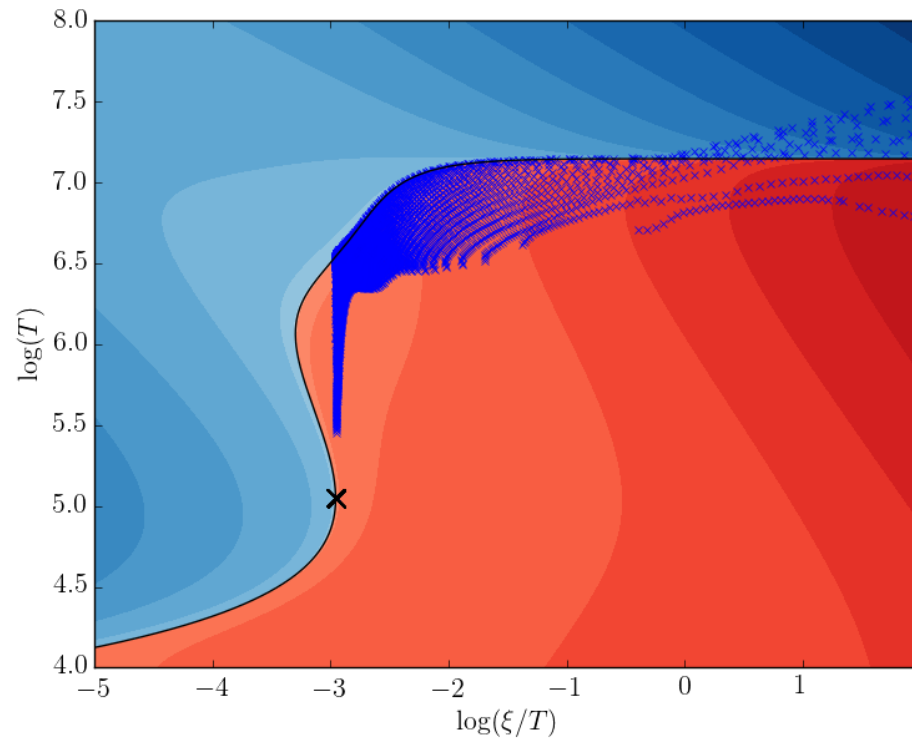
- Increased domain size – requires much more space to accelerate
- Outflow arises outside $1R_{\text{IC}}$ – long period systems only?
- Mass loss rate is 15x accretion rate – could destabilise disk



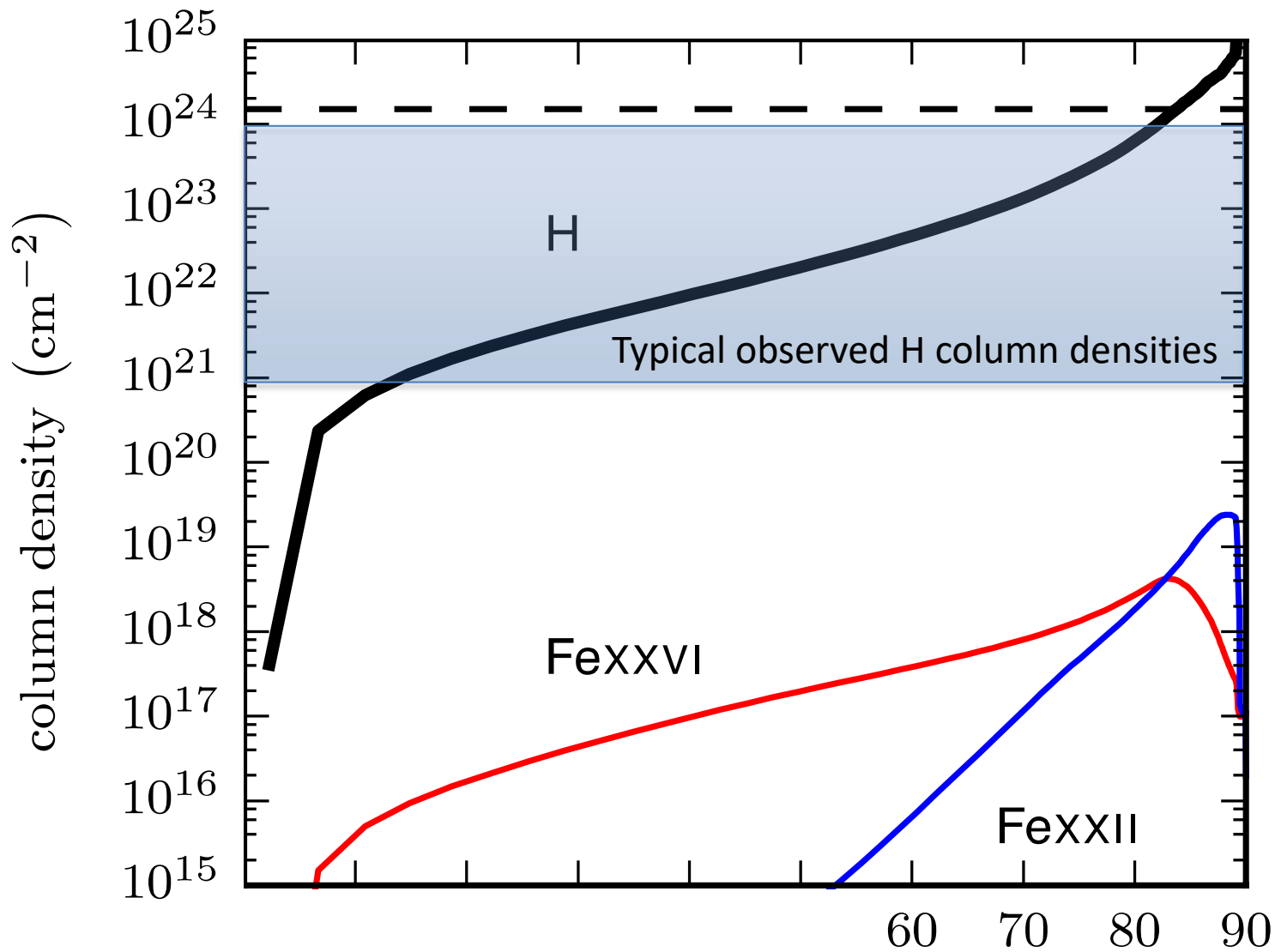
Phase diagrams explain why flow is so different.

Approximate analytic H/C rates

Exact numerical rates



Observables 1: Column densities

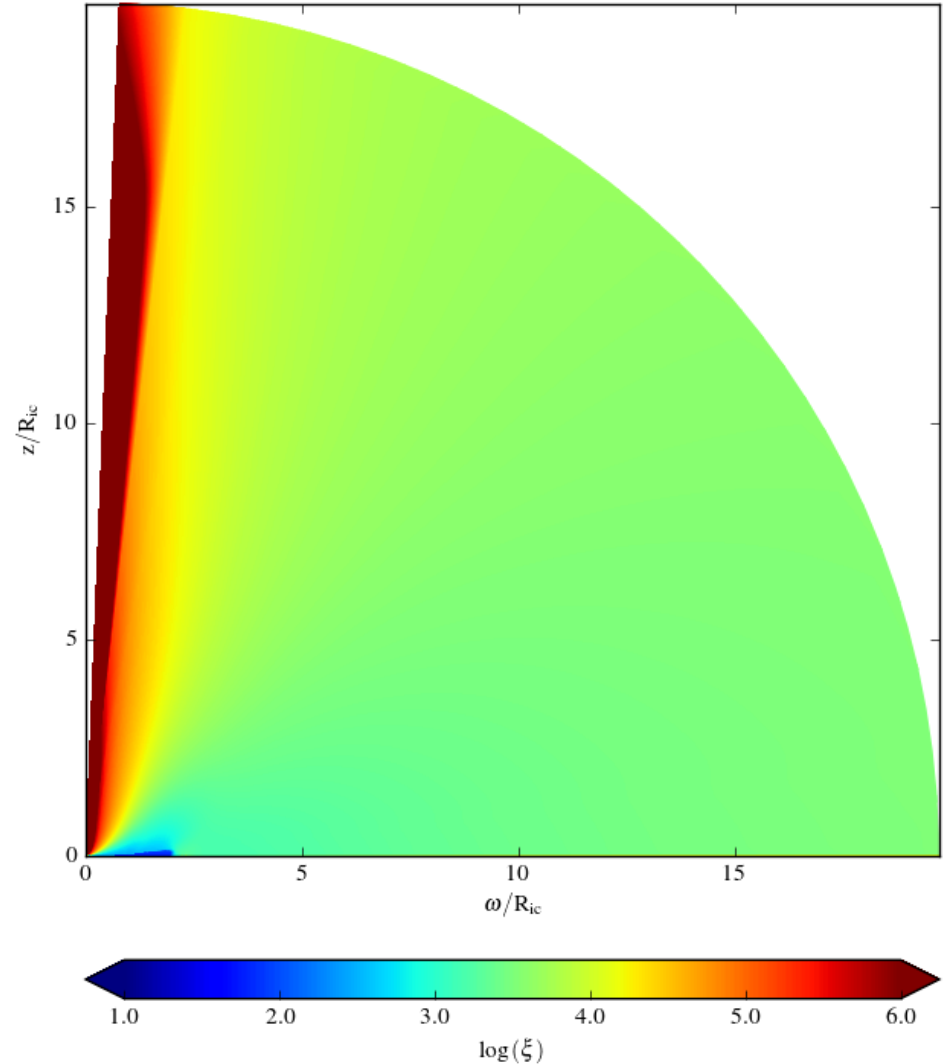
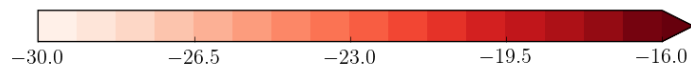
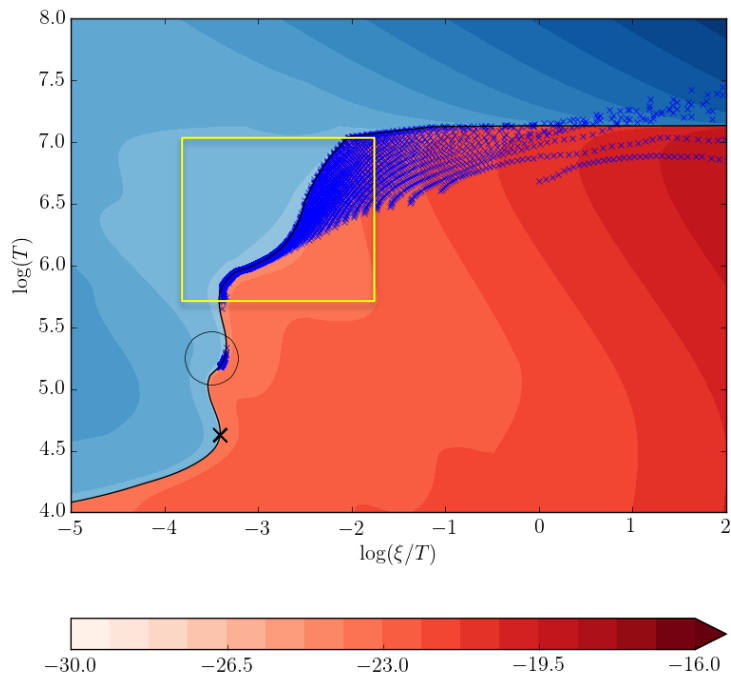


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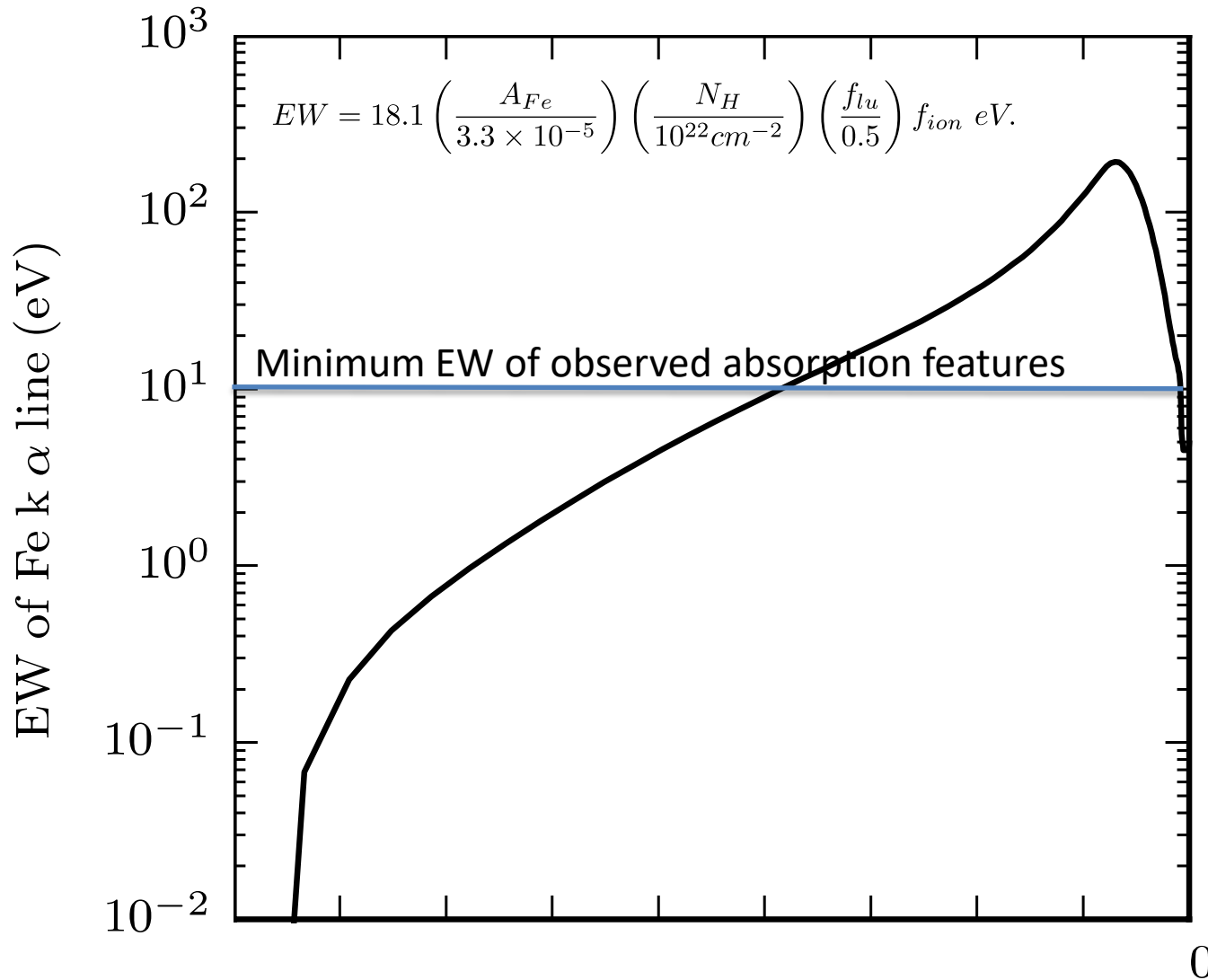
Higginbottom + 17 (in press)

Observables 2 : Ionization parameter

- The value inferred from observations is $\log(\xi) \approx 3$

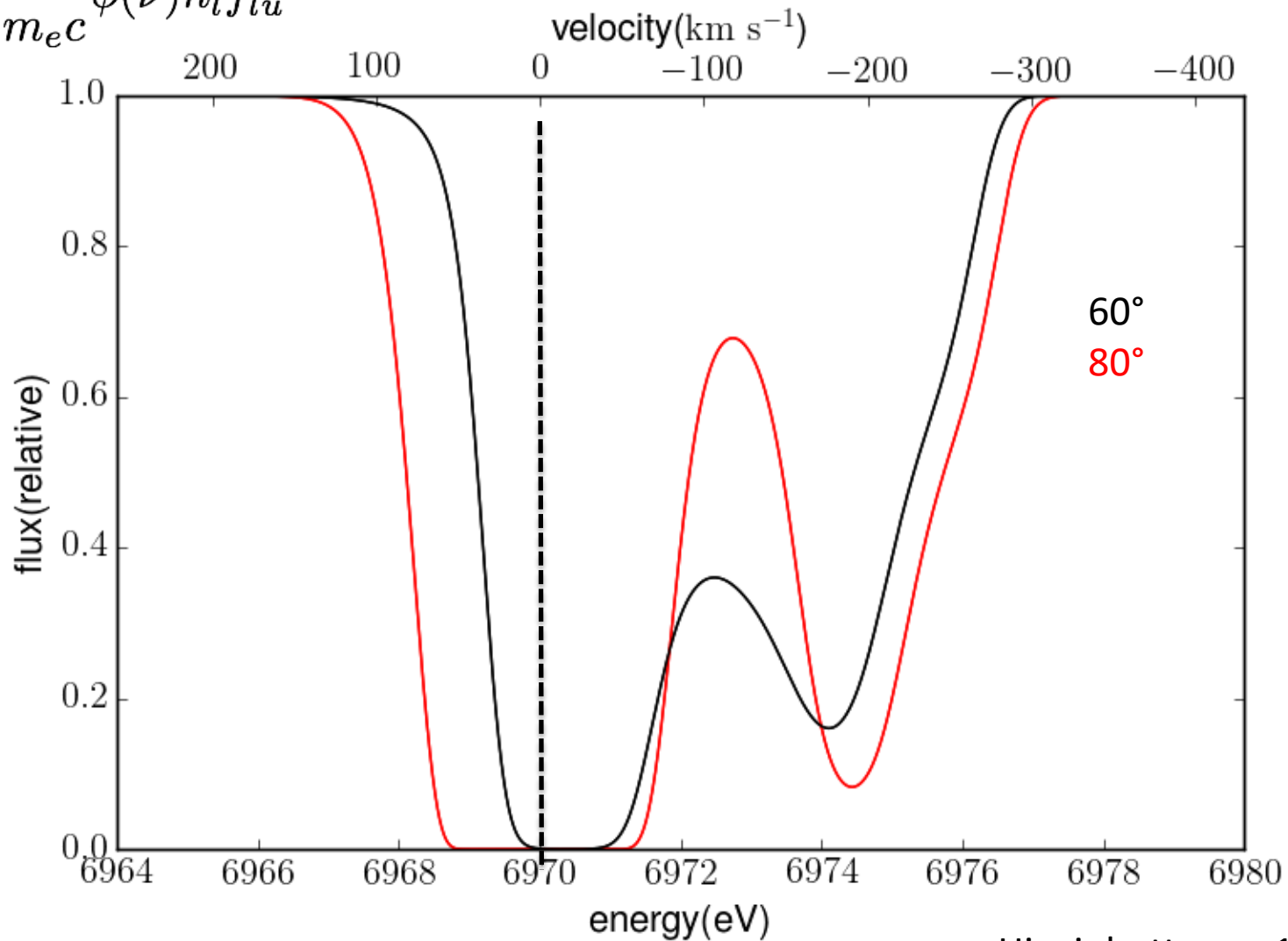


Observables 3 : Equivalent widths



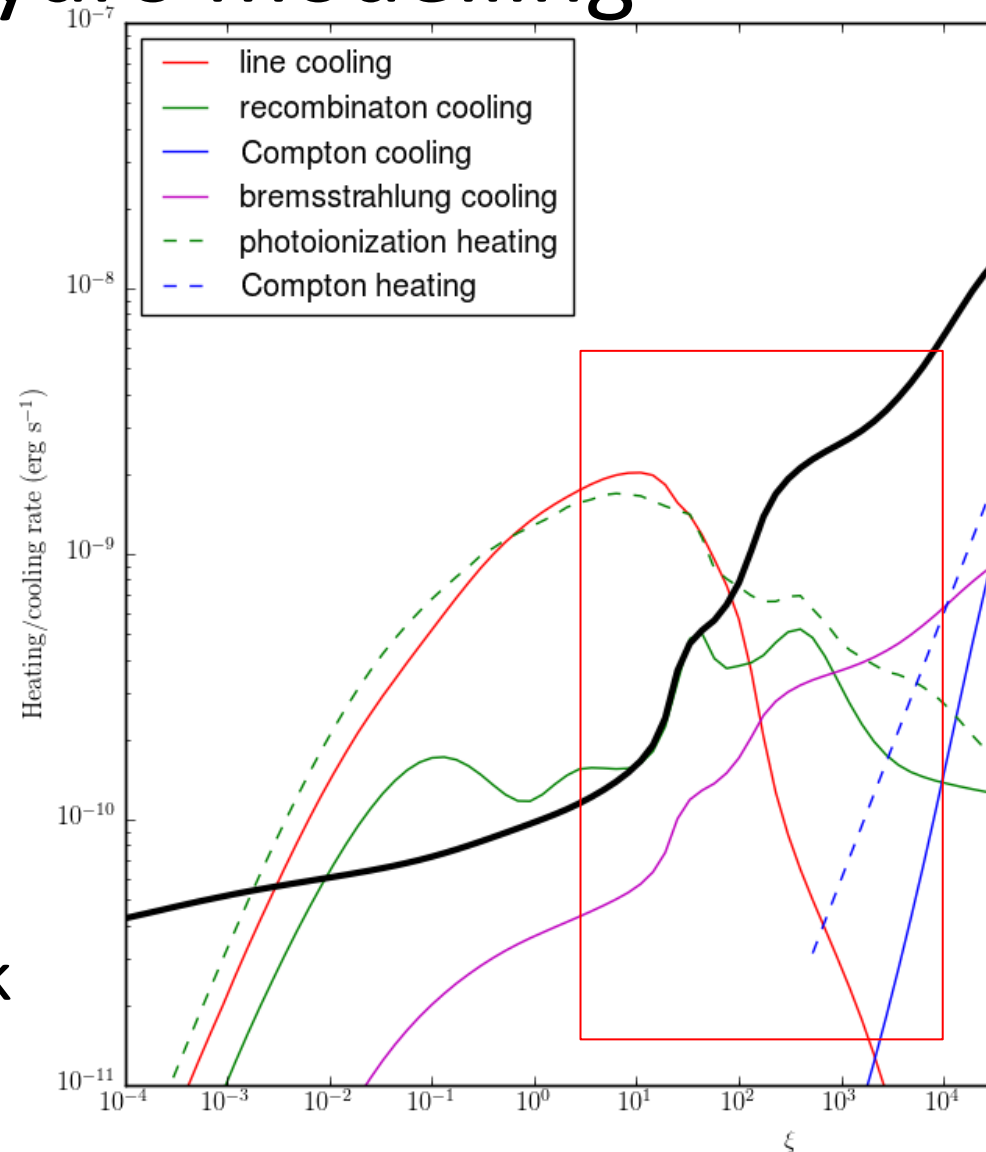
Observables 4: Synthetic Fe K α Absorption line

$$\alpha(\nu) = \frac{\pi e^2}{m_e c} \phi(\nu) n_l f_{lu}$$

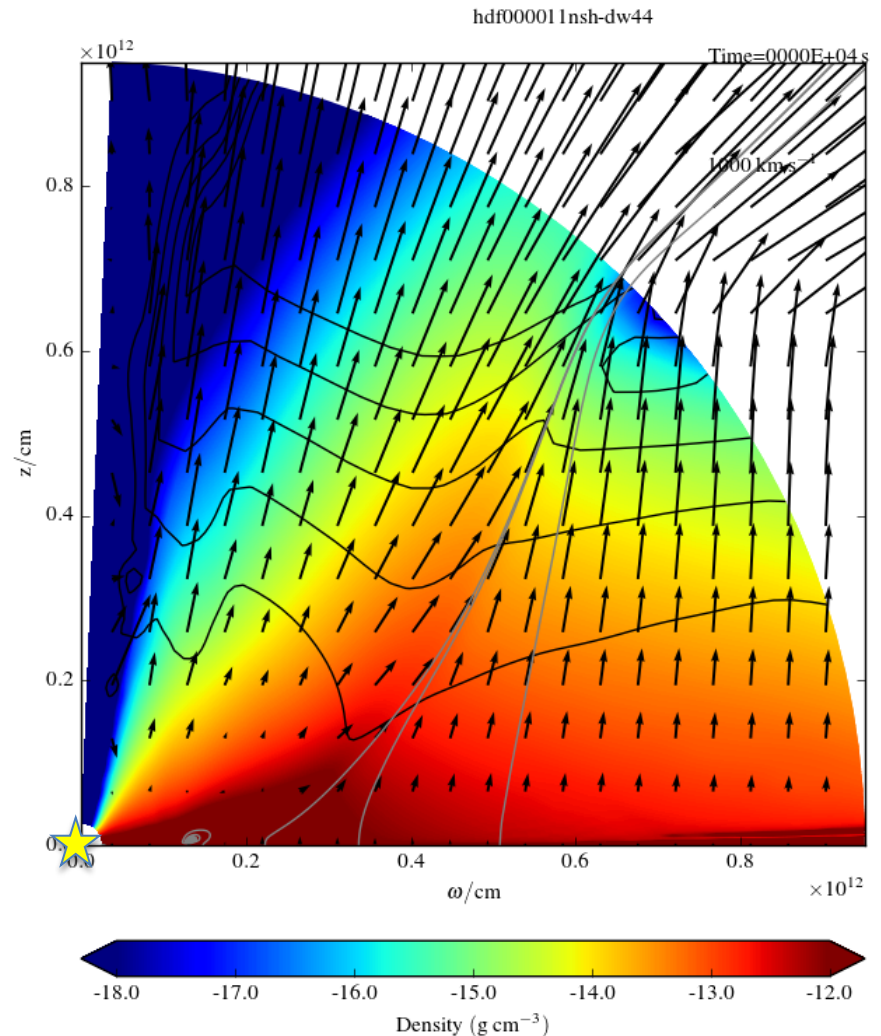
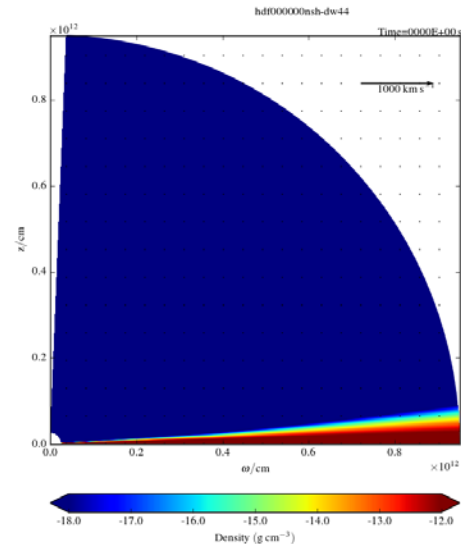


The next step – full Radiation Transport / Hydro modelling

- Onset of thermal instability drives the outflow
- The precise form of the transition defines the properties of the wind.
- The mechanisms responsible are highly sensitive to SED/RT
- Must include RT to check the effect



An operator splitting method for RT-Hydro



- Run initial simulation for a short while
- Import geometry (v, T, ρ) into our Monte Carlo RT code
- Compute ionization state and hence heating/cooling rates
- Import updated estimates of H/C rates and apply correction factors in hydro.
- Repeat to convergence.

Summary

- Thermal winds generated from accurate heating and cooling rates are currently:
 - Moderately dense (optically thick at the base)
 - Slow (Less than typically observed blue shifted absorption line velocity)
 - Have mass loss rates just about sufficient to destabilize the disk (state change?)
 - Arise at large radii (Need long period systems)
- Next step – full radiative transfer treatment.
 - Different SEDs? (Dyda+ 16)
 - Then line driving simulations for AGN.