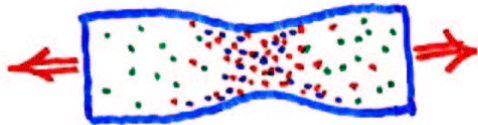


# DYNAMICS OF SHEAR-TRANSFORMATION ZONES IN AMORPHOUS SOLIDS

J.S. Langer, UCSB

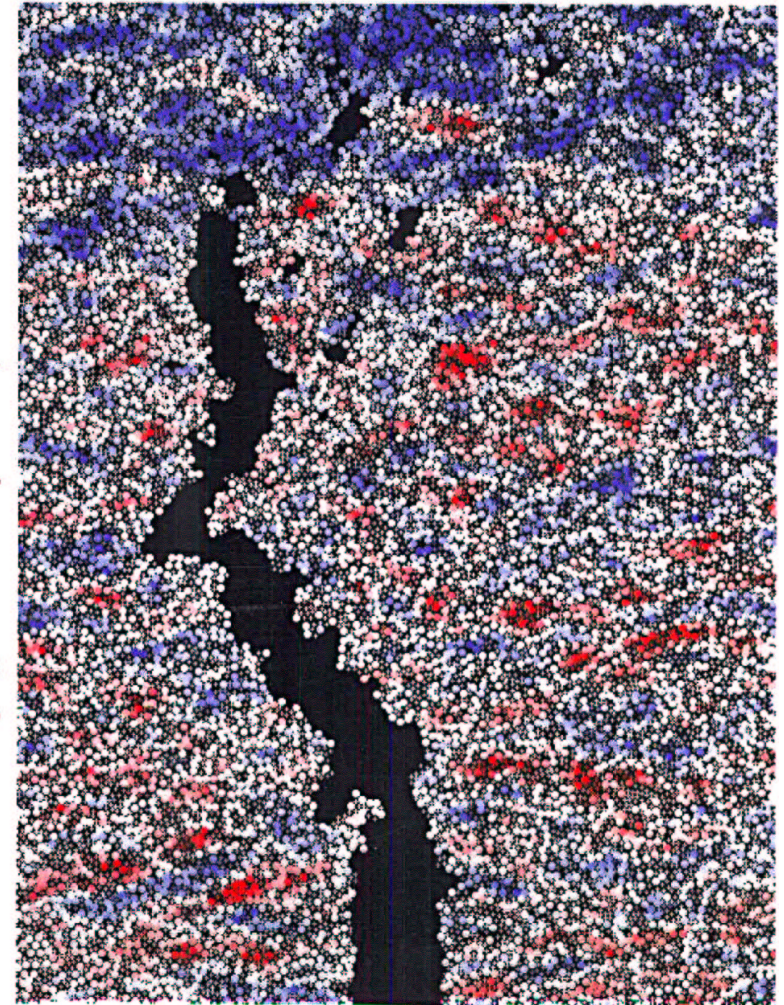
KITP Conference on Glassy States of Matter  
May 19, 2003



Collaborators: M. Falk, L. Pechenik,  
A. Lemaitre, L. Eastgate, C. Malen,  
A. Foglia

## M. Falk Closeup of Crack Tip In Brittle Fracture

$10^5$  Molecule 2D Compressed LJ Solid with distribution of molecular radii  
colored by  $\sigma_{yy}$  - red = compression, blue = tension

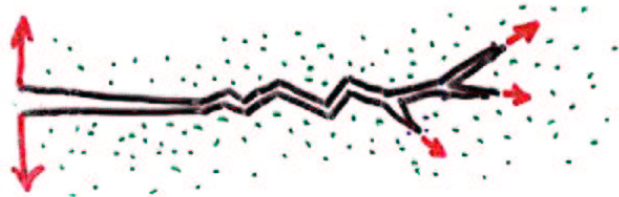


**FUNDAMENTAL PUZZLES IN FRACTURE DYNAMICS**

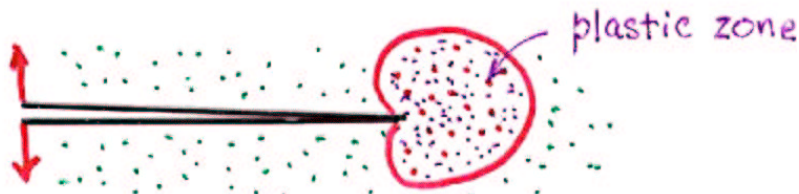
How can we understand brittle and ductile behaviors, especially in noncrystalline solids?



What is the origin of dynamic instabilities in brittle fracture?

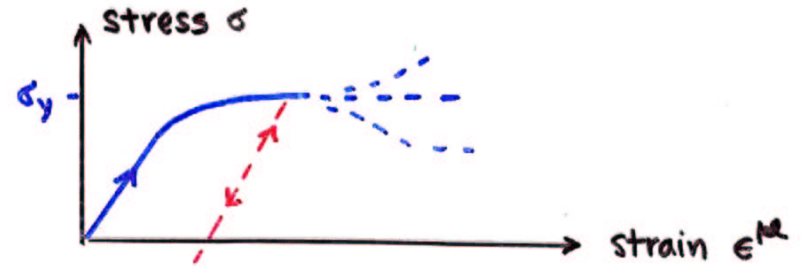


If there is always a plastic yield stress, how can a (higher) breaking stress be transmitted to a crack tip?



CONVENTIONAL DESCRIPTIONS OF PLASTICITY

Time - Independent



Rate - Dependent





What would be a suitable form for a theory of plasticity?

Equations of Motion

$$\frac{d\epsilon^p}{dt} = F(\sigma, \Delta, \dots)$$

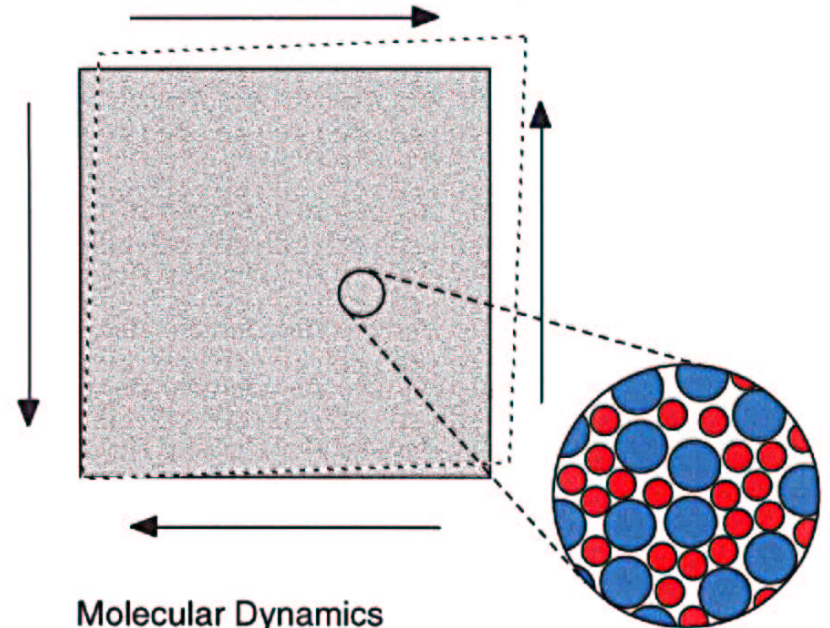
$$\frac{d\Delta}{dt} = G(\sigma, \Delta, \dots)$$

$\sigma$  = stress;  $\epsilon^p$  = plastic strain

$\Delta_{i,j}$  = internal state variables (not including  $\epsilon^p$ )

Later, we must generalize these equations to include elasticity, boundary conditions, etc. – and construct a theory of large-scale deformations.

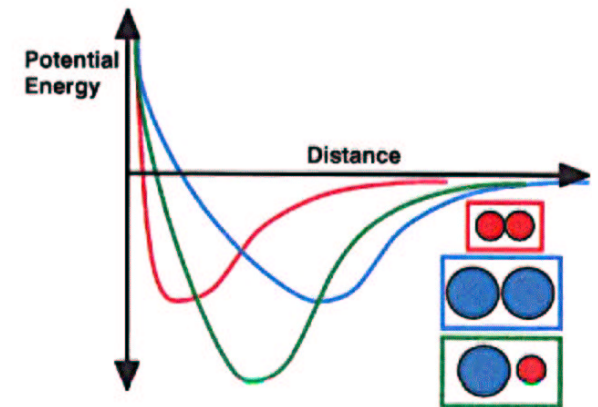
2-D 2-Component LJ Solid Under Applied Simple Shear



Molecular Dynamics

with modified equations of motion to include:

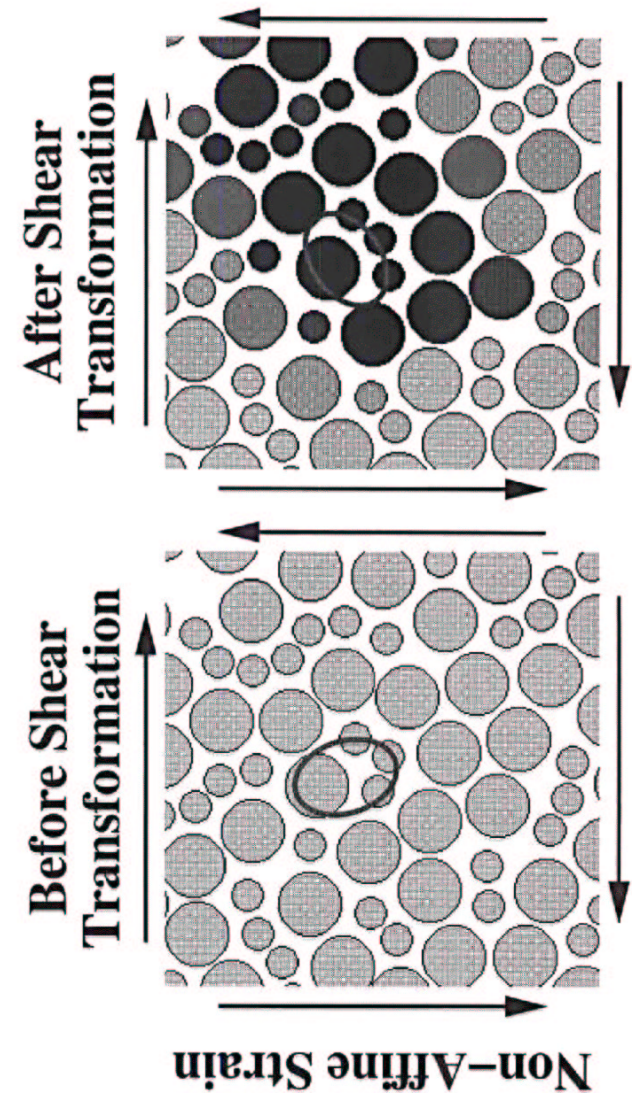
- Thermostat
- Pressure-Stress Barostat





## Periodic Cell Under Applied Pure Shear Stress

red regions denote areas of local deviation from affine deformation

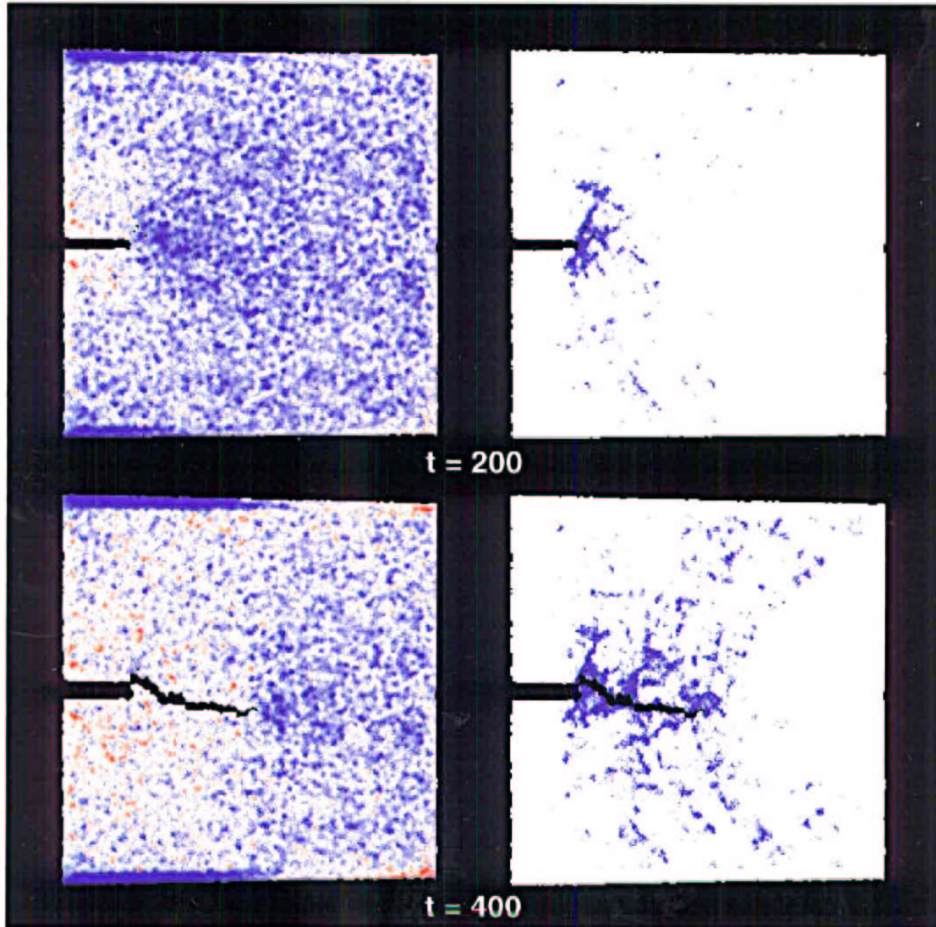




# Brittle Crack

Local Hydrostatic Stress

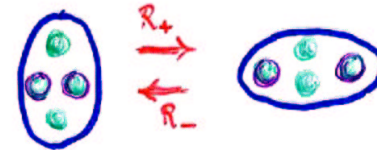
Local Non-Affine Rearrangement



## Dynamics of Shear-Transformation Zones (STZ's)

M. Falk and JSL, PRE 1998

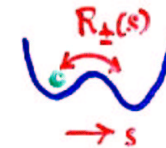
### Simple Two-State Version



Plastic strain rate:  $\dot{\epsilon}^p \sim R_+ m_+ - R_- m_-$

$m_{\pm}$  = density of  $\pm$  STZ's       $s$  = deviatoric stress

Transition rates:



$$\dot{m}_{\pm} = R_{\mp} m_{\mp} - R_{\pm} m_{\pm} + \Gamma(s, \dots) (A_{02} - A_{ann} m_{\pm})$$

$\Gamma(s, \dots) \hat{=}$  STZ creation and annihilation rates

$\sim$  Energy dissipation rate (Pechenik)

**STZ ORDER PARAMETERS  
(Internal State Variables)**

$\Lambda = \frac{n_+ + n_-}{m_\infty} =$  scaled, scalar density of STZ's

$\Delta = \frac{n_- - n_+}{m_\infty} =$  orientational bias of STZ's (becomes a traceless, symmetric tensor)

$m_\infty = \frac{2A_{cr}}{A_{ann}} =$  steady-state density of STZ's

Are there other relevant dynamical state variables?

**QUASILINEAR EQUATIONS OF MOTION**

(do not account properly for memory effects)

$\Lambda \rightarrow 1; \quad s/s_y \rightarrow \tilde{\sigma}$

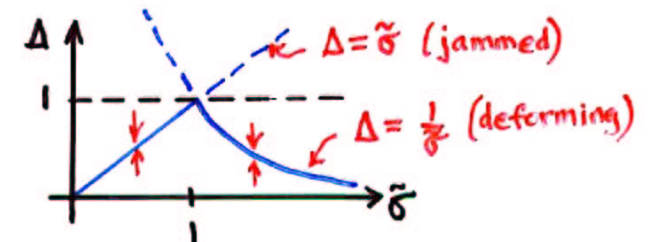
$S_y =$  yield stress = combination of material parameters and couplings

$\dot{\epsilon}^{pl} \sim \tilde{\sigma} - \Delta \sim$  ("effective stress")

$\Gamma(\tilde{\sigma}, \Delta) = \frac{(\tilde{\sigma} - \Delta)^2}{1 - \Delta^2} \sim$  dissipation rate

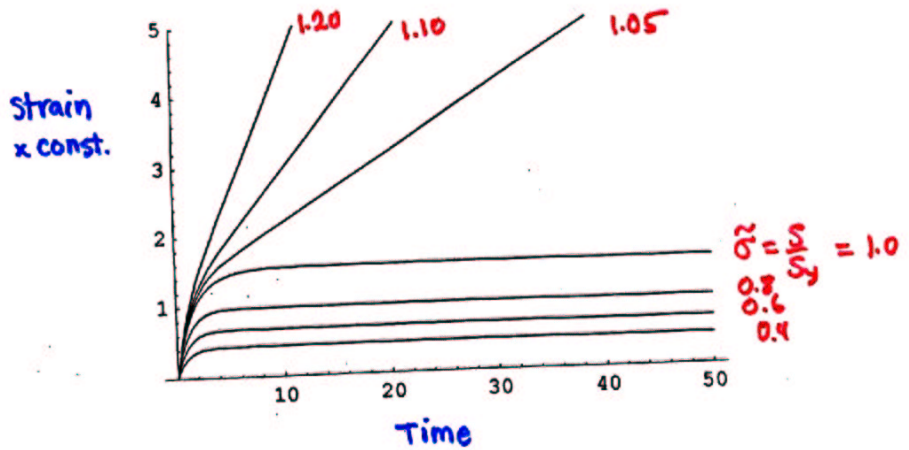
$\dot{\Delta} \sim \frac{(\tilde{\sigma} - \Delta)(1 - \tilde{\sigma}\Delta)}{1 - \Delta^2}$

Dynamic interpretation of the yield stress: Exchange of stability between non-deforming jammed states at low stresses and plastically deforming states at higher stresses.



QUASI-LINEAR STZ THEORY

"Creep Tests" (constant stress)



Energy Balance (Pechenik + JSL)

STZ STATE VARIABLES

$\Lambda \sim$  density of STZ's

$\Delta \sim$  orientational bias

Strain rate  $\dot{\epsilon} \sim \Lambda \tilde{\sigma} - \Delta$

$$\dot{\Delta} = \Lambda \tilde{\sigma} - \Delta - \Gamma(\tilde{\sigma}, \Lambda, \Delta) \Delta$$

$$\dot{\Lambda} = \Gamma(\tilde{\sigma}, \Lambda, \Delta) (1 - \Lambda)$$

$\tilde{\sigma} =$  deviatoric stress / yield stress

$\Gamma(\tilde{\sigma}, \Lambda, \Delta) \sim$  STZ creation and annihilation rates

What is  $\Gamma(\tilde{\sigma}, \Lambda, \Delta)$  ?

(Original F-L conjecture  $\Gamma \sim \dot{\epsilon} \cdot s$  -i.e. plastic work; but  $\dot{\epsilon} \cdot s < 0$  during unloading.)



Energy balance:  $\tilde{\sigma} \dot{\epsilon} \sim \frac{d}{dt} \psi(\Lambda, \Delta) + Q(\tilde{\sigma}, \Lambda, \Delta) *$

$\psi(\Lambda, \Delta)$  = recoverable energy associated  
with the STZ degrees of freedom.

$Q(\tilde{\sigma}, \Lambda, \Delta)$  = dissipation rate  $\geq 0$  (2nd Law)

Pechenik's conjecture:  $Q(\tilde{\sigma}, \Lambda, \Delta) = a(\Lambda) \Gamma(\tilde{\sigma}, \Lambda, \Delta)$

Use  $\frac{d\psi}{dt} = \frac{\partial \psi}{\partial \Lambda} \dot{\Lambda} + \frac{\partial \psi}{\partial \Delta} \dot{\Delta}$  and solve \* for  $\Gamma$ .

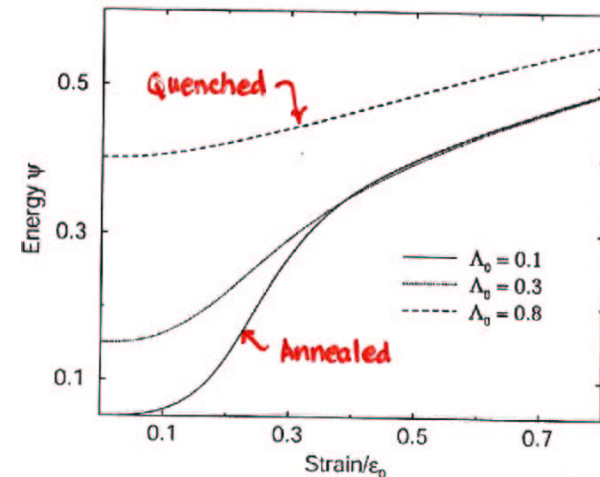
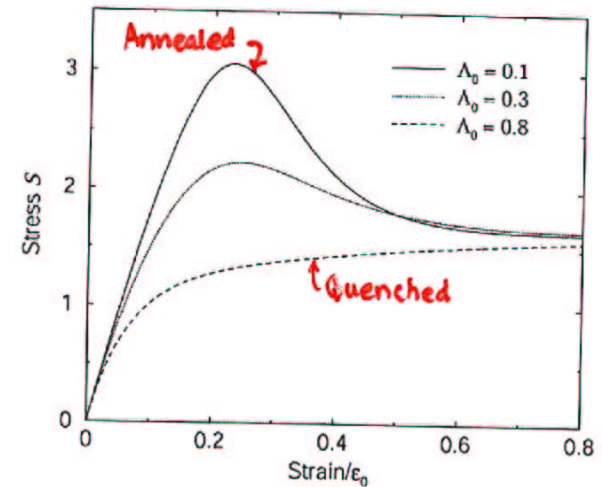
The result is:

$$\Gamma(\tilde{\sigma}, \Lambda, \Delta) = \frac{2\Lambda (\Lambda \tilde{\sigma} - \Delta)^2}{(1+\Lambda)(\Lambda^2 - \Delta^2)}$$

$$a(\Lambda) = \Lambda$$

$$\psi(\Lambda, \Delta) = \frac{\Delta^2}{2\Lambda} + \frac{1}{2}\Lambda$$

Constant strain rate simulations





O.A. Hasan and M. C. Boyce, Polymer 34, 5085, (1993)  
 Constant strain rate loading of polystyrene(PS) sample

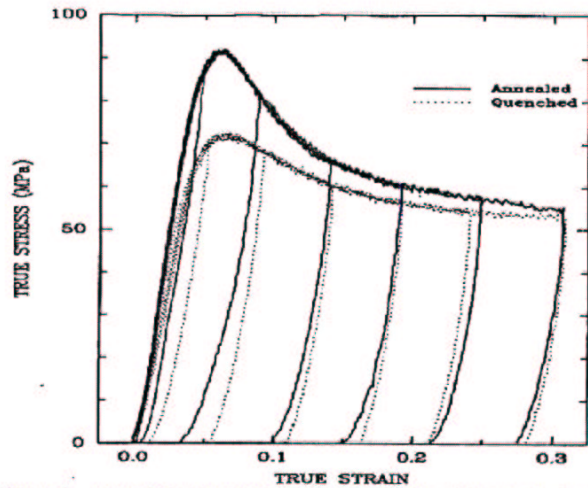


Figure 2 Annealed and quenched PS loaded to different strains at temperature 296 K and strain rate  $-0.001 \text{ s}^{-1}$

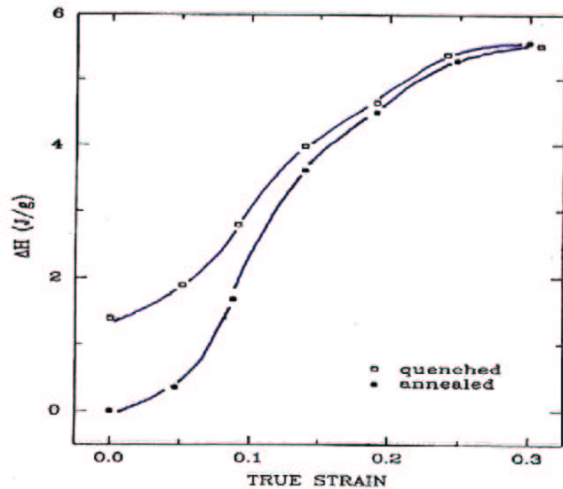


Figure 4 Change in enthalpy of annealed and quenched PS with increasing strain ( $\rho = 1.06 \text{ g cm}^{-3}$ )

## DISORDER TEMPERATURE (Lemaitre)

$$\text{Steady-state density of STZs} \sim n_{ss} \sim \frac{\text{Creation rate}}{\text{Annihilation rate}} \sim \frac{e^{-1/\chi}}{1}$$

$\chi \sim$  disorder temperature  $\rightarrow T$  in equilibrium?

$$\dot{\chi} = c_1 \dot{\epsilon} - c_2 e^{-\chi/\chi_0}$$

Rate of energy dissipation by plastic deformation

Slow, spontaneous relaxation  $\sim \Lambda^{-\chi}$

Results:

Constant strain rate:  $\dot{\epsilon}^{pl} \sim \frac{1}{q\tau} (\tilde{\sigma}^2 - 1)^{\chi/2 - 1}$

$$\chi \sim -\frac{\chi}{\ln \dot{\epsilon}^{pl}} \text{ for } \dot{\epsilon}^{pl} \rightarrow 0$$

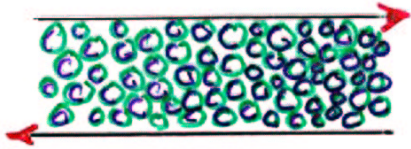
Stress relaxation for  $\tilde{\sigma} \gg 1$ ;  $\dot{\epsilon}^{tot}$  fixed

$$\tilde{\sigma}(t) \sim \exp[-\text{const.} \cdot t^\beta]$$

$$\beta = 1 - \frac{1}{\chi}$$

Effective Temperatures

Ono et al., "Effective Temperatures of a Driven System Near Jamming," PRL 89, 095703 (2002).



Numerical simulation of a sheared foam: Temperature, computed in several independent ways, goes to a non-zero constant in the limit of vanishing shear rate !! ( $\dot{\epsilon} \rightarrow 0$ )

This result is implied by STZ-like theories, essentially by dimensional analysis:

Viscosity  $\eta \sim s_y / \dot{\epsilon}$

Diffusion constant  $D \sim l^2 \dot{\epsilon}$

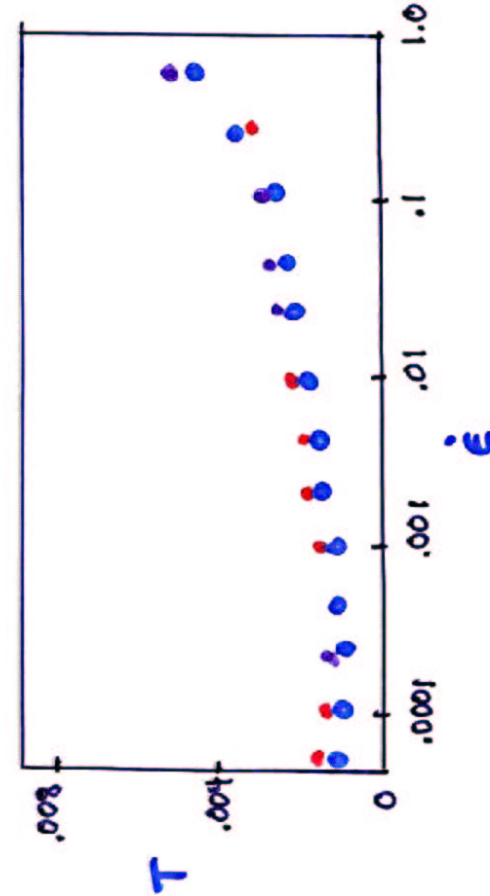
$l \sim$  jump size  $\sim$  bubble size

Response-fluctuation theorem

$$D \sim \frac{T_{\text{eff}}}{\eta l} \Rightarrow T_{\text{eff}} \sim s_y l^3$$

What is the meaning of this non-equilibrium effective temperature?

Effective Temperatures of a Driven System Near Jamming



PRL 89, 095703 (2002)

Ono, O'Hern, Durian, Langer (S), Liu, Nagel



**CONCLUDING REMARKS**

**There is a wide range of deep, urgent problems to be solved in theories of deformable solids and solid-like materials.**

**Solving these problems will require new ideas about the physics of driven, out-of-equilibrium systems.**

**Solving these problems also will require a much closer interaction between experiment, theory, and numerical simulation than exists today.**