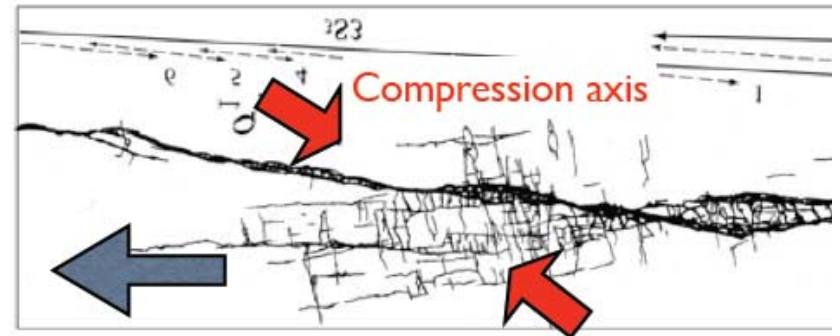
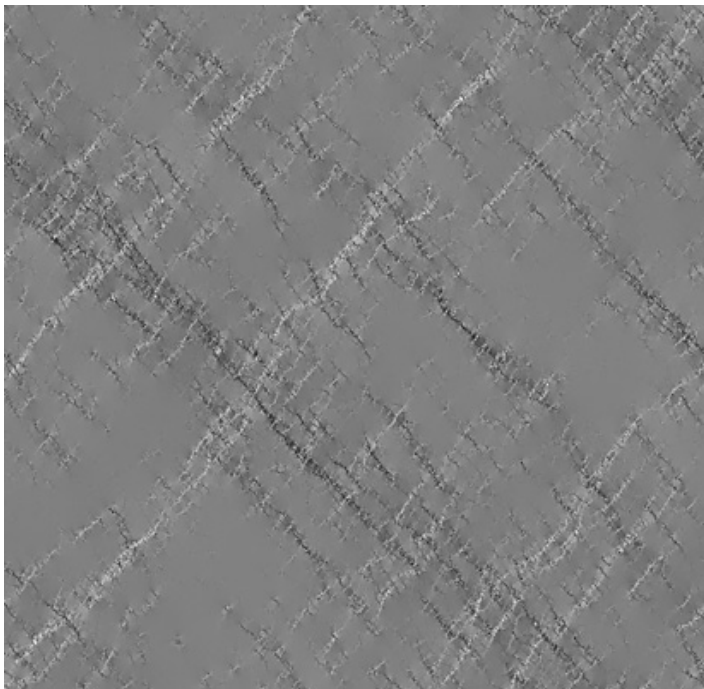


Deformation Mechanisms and Rates in Glasses

M. O. Robbins, K. M. Salerno, J. Rottler, R. S. Hoy, JHU
C. Maloney, Carnegie Mellon Univ,

KITP, June 15, 2010



What values of stress tensor σ_{ij} cause yield?

Isotropic \Rightarrow Construct scalars from eigenvalues of σ_{ij}

$$p = -(\sigma_1 + \sigma_2 + \sigma_3) / 3$$

$$\tau_{dev} = \frac{1}{3} \left[(\sigma_1 - \sigma_2)^2 + (\sigma_2 - \sigma_3)^2 + (\sigma_3 - \sigma_1)^2 \right]^{1/2} \quad \tau_{\max} = \frac{1}{2} |\sigma_i - \sigma_j|_{\max}$$

Classic **yield criteria** for atomic and granular solids:

von Mises \rightarrow yield when shear energy large $U \propto \tau_{dev}^2$

Glasses harder to shear when under pressure

\Rightarrow Pressure-modified von Mises: $\tau_{dev}^y = \tau_0 + \alpha p$

Influence of all $\sigma_i \Rightarrow$ rotating region not sliding on plane

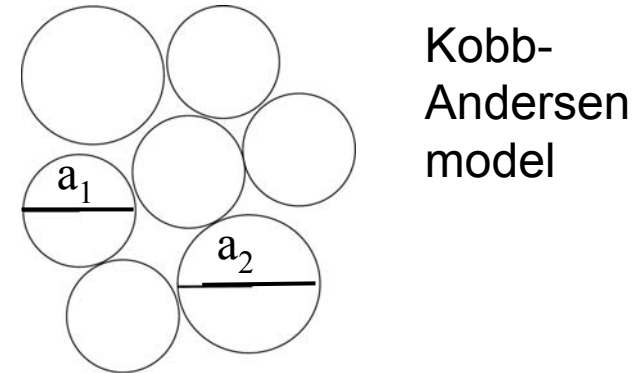
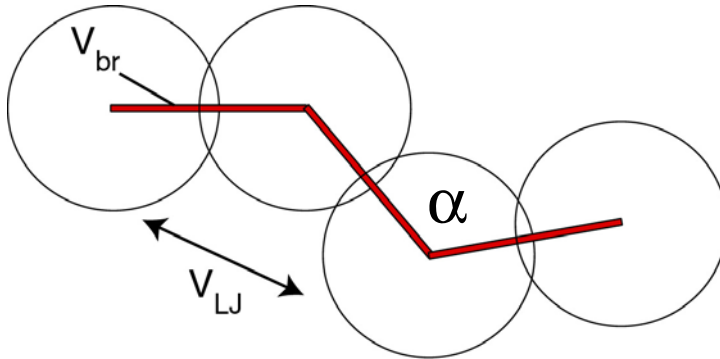
Pressure-modified Tresca (PMT): $\tau_{\max}^y = \frac{3}{\sqrt{2}} (\tau_0 + \alpha p)$

Mohr-Coulomb (MC) \rightarrow friction motivated, anisotropic

Yield if (shear stress)/(normal stress) $> \mu$ on some plane

Potentials and Shear Geometries

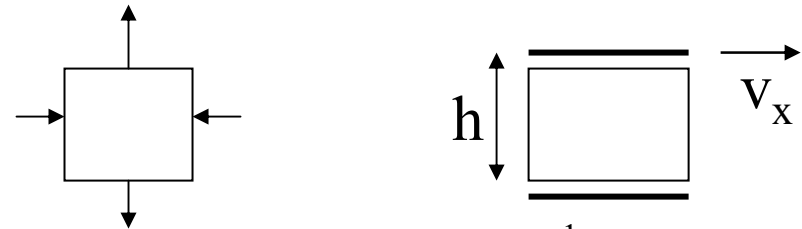
Bead spring model for polymers: Binary mixture: LJ or harmonic



- Lennard-Jones potential $V_{LJ}(r) = 4u_0[(a/r)^{12} - (a/r)^6] \rightarrow$ van der Waals energy $u_0 \sim \text{meV}$, length $a \sim \text{nm}$, time $\tau_{LJ} \sim \text{ps}$, max force f_{LJ}
- Covalent bonds $V_{br} \rightarrow$ FENE potential form linear chains of N spheres bond-angle potential straightens chains \rightarrow change entanglement length N_e
- Competing lengths \Rightarrow Frustration \rightarrow **amorphous glass** below $T_g \sim 0.35u_0/k_B$

Vary T from 0.0 to $0.3u_0/k_B \sim T_g$

Apply strain in two ways:



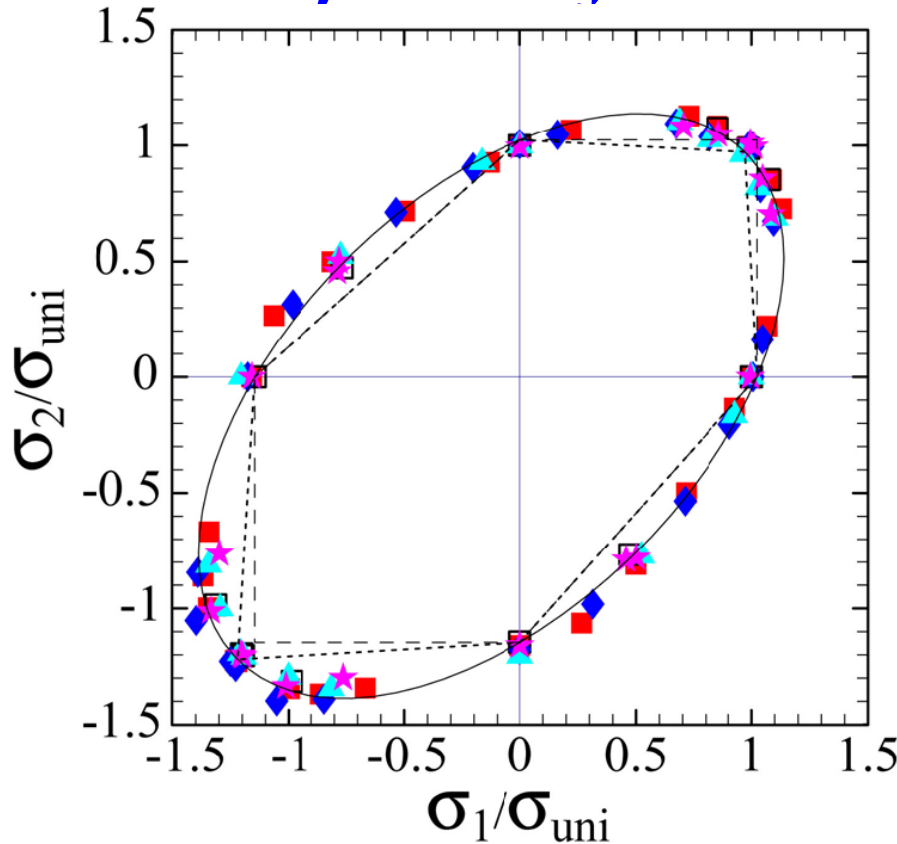
Strain periodic cell by changing L_x, L_y, L_z at fixed $\dot{\epsilon}_z = L_z^{-1} dL_z/dt$

Confine binary mixture between moving walls \rightarrow mean $\dot{\gamma} = v_x/h$

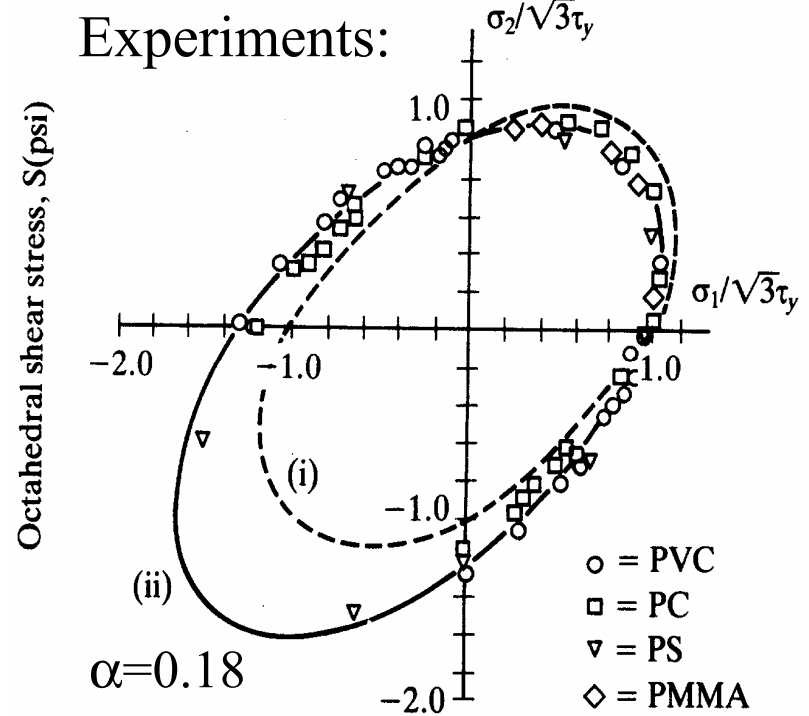
At least 32,768 beads in system unless noted

Test of shear yield criteria for biaxial loading

Phys. Rev. E 64, 051801 (2001)



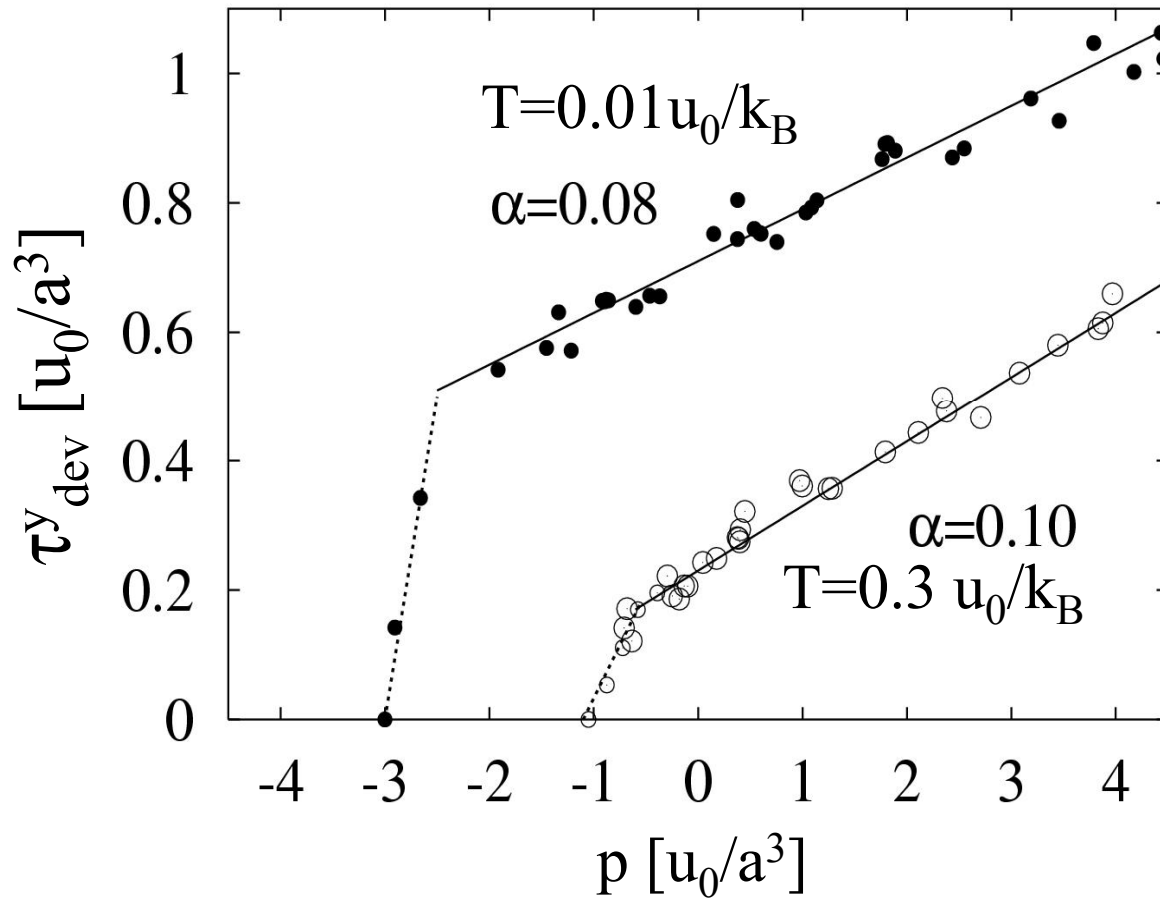
$T=0.01-0.3 \sim T_g$, binary LJ,
short & long chains, flex & semiflex



From: T.H.Courtney, Mechanical Behavior of Materials

- Define yield by peak in stress-strain curve. 0.2% yield gives same behavior
- **Pressure modified Von Mises** → elliptical yield surface fits data for different chain lengths, bond-angle forces, system sizes, adhesion
- Tresca (dotted) and Mohr-Coulomb (dashed) → polygonal yield surface, poor fit

Pressure-modified Von Mises collapses multiaxial results



Equally good collapse for binary mixture, flexible & semiflexible polymers

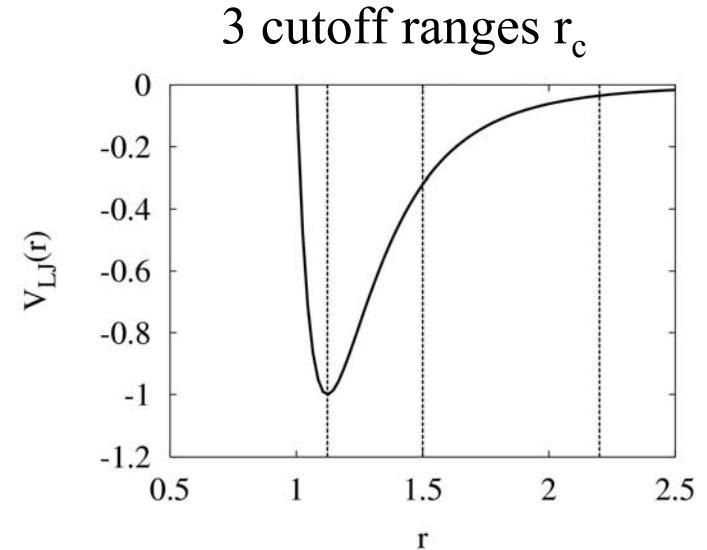
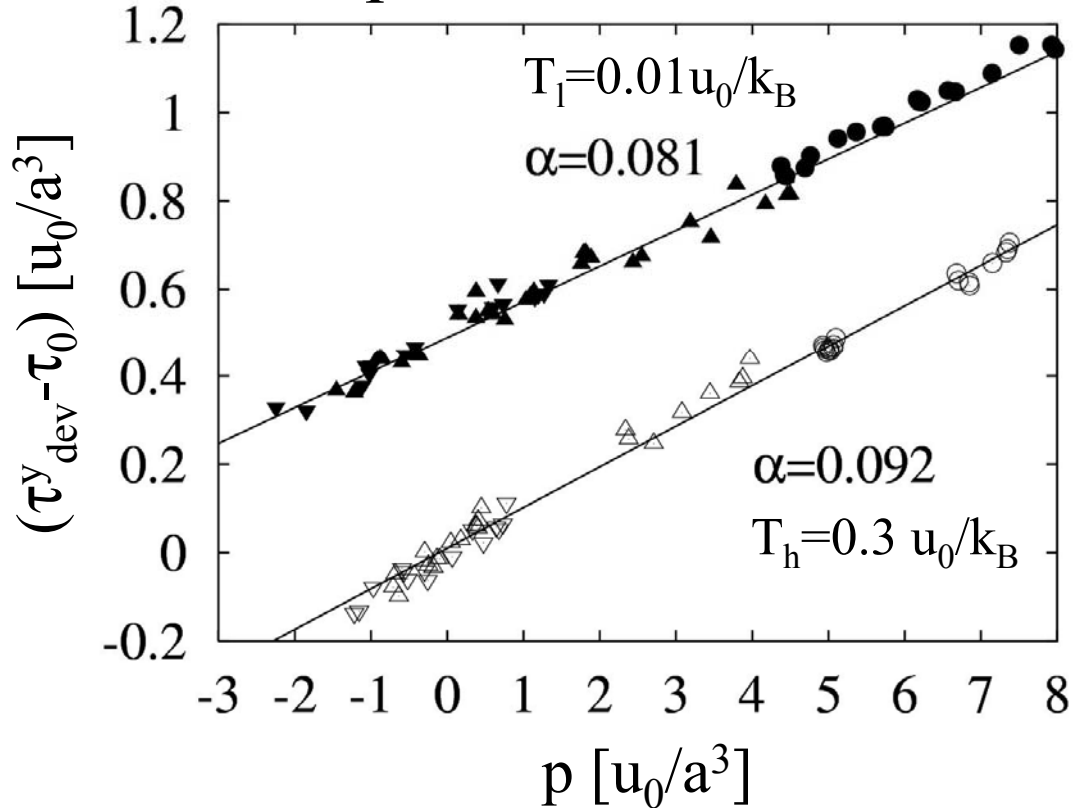
(JR and MOR, Phys. Rev. E 64, 051801 (2001))

\Rightarrow Von Mises criterion $\tau^y_{dev} = \tau_0 + \alpha p$ describes yield by **shear** under multiaxial loading (solid lines)

\Rightarrow Fails when system **cavitates** \rightarrow craze forms if $N \geq 2N_e$
New criteria for cavitation $p^c = p_0 + \beta \tau_{dev}$ (dashed lines)

What determines τ_0 and α ?

Data collapse for 3 different amounts of adhesion $\rightarrow r_c$

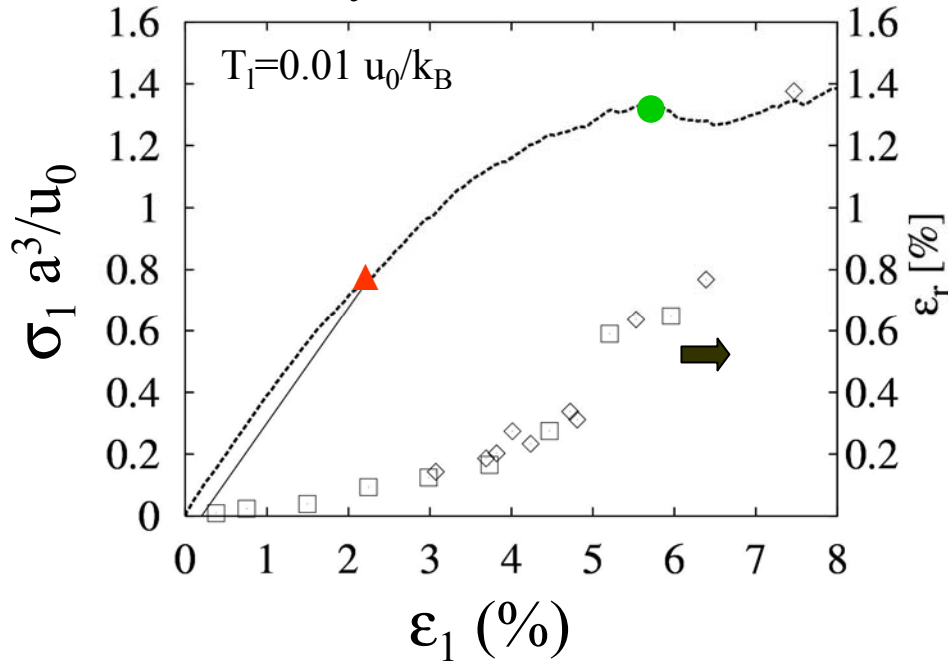


$$\tau_{dev}^y = \tau_0 + \alpha p$$

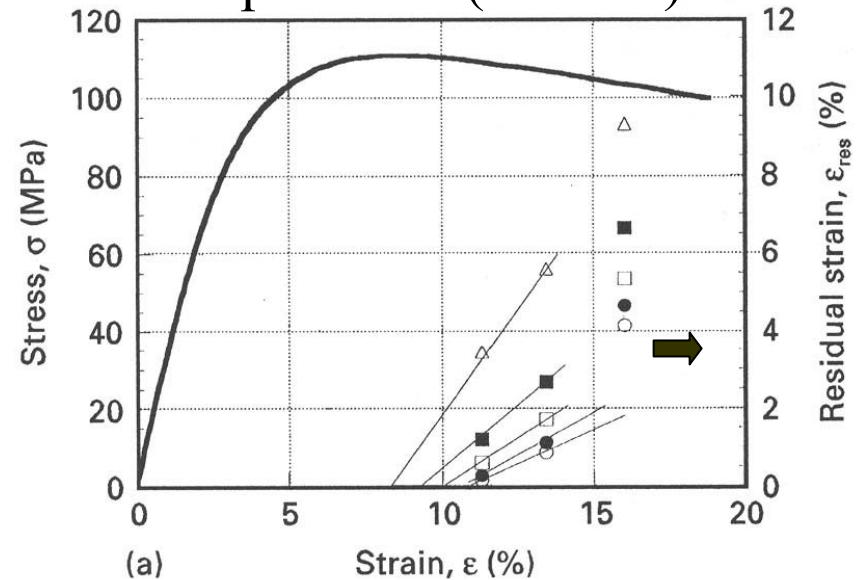
- τ_0 set by adhesive interaction (cutoff range r_c)
- α independent of r_c , set by bead geometry, as in solid friction
- No dependence on chain length N , only local structure important
- Difficulty of rotating region increases with pressure confining it

Residual Strain After Stress Cycle \rightarrow No Elastic Region

Polymer Simulation



Experiment (PMMA)

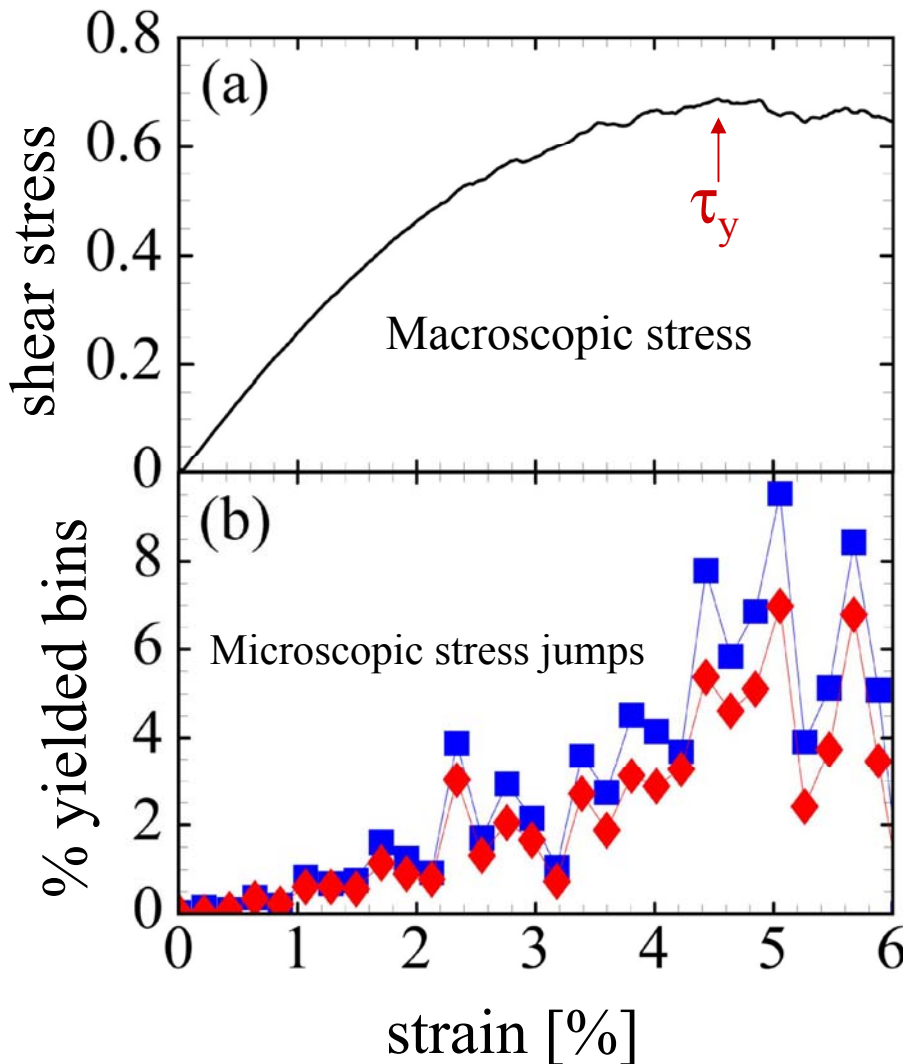


(a) Quinson et al., J. Mat. Sci. **32**, 1371 (1997)

- Simulation and experiment show similar stress curves
- Simulations indicate any nonzero strain gives $\epsilon_r > 0$ in thermodynamic limit!
- As increase system size \rightarrow first event at smaller strain
 \rightarrow decrease structure on σ_1 from individual plastic events
- Common to define yield at maximum stress \bullet , 0.2% yield stress \blacktriangle

Microscopic plastic events during shear

J. Rottler and M. O. Robbins, Comp. Phys. Comm. (2005)



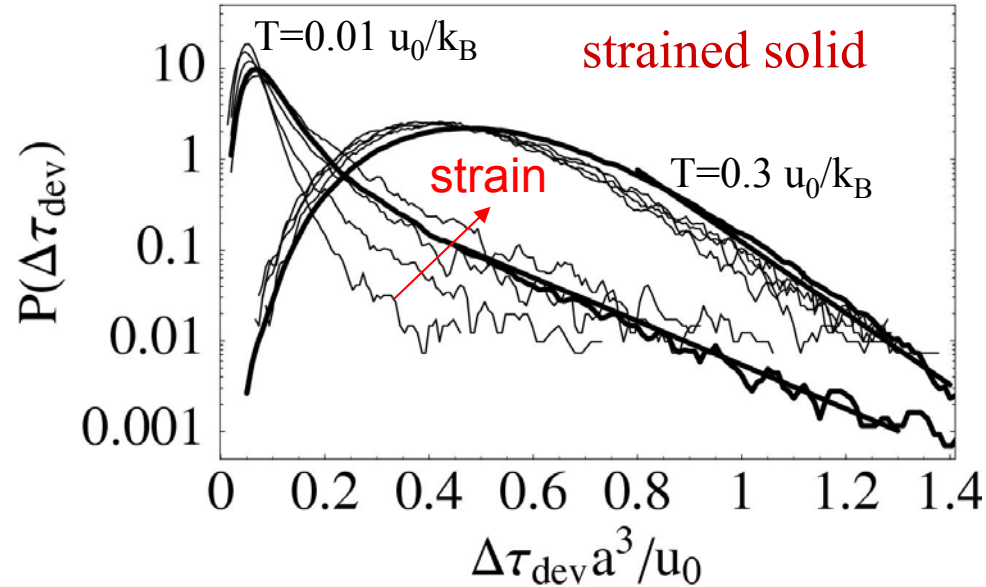
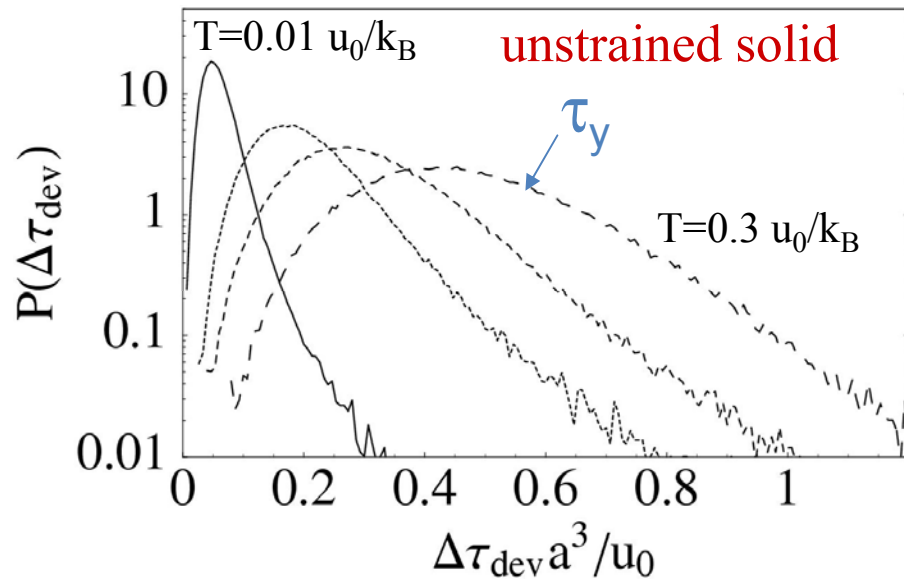
- Divide solid into small volumes: $8a^3$
- Calculate shear stress and nonaffine disp. $\sum_i (r_i - \epsilon_{ij} r_j)^2$ in each
- Record number of jumps in a small strain interval as a function of strain
- # and size of stress jumps rises rapidly as peak stress is approached, but present at arbitrarily small strains
 → no clear point where yield starts
 → Identify yield stress with initial peak in octahedral stress
- At low T, strain increases event rate
- Near T_g the rate of events is nearly independent of strain

MR4

What can one say about relation between rate of plastic deformation and deviation from linear elasticity? Is it a tautology that the acoustic emission tracks the anelastic behavior, or does one need to look at work and energy to figure this out?

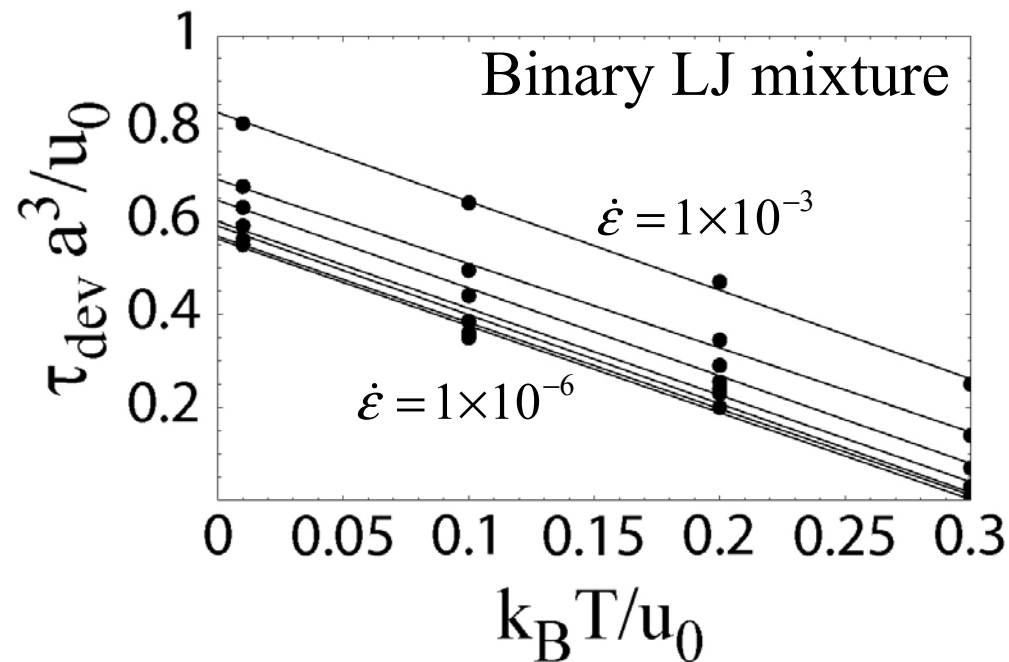
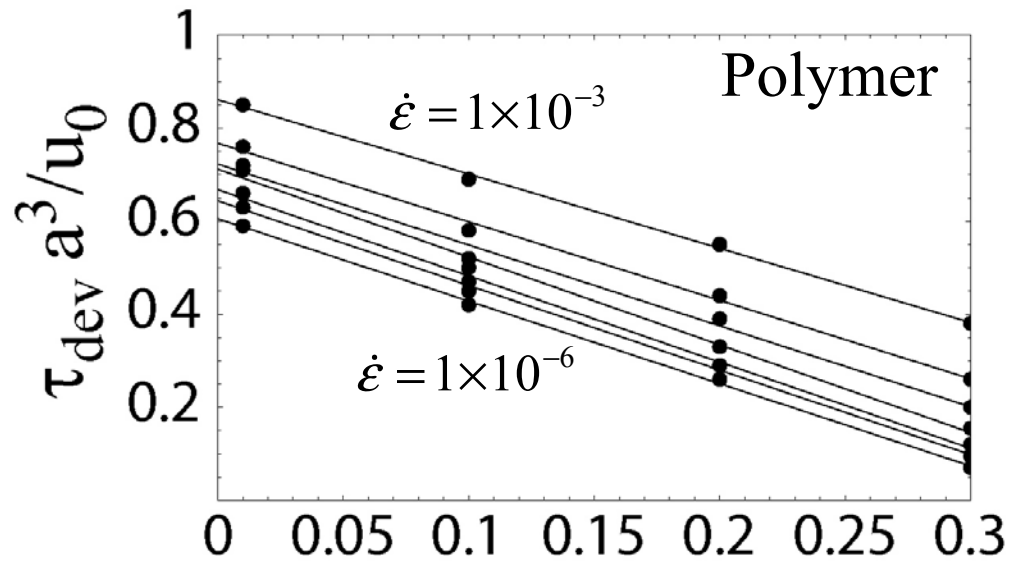
Mark Robbins, 2/4/2007

Microscopic Stress Dynamics



- $\Delta\tau_{\text{dev}}$ - change in **local stress tensor** over $7.5\tau_{LJ}$ in small volume elements containing 7-8 particles
- close to $T_g=0.35$, $P(\Delta\tau_{\text{dev}}) \sim$ independent of shear strain
- low T , tail grows with increasing strain
- tail can be fitted to **exponential**, similar slope near peak stress as for steady shear – dark lines \Rightarrow microscopic evidence for noise temperature “x”?

Temperature dependence of τ^y_{dev}



- Both models show linear decrease in τ^y_{dev} as T rises (fix $p=0$ not density)
- Slope independent of strain rate, offset varies with rate
- Yield stress vanishes above rate-dependent “ T_g ”

Thermal and Energetic Stresses

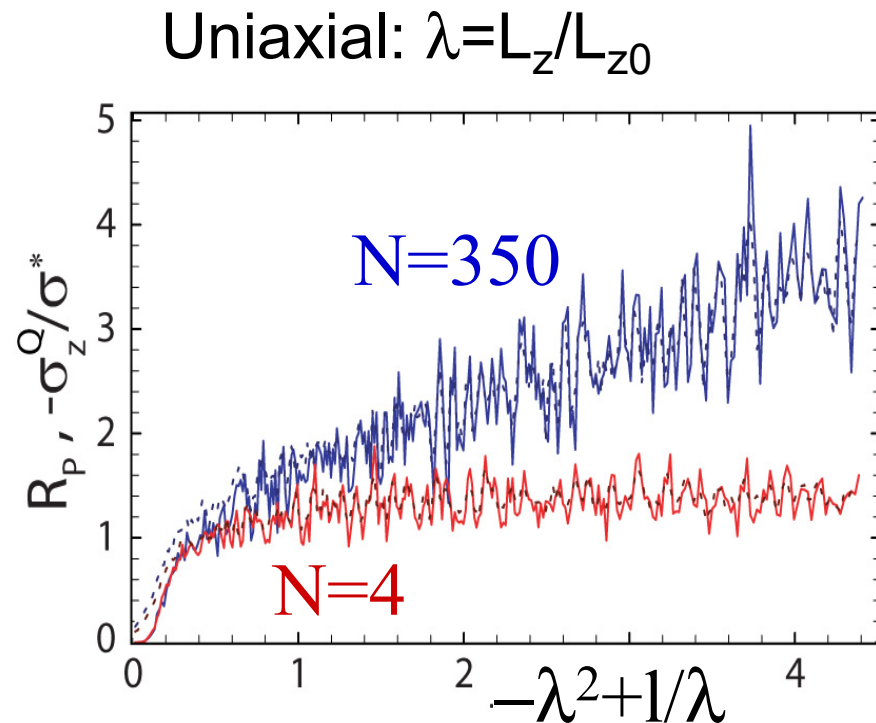
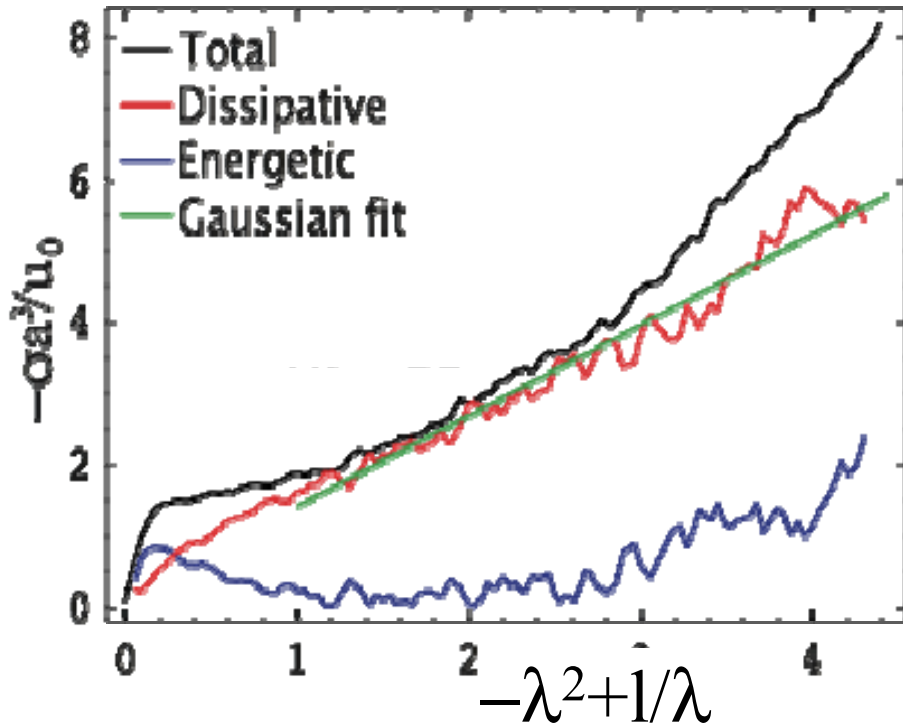
Total stress: $\sigma_{\text{tot}} = -(\partial w / \partial \lambda) = (\partial u / \partial \lambda) - (\partial q / \partial \lambda) = \sigma_U + \sigma_Q$

Find energetic stress strongly dependent on initial conditions

Thermal stress σ_Q strongly correlated with dissipated energy

T=0 direct relation to rate of plasticity $R_p \equiv f / \delta \epsilon$

Fraction f of bonds ($r < 1.5a$) that “break” ($|\Delta r| > 20\%$)
over small strain interval $\delta \epsilon = 0.005$



MR5

Mention experiment

Mark Robbins, 3/7/2007

Main Conclusions

1. Yield criterion provides information about deformation mode
Find pressure-modified von-Mises in experiment and theory
Implies all eigenvalues of pressure-stress tensor matter, not just smallest and largest that define shear plane.
Suggests complex domains with boundaries in all directions
move past each other, not simple plane of slip
2. Plastic rearrangements occur at arbitrarily small strains in the thermodynamic limit.
Observe as bond-breaking, large changes in stress or non-affine displacements, unrecoverable strain after unloading
Rate of plasticity rises rapidly as approach peak stress (yield)
then saturates in steady state

Main Conclusions (cont.)

3. Common view is that stress plays a key role in reducing barriers for plastic flow and enhancing thermal activation
Direct measure of rate and magnitude of local changes shows large stress effect at low temperatures – $T_g/30$
However, near T_g stress has little affect on rate of plasticity
Consistent with observation that yield stress has dropped significantly from intrinsic value set by density and scale of interactions \Rightarrow fluctuations overwhelm $T=0$ barriers
Yield stress drops nearly linearly at each strain rate hitting zero at something like strain-rate dependent T_g
4. Dissipative stress = rate of work – rate of pot. energy rise
scales directly with rate of bond breaking events

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