

Dark Matter Detection using Phonons + Kinetic Inductance Detectors

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Caltech

New Probes for Physics Beyond the Standard Model

KITP

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Overview

Basics of kinetic inductance detectors

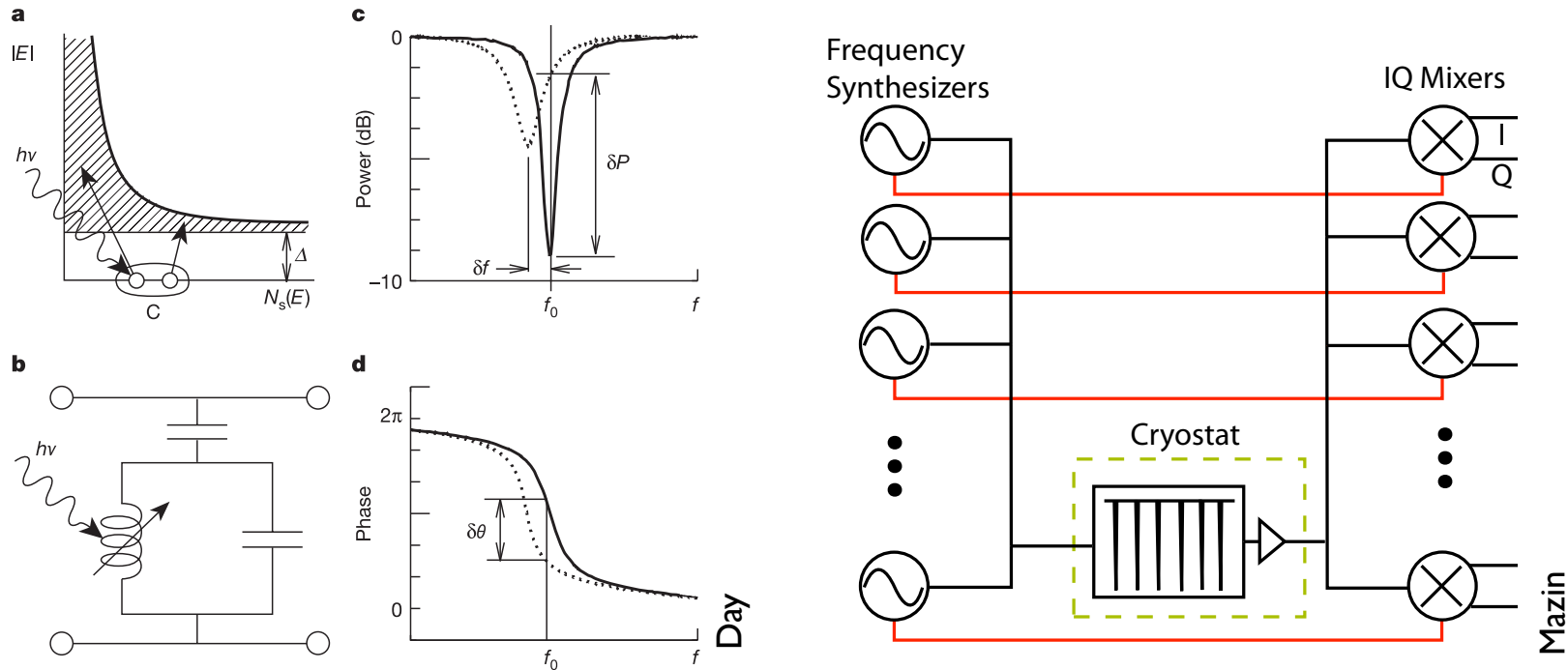
Expected energy resolution

Architectures for different science goals

Progress to date and plans

Readout

Basics of Kinetic Inductance Detectors



Superconductors have an AC inductance due to inertia of Cooper pairs
 alternately, due to magnetic energy stored in screening supercurrent

Changes when Cooper pairs broken by energy, creating quasiparticles (qps)
 Sense the change by monitoring a resonant circuit

Key point: superconductors provide very high Q ($Q_i > 10^7$ achieved), so
 thousands of such resonators can be monitored with a single feedline
 enormous cryogenic multiplex technology relative to existing ones
 very simple cryogenic readout components

Quasiparticles to Conductivity

Conductivity from microscopic BCS theory by Mattis and Bardeen

Use perturbation theory to calculate response of BCS superconductor to EM field
M&B assume extreme anomalous limit, but analysis can also be used for local limit with appropriate modification (see, e.g., Gao thesis Ch 2).

Yields complex conductivity:

$$\frac{\sigma_1}{\sigma_n} = \frac{2}{\hbar\omega} \int_{\Delta}^{\infty} d\epsilon \frac{[f(\epsilon) - f(\epsilon + \hbar\omega)] (\epsilon^2 + \Delta^2 + \hbar\omega\epsilon)}{\sqrt{\epsilon^2 - \Delta^2} \sqrt{(\epsilon + \hbar\omega)^2 - \Delta^2}} \quad \text{resistive}$$
$$\frac{\sigma_2}{\sigma_n} = \frac{1}{\hbar\omega} \int_{\Delta - \hbar\omega}^{\Delta} d\epsilon \frac{[1 - 2f(\epsilon + \hbar\omega)] (\epsilon^2 + \Delta^2 + \hbar\omega\epsilon)}{\sqrt{\Delta^2 - \epsilon^2} \sqrt{(\epsilon + \hbar\omega)^2 - \Delta^2}} \quad \text{reactive}$$

$f(\epsilon) = 1/[e^{\epsilon/k_B T} + 1]$

Two-fluid model: imaginary (reactive) part scales with Cooper pair component, real (resistive) part scales with quasiparticle density

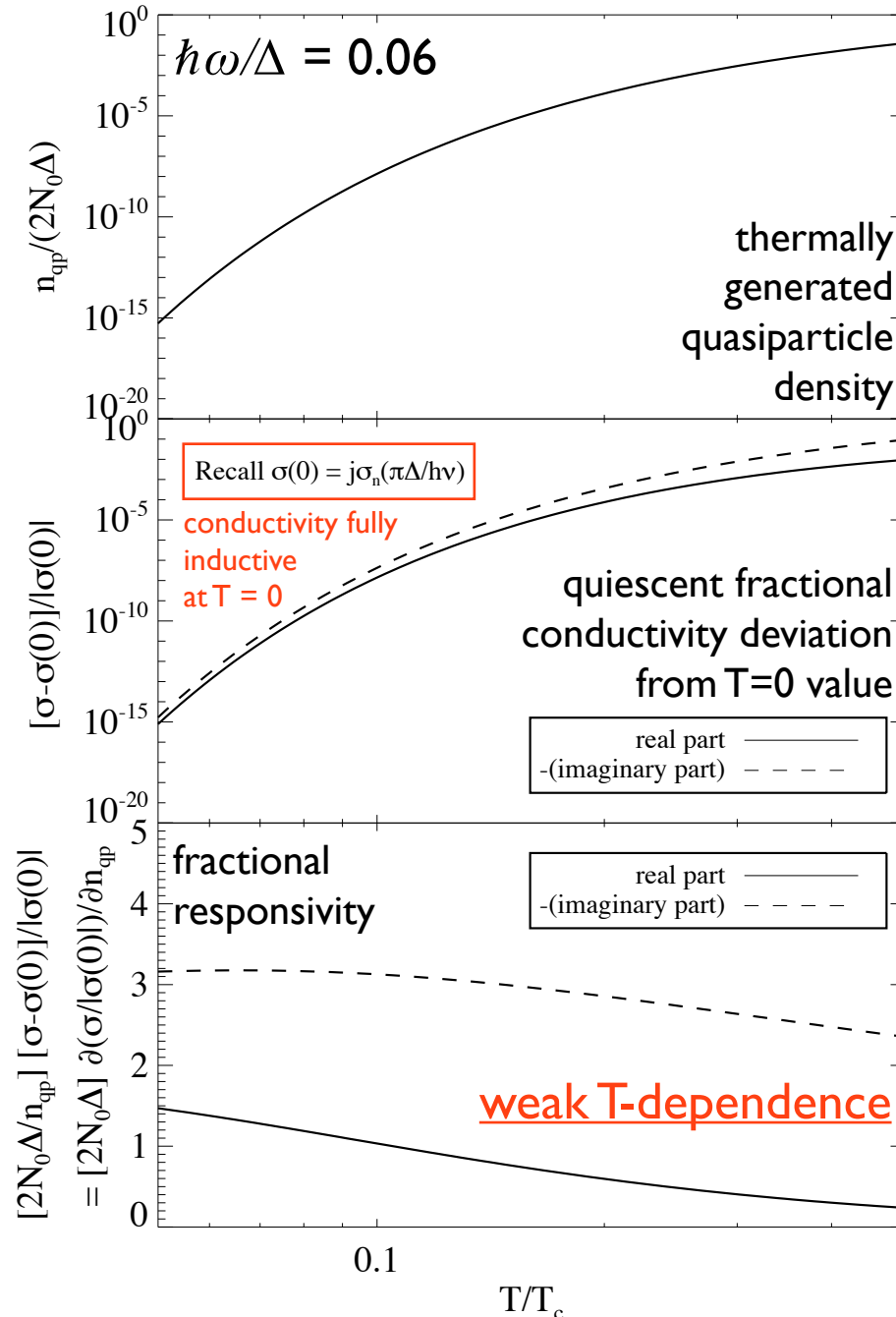
Quasiparticle/Cooper pair population change \Rightarrow conductivity change

T. Klapwijk and others: “engineering” model insufficient due to non-BCS density of states, effects of readout power

For clarity here, stick with engineering model: changes in quasiparticle number completely characterize effect of energy input

Quasiparticles to Conductivity

MB gives characteristic T and $\hbar\omega/\Delta$ dependence



$$\frac{\sigma_1}{|\sigma(0)|} = \frac{4}{\pi} \frac{n_{qp}}{2N_0\Delta} \frac{1}{\sqrt{2\pi\frac{kT}{\Delta}}} \sinh\left(\frac{\hbar\omega}{2kT}\right) K_0\left(\frac{\hbar\omega}{2kT}\right)$$

$$\frac{\sigma_2}{|\sigma(0)|} = 1 - \frac{n_{qp}}{2N_0\Delta} \left[1 + \sqrt{\frac{2\Delta}{\pi kT}} \exp\left(-\frac{\hbar\omega}{2kT}\right) I_0\left(\frac{\hbar\omega}{2kT}\right) \right]$$

$$2N_0\Delta \left. \frac{\partial(\sigma_1/|\sigma(0)|)}{\partial n_{qp}} \right|_T = \frac{2N_0\Delta}{n_{qp}} \frac{\sigma_1}{|\sigma(0)|}$$

$$2N_0\Delta \left. \frac{\partial(\sigma_2/|\sigma(0)|)}{\partial n_{qp}} \right|_T = \frac{2N_0\Delta}{n_{qp}} \frac{\sigma_2 - \sigma_2(0)}{|\sigma(0)|}$$

Key features

Quiescent n_{qp} exponentially suppressed as T decreases*

* as long as no anomalous qp recombination physics

* as long as no anomalous qp creation

Responsivity only weakly T-dependent (not exponential!)

Conductivity to Observables

Observables

Surface impedance is $Z_s = E / H$ for EM wave propagating normal to surface

For thin films (thickness t , therefore local limit; $\gamma = -1$):

$$Z_s = R_s + i X_s \approx \frac{1}{(\sigma_1 - i \sigma_2) t} \quad Z_s \rightarrow i X_s(T=0) = i \omega L_s(T=0) \propto -[\sigma(T=0)]^{-1} = i [\sigma_2(T=0)]^{-1}$$

σ_2 dominates for $T \ll T_c$, so X_s dominates

$$Q_s = X_s(T=0)/R_s = \sigma_2(T=0)/\sigma_1(T)$$

Relate fractional changes in σ to fractional changes in Z_s (thin film limit)

$$\frac{\delta Z_s}{Z_s(T=0)} = \frac{\delta \sigma}{\sigma(T=0)} \quad \frac{\delta L_s}{L_s} = \frac{\delta \sigma_2}{\sigma_2(T=0)} > 0 \quad \frac{\delta R_s}{\omega L_s} = \frac{\delta \sigma_1}{\sigma_2(T=0)} > 0$$

“kinetic impedance”

“kinetic inductance”

“kinetic resistance”

Recall that the fractional conductivity change shows weak temperature dependence.

So, given a measurement of surface impedances in a thin film, we can infer changes in conductivity and thus qp density.

KID Readout and Multiplexing

KIDs response in both reactance and resistance

High Q_s suggests KIDs can be incorporated into high- Q resonant circuits; yields frequency and Q response

High- Q circuits lend themselves to frequency-domain multiplexing

Principle identical to AM/FM radio:
frequency \rightarrow phase (FM),
 $Q \rightarrow$ amplitude (AM)

Don't forget resonator bandwidth!
 $f_{qp} < f_r / 2Q_r$

Ever-growing capabilities in GHz digital electronics:

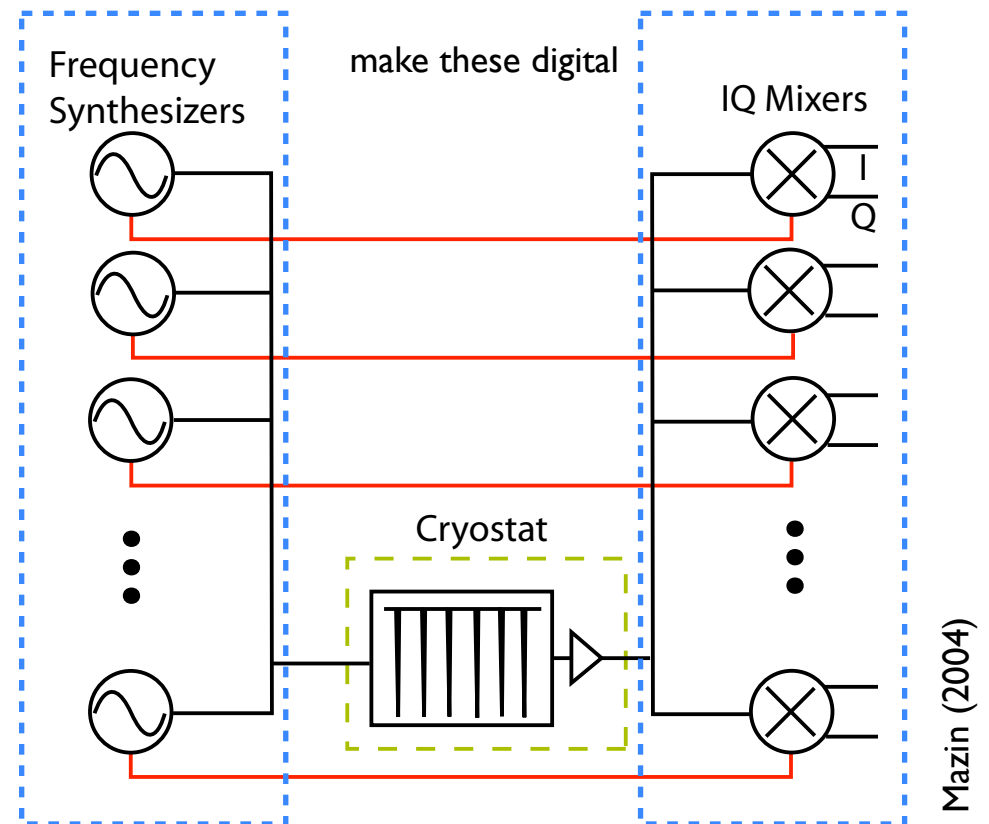
Fully digital generation, reception, and demodulation now possible

$$\frac{1}{Q_{i,qp}} = \frac{R_s}{\omega (L_m + L_s(T=0))} = \alpha \frac{R_s}{\omega L_s(T=0)}$$

kinetic inductance fraction

$$\frac{f_r - f_r(T=0)}{f_r(T=0)} = -\frac{1}{2} \alpha \frac{L_s - L_s(T=0)}{L_s(T=0)}$$

$$\delta S_{21}|_{f=f_r} = \frac{Q_r^2}{Q_c} \left(\delta \frac{1}{Q_{i,qp}} - 2i \frac{\delta f_r}{f_r} \right)$$



Quasiparticle Response to Energy Input

Quasiparticle response governed by quasiparticle lifetime, observed to follow

$$\tau_{qp} = \frac{\tau_{max}}{1 + n_{qp}/n_*}$$

where n_* may be a limiting qp density

Frequently written as

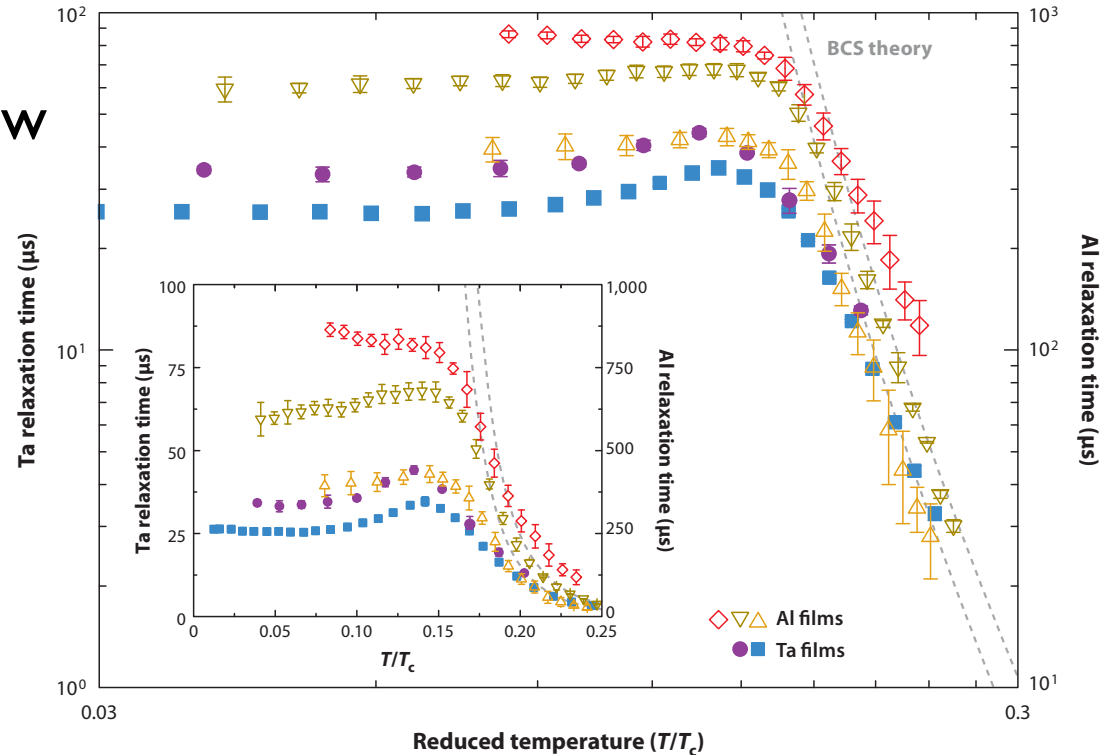
$$\frac{1}{\tau_{qp}} = 2 R n_{qp} + \frac{1}{\tau_{max}}$$

with the recombination constant

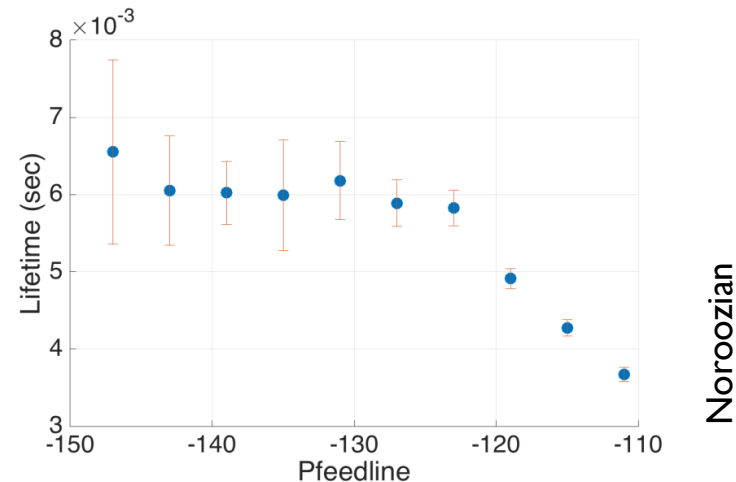
$$R = (2 n_* \tau_{max})^{-1}$$

Many ms lifetimes achievable but perhaps only at low readout powers!

asymptotic regime; limiting excess qp density n_* , or something else? related to disorder? (Barends et al implantation experiment)



Barends et al PRL (2008)
as reproduced in Zmuidzinas, ARCOMP (2012)



Quasiparticle Response to Energy Input

quiescent point (τ_{qp} and n_{qp}) set using g-r equation to balance qp generation by power (readout and stray) and qp decay:

$$\frac{\eta P}{\Delta} = N_{qp} \left(\frac{1}{\tau_{max}} + R \frac{N_{qp}}{V} \right) \quad N_{qp} = n_{qp} V \quad N_* = n_* V$$

$$\implies \tau_{qp} = \frac{\tau_{max}}{\sqrt{1 + 2 (\eta P / \Delta) \tau_{max} / N_*}} \quad \frac{N_{qp}}{N_*} = \sqrt{1 + 2 (\eta P / \Delta) \tau_{max} / N_*} - 1$$

In absence of known power, $\tau_{qp} \rightarrow \tau_{max}$, $N_{qp} \rightarrow N_*$, and $\eta P \rightarrow N_* \Delta / \tau_{max}$

Dynamic response: use dynamic g-r equation to obtain

$$\frac{\delta N_{qp}(f)}{N_{qp}} \propto \frac{1}{1 + 2 \pi i f \tau_{qp}} \frac{\delta P(f)}{P} \frac{1 + N_{qp} / N_*}{1 + N_{qp} / 2 N_*}$$

Calorimetric mode: $\delta P(f) = \delta E$: exponentially decaying pulse response with pulse height $\delta n_{qp} = \eta \delta E / \Delta$ and decay time τ_{qp}

Use relations between δn_{qp} and observables to obtain expected signal

Don't forget resonator bandwidth! $f_{qp} < f_r / 2Q_r$

Noise

$$\text{NEP}_{\text{diss}}^2 = \underbrace{\frac{4\eta_a \chi_{qp} \Delta_0}{\eta_o^2} P_a + \frac{2N_{qp} \Delta_0^2}{\eta_o^2} (\tau_{\text{max}}^{-1} + \tau_{qp}^{-1})}_{\text{generation-recombination noise}} + \frac{8N_{qp}^2 \Delta_0^2}{\eta_o^2 \chi_c \chi_{qp}^2 \tau_{qp}^2} \frac{kT_a}{P_a}$$

amplifier noise temperature

$$\text{NEP}_{\text{freq}}^2 = \underbrace{\text{NEP}_{\text{g-r}}^2}_{\text{generation-recombination noise}} + \underbrace{\frac{8N_{qp}^2 \Delta_0^2}{\beta^2 \eta_o^2 \chi_c \chi_{qp}^2 \tau_{qp}^2} \frac{kT_a}{P_a}}_{\text{amplifier noise}} + \underbrace{\frac{8N_{qp}^2 \Delta_0^2 Q_i^2}{\beta^2 \eta_o^2 \chi_{qp}^2 \tau_{qp}^2} S_{\text{TLS}}}_{\text{two-level system noise}}$$

$P_a = (\chi_c/2) P_g$

readout power stored in resonator feedline readout power

$$\beta = \frac{\delta\sigma_2}{\delta\sigma_1} \quad \begin{array}{l} \text{ratio of imaginary (frequency)} \\ \text{to real (dissipation) response} \end{array}$$

$$\eta_o \quad \begin{array}{l} \text{efficiency for creation of} \\ \text{qps from energy in target} \end{array}$$

$$\eta_a = (\Delta_0/\chi_{qp}) \partial\Gamma/\partial P_a \quad \begin{array}{l} \text{differential efficiency for} \\ \text{creation of qps} \\ \text{from readout power} \end{array}$$

$$\chi_c = \frac{4Q_c Q_i}{(Q_c + Q_i)^2} \leq 1 \quad \begin{array}{l} \text{resonator-feedline} \\ \text{coupling efficiency} \end{array}$$

$$\chi_{qp} = Q_i/Q_{qp} \leq 1$$

quasiparticle quality factor efficiency

qp internal quality factor

total internal quality factor

Generation and recombination noise for qps created by readout
 Amplifier noise reduced by factor β in frequency direction
 TLS noise only in frequency direction

no quasiparticle trapping!

Characteristic Energy Resolution

Assume

delta-function-like energy deposition

qp population determine by readout power generation

dissipation readout (no TLS noise)

amplifier noise dominant over g-r noise ($T \sim 0.1 T_c$ required)

$$\sigma_E = 2\Delta \sqrt{\frac{\eta_a}{\chi_c \chi_{qp}}} \sqrt{\frac{k T_a N_0 V_r}{\left[2N_0 \Delta \frac{\partial(\sigma_1/|\sigma(0)|)}{\partial n_{qp}} \right] Q_s}}$$

normal state single-spin density of states

resonator effective volume (weighted by current²)

= $X_s(T=0)/R_s$
intrinsic surface quality factor of film (generally lower than qp-limited value, 10^5 - 10^7 achievable)

dissipation fractional responsivity; approaches unity for $T \ll T_c$

$$\sigma_E \approx 100 \text{ meV} \left(\frac{2\Delta}{363 \text{ } \mu\text{eV}} \right) \sqrt{\frac{\eta_a}{\chi_c \chi_{qp}}} \sqrt{\frac{T_a}{5 \text{ K}} \frac{V_r}{10^4 (\mu\text{m})^3} \frac{10^6}{Q_s}}$$

BCS aluminum

typical amplifier noise temperature

$1 \text{ mm}^2 \times 10 \text{ nm}$

Architectures

Small detectors (gram-scale)

Goal: detection of sub-eV energies from:

Dark photon absorption

DM-e scattering

Scalar-mediated nucleon scattering at very low recoil energies producing phonons

Methods:

Detection of qp creation in superconducting target via phonons (Hochberg, Zhao, Zurek, arXiv:1504.07237)

qp propagation diffusive, subject to pair recomb.

phonons quasiballistic, long decay times

Detection of optical phonon production in polar materials:

GaAs (Knapen, Lin, Pyle, Zurek, arXiv:1712.06598)

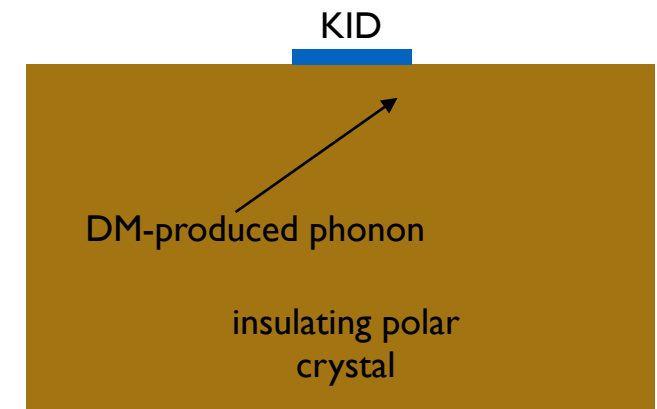
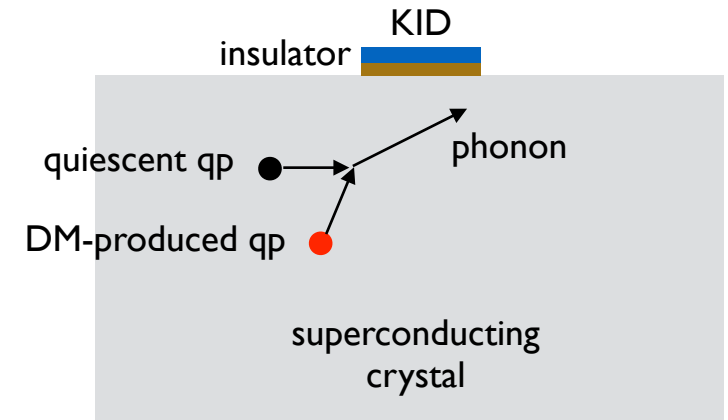
Al₂O₃ (Knapen talk (Tues))

Architecture:

single mm-scale KID on few-mm target substrate

previous slide energy estimate ~ valid

Need lower-gap superconductor for KID (e.g., AlMn) or better amplifiers (kinetic inductance parametric amplifier recently demo'd $T_a \sim 70$ mK at 3 GHz)



no quasiparticle trapping!

Architectures

Large detectors (kg-scale)

Goal:

traditional nuclear recoil search at very low recoil energies (10 eV_r)

DM-e scattering at eV scales

Method:

Neganov-Luke-Trofimov phonon production by drifting e-h pairs in large electric field (Romani et al APL 112, 043501 (2018)) providing single e-h pair detection

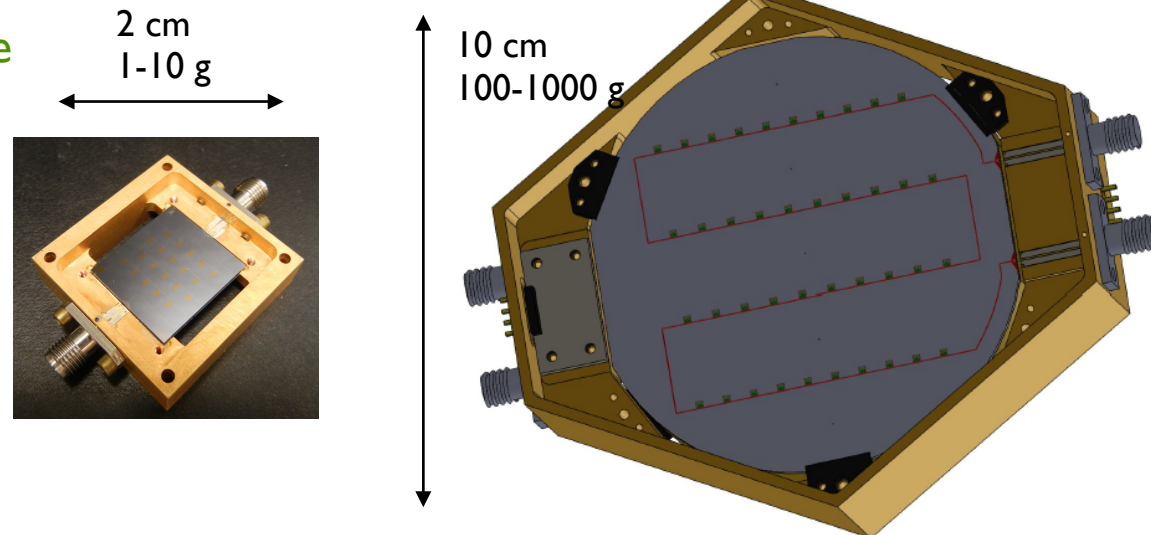
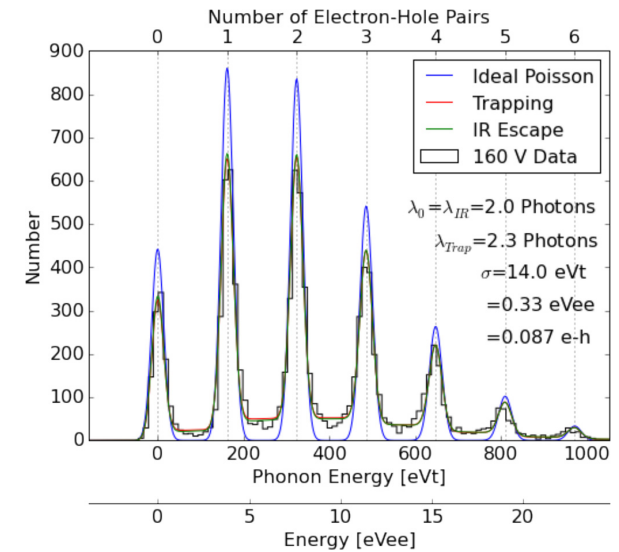
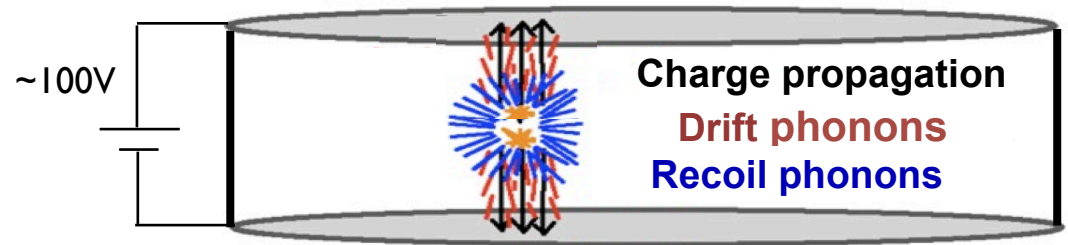
Architecture:

few KIDs on cm-scale substrate

~100 KIDs on 10-cm-scale substrate

Fine pixellization intended to provide fiducialization away from detector surfaces (most low-energy bg)

Also provide pos'n correction for energy



no quasiparticle trapping!

Large Detector Energy Resolution

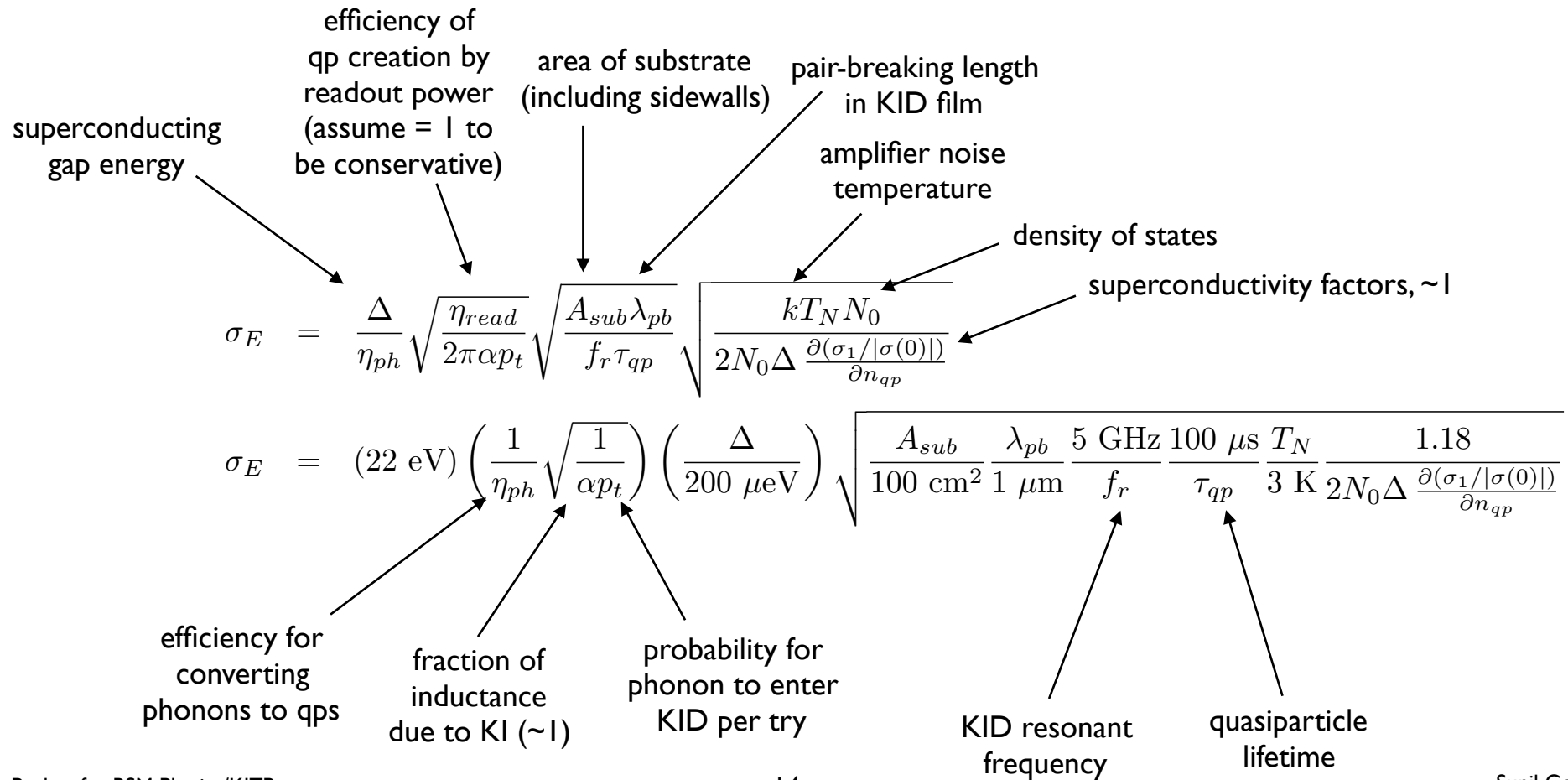
Assume:

readout noise dominates ($T \ll T_c$ ensures g-r noise subdominant)

qp density determined by readout power generation

resonator is coupling dominated ($Q_c \ll Q_i$)

quasiparticle lifetime in KID \ll phonon absorption timescale ($\tau_{qp} \ll \tau_{abs}$)



no quasiparticle trapping!

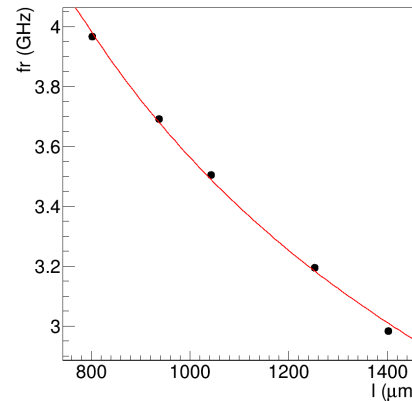
KID Design

10-30 nm thick film

Inductor

Symmetric coplanar strip design
minimizes dipole crosstalk while
maintaining >95% current
density uniformity

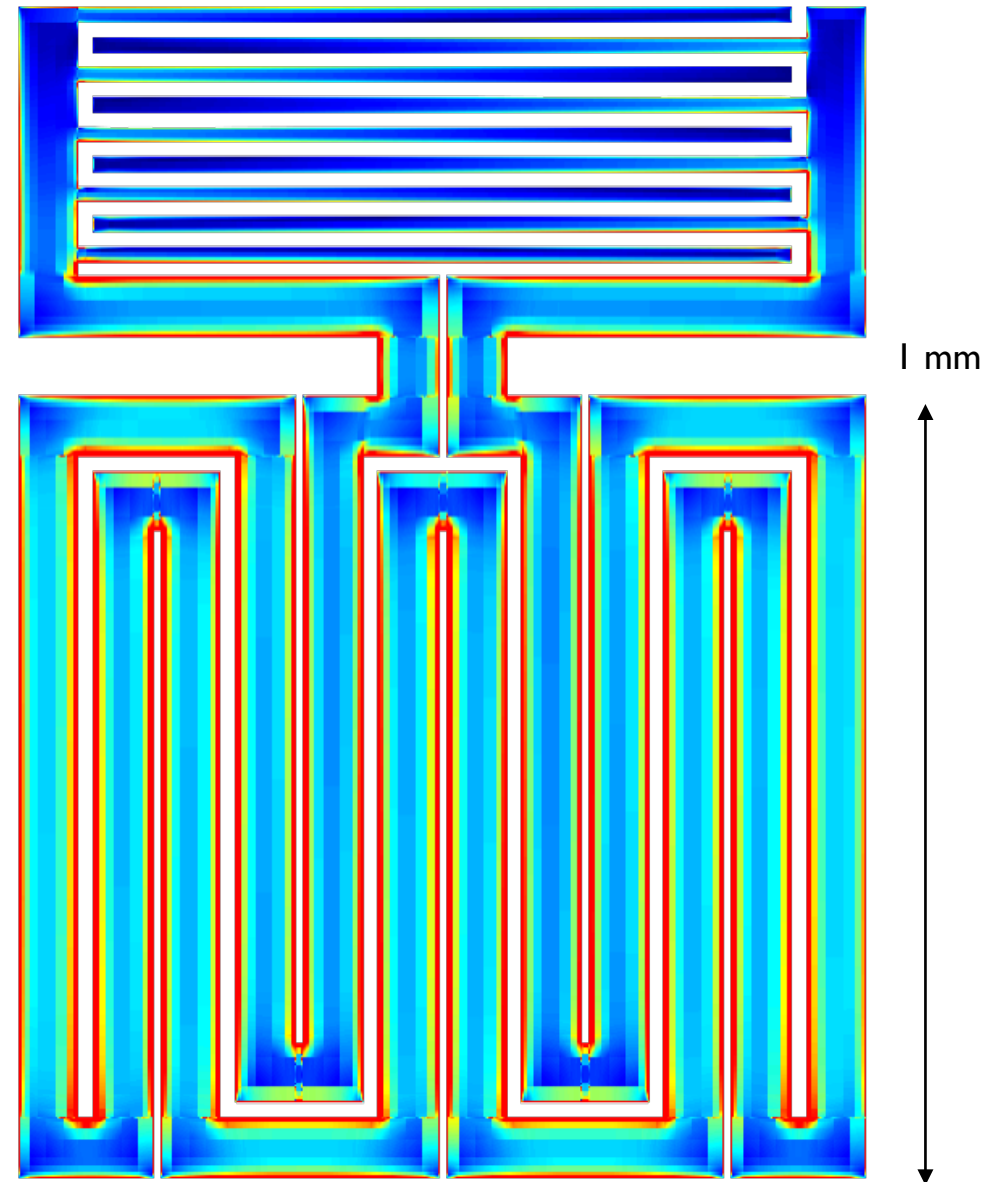
Frequency tuning
is done by
adjusting
inductor length
 $\sim 10^4 (\mu\text{m})^3$ active
volume



Capacitor

Standard interdigitated capacitor to
minimize TLS noise

Can be made out of Nb in long run
to avoid absorbing phonons



no quasiparticle trapping!

Full Wafer Design

Feedline: 300 nm Nb coplanar waveguide

Thick feedline ensures reliable fab, good transmission

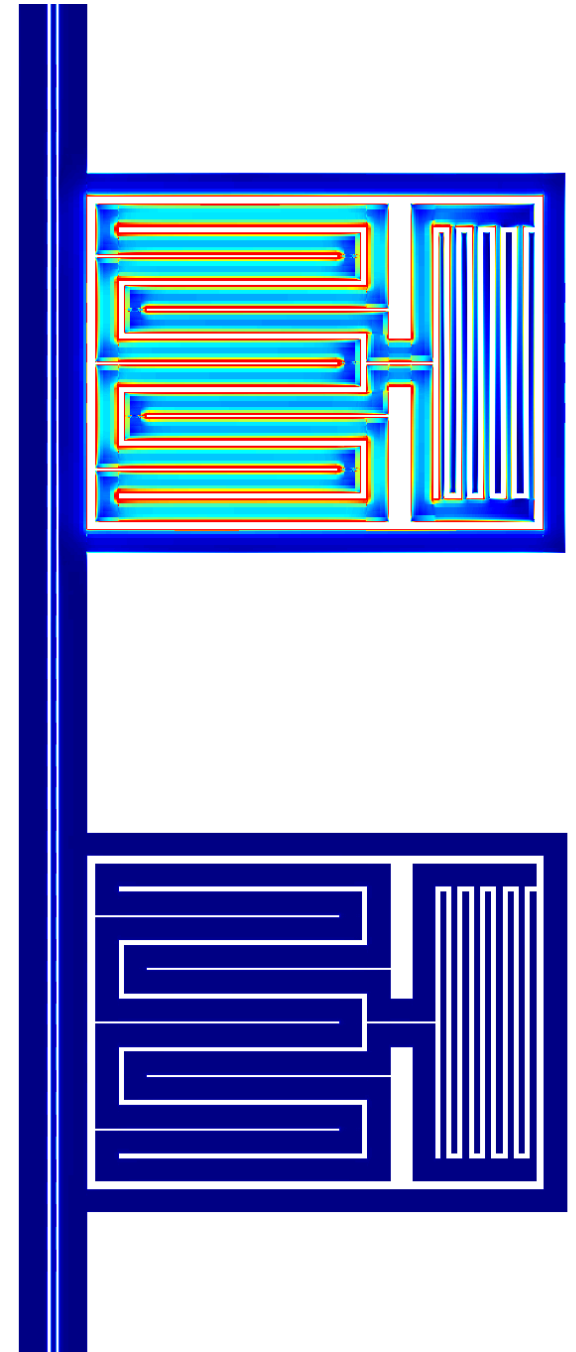
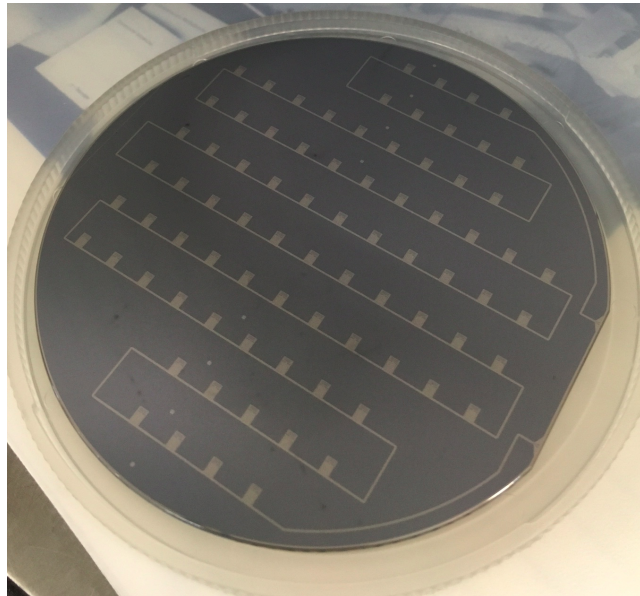
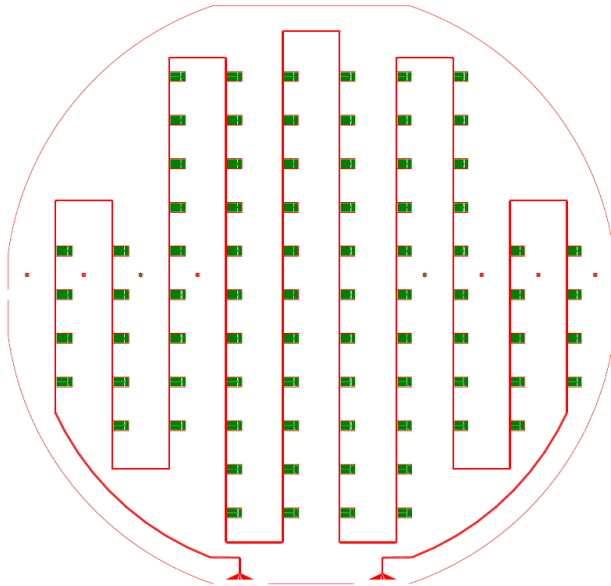
Crosstalk minimized

Using the specialized inductor design with ground shield (a la CALDER) see negligible crosstalk in simulation

Critical for ensure frequency predictability

Full wafer fab via contact mask

Large features ($10\ \mu\text{m}$)



RF Performance

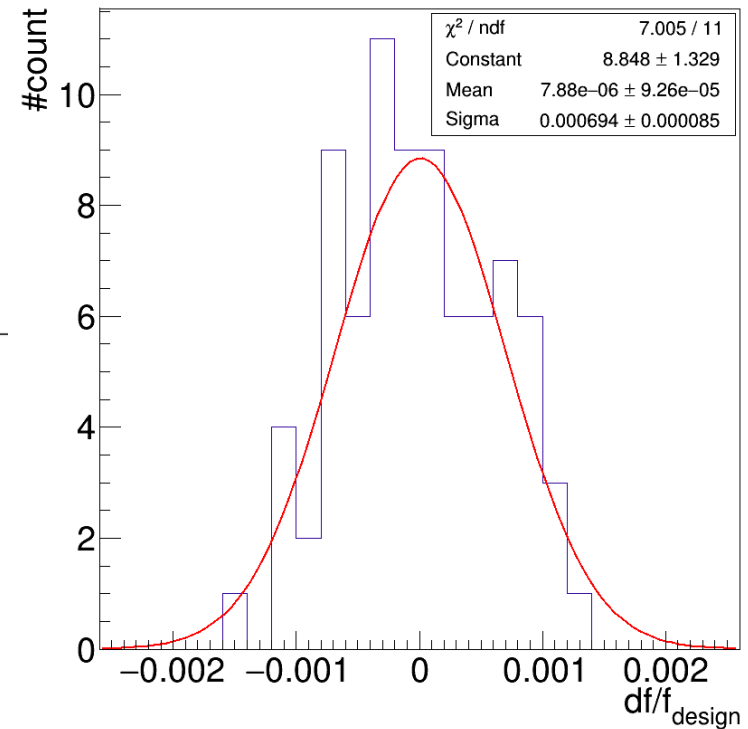
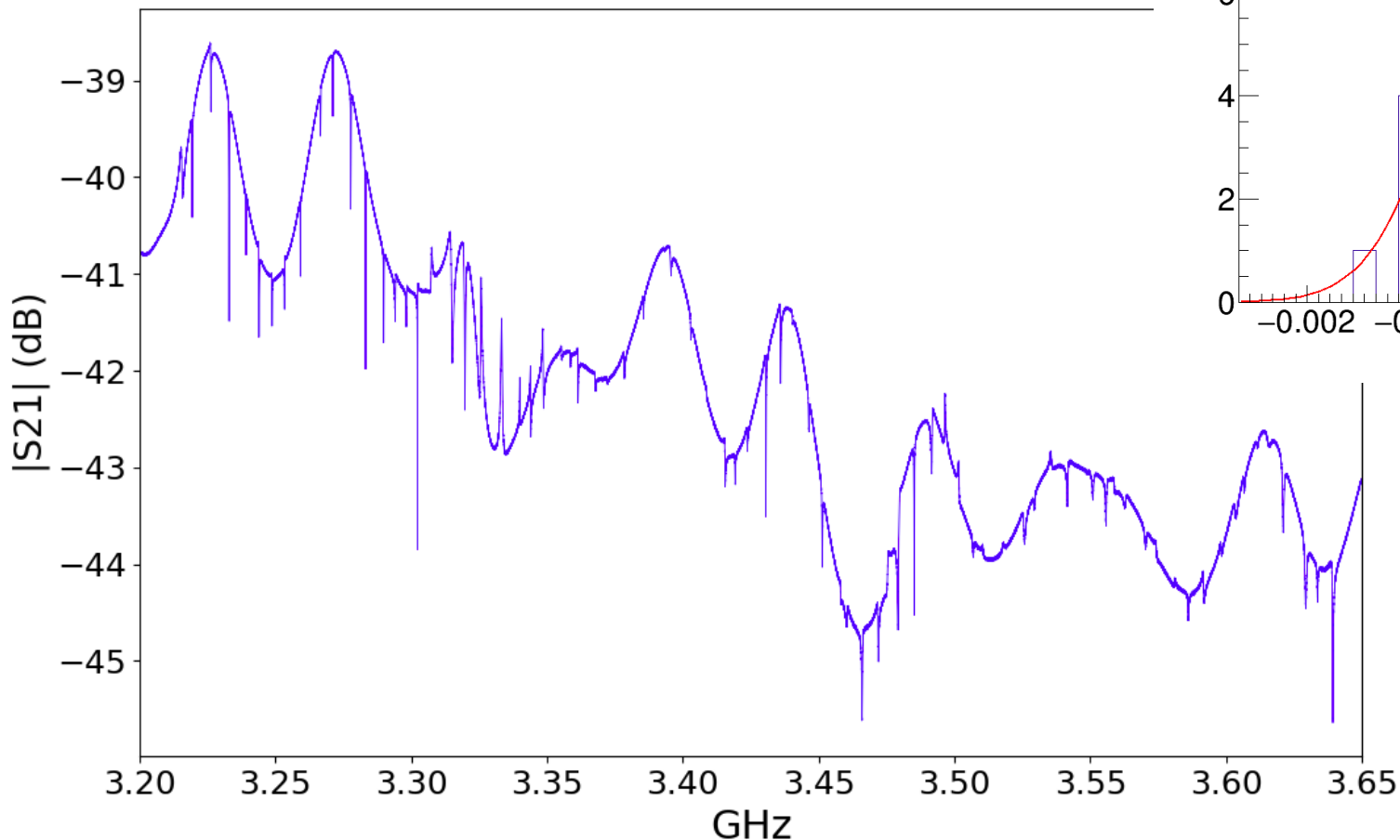
Fabricate a Nb-only device to test RF simulations

Excellent performance!

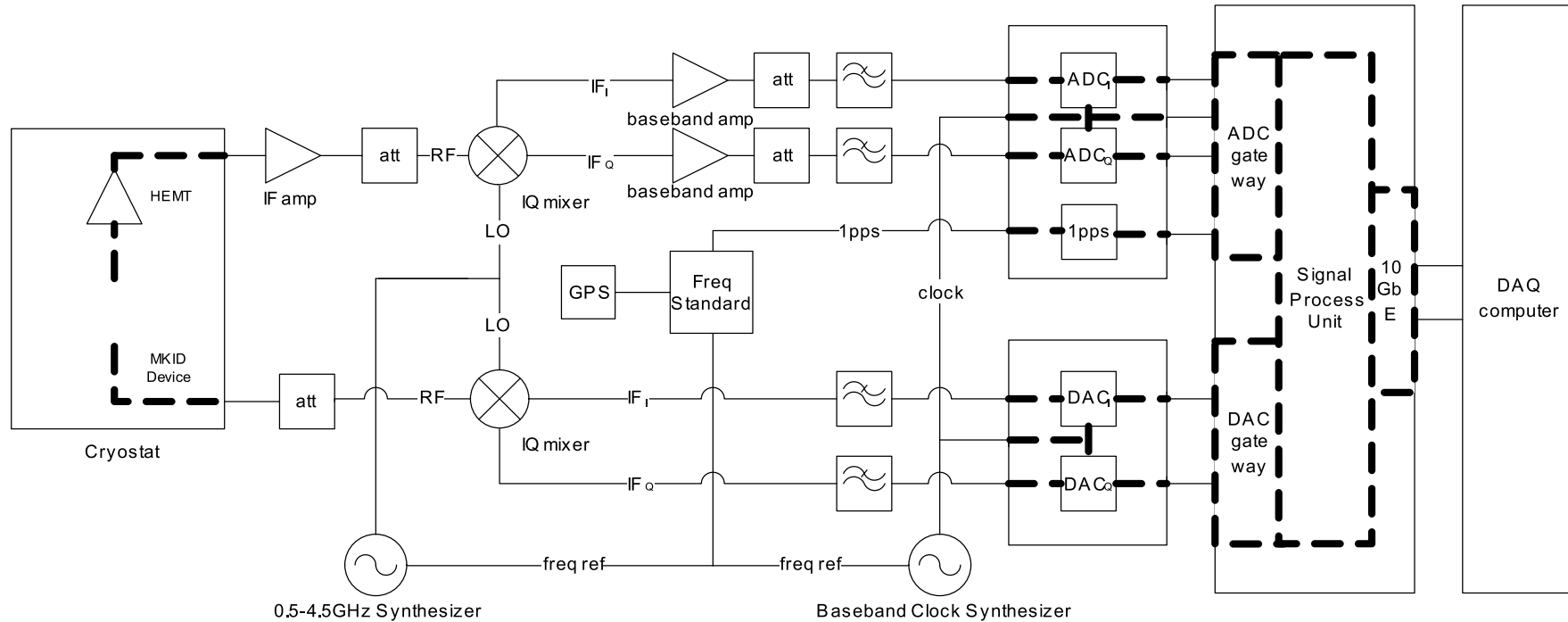
Detected almost all 80 resonances

Scatter = 7×10^{-4} fractional = 2.5 MHz

No exchanged resonances, no collisions!



Multiplexed Readout



UCSB/Caltech/JPL + partners have developed digital readout

Signal generation and demodulation done digitally

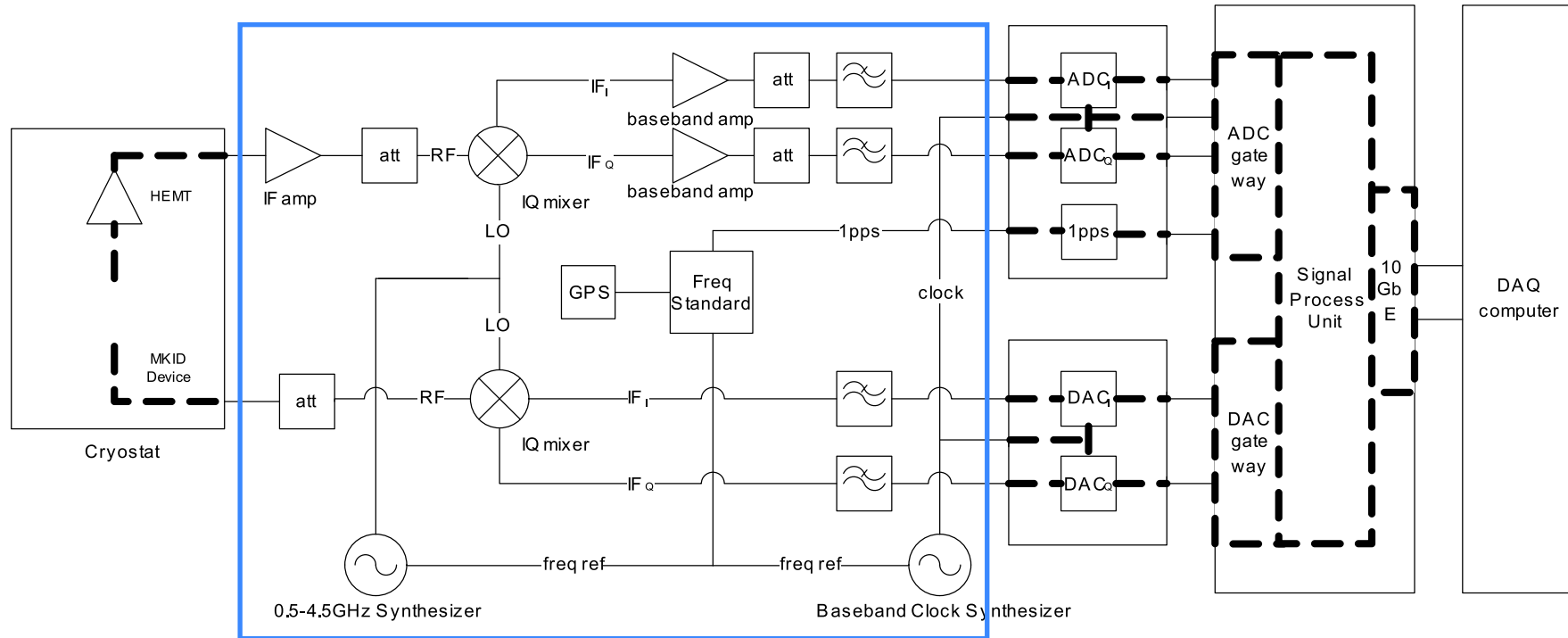
IF system block upconverts from DAC/ADC baseband (0-500 MHz) to resonator RF band (3 GHz)

Critical issues:

ADC SNR: need 12 bits @ 500 MHz to ensure readout white noise ok

1/f: for bolometric instruments, need stability down to 0.01-0.1 Hz

Multiplexed Readout



IF (intermediate frequency) board:

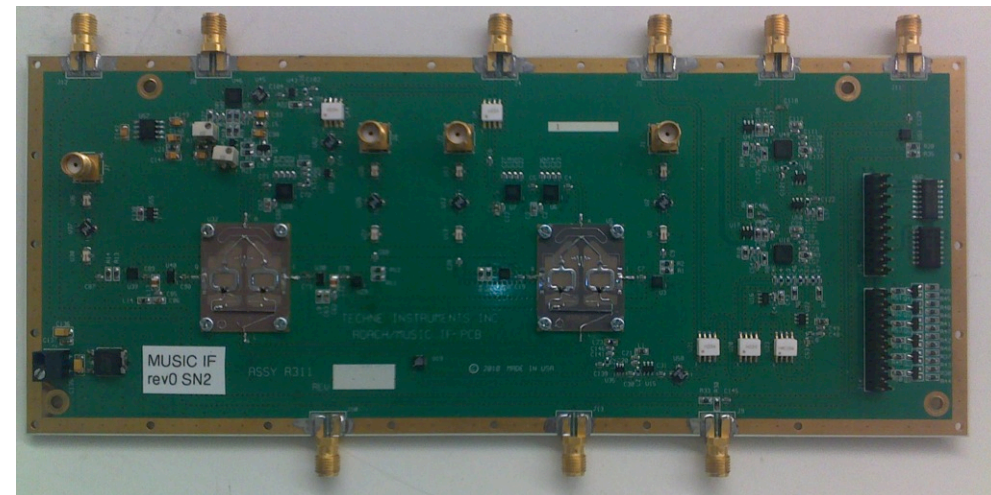
Freq synth to generate local osc. locked to GPS-referenced 10 MHz Rb freq std

Analog IQ mixers to up- and down-convert w/double-sideband recovery

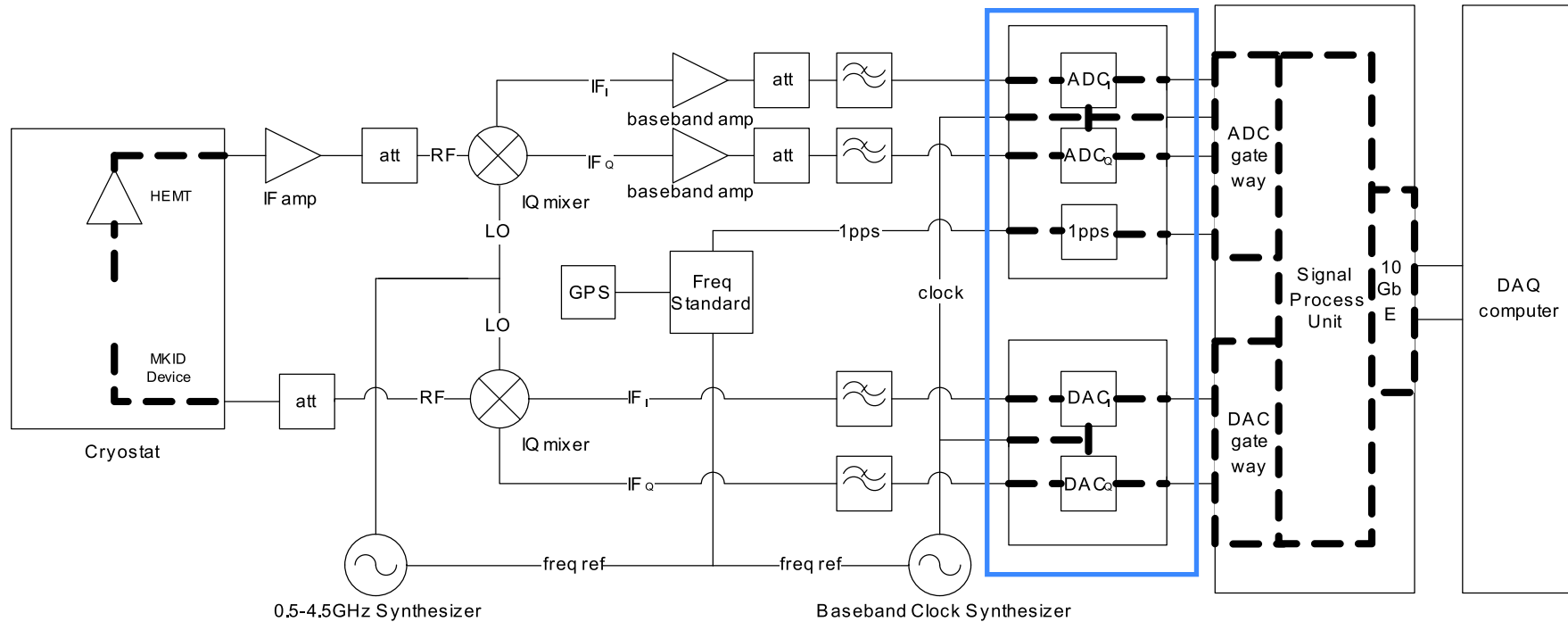
Anti-alias filtering

Gain/atten. to match to DAC/ADC ranges

Great care taken with heatsinking for I/f



Multiplexed Readout



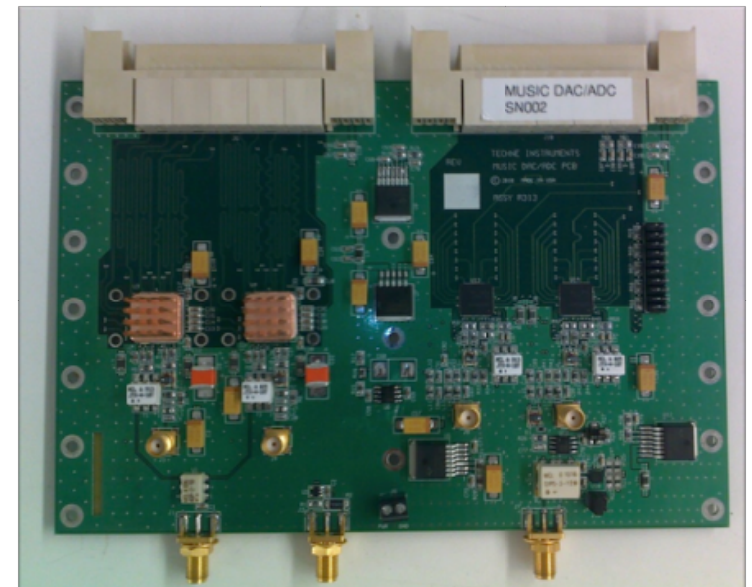
ADC/DAC board:

12-bit 550 MHz ADC (TI ADS5463)

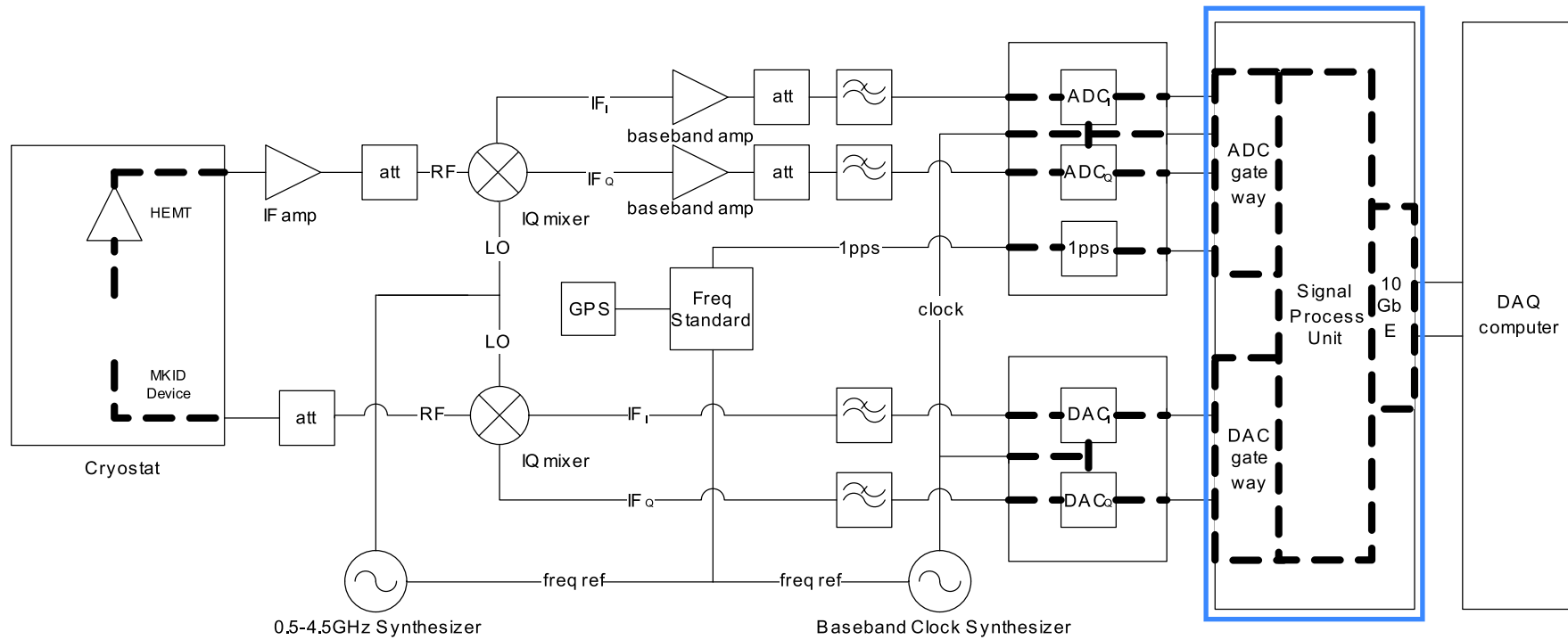
16-bit 1000 MHz DAC (TI DAC5681)

Common voltage reference, extensive heat-sinking to minimize I/f

Mates to ROACH FPGA/PowerPC platform



Multiplexed Readout



ROACH board

FPGA + CPU + memory

Simulink FPGA programming

System built on ROACH1/Virtex5

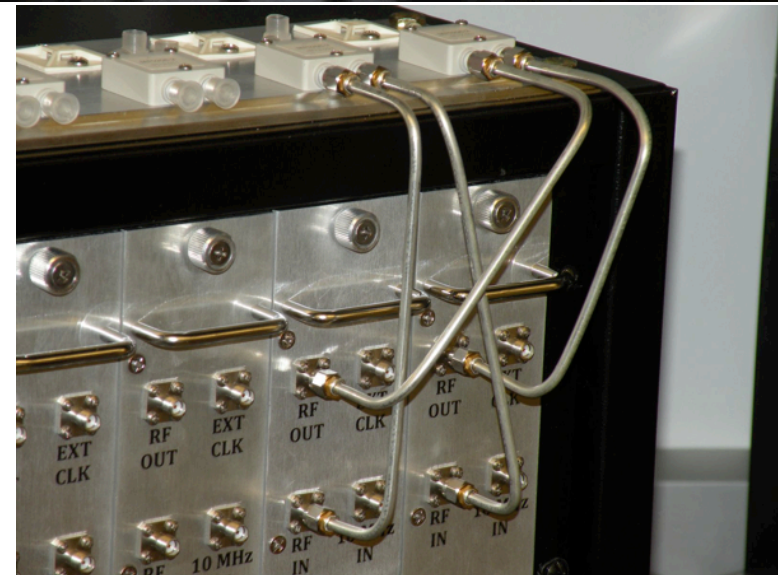
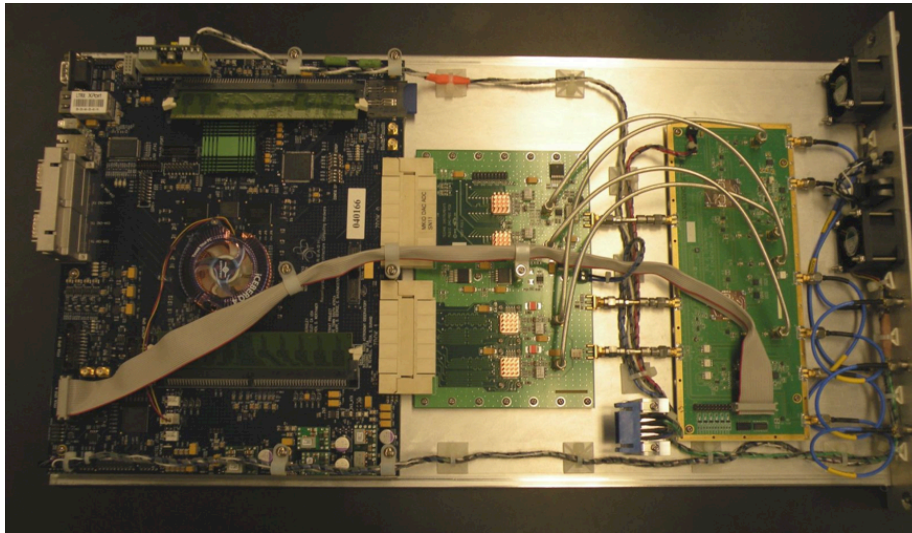
UCSB has developed 256-ch digital
downconverter (multiplier) firmware

ROACH2 based on Virtex6 now standard
(firmware ported by UCSB)



Multiplexed Readout

8-block crate developed; high-stability PSU for IF, ADC/DAC



New Readout Option

ROACH system good for mid-scale instrument deployment

Optimized firmware and data transport
 → max channel count, min cost/channel

ROACH system not good for lab development

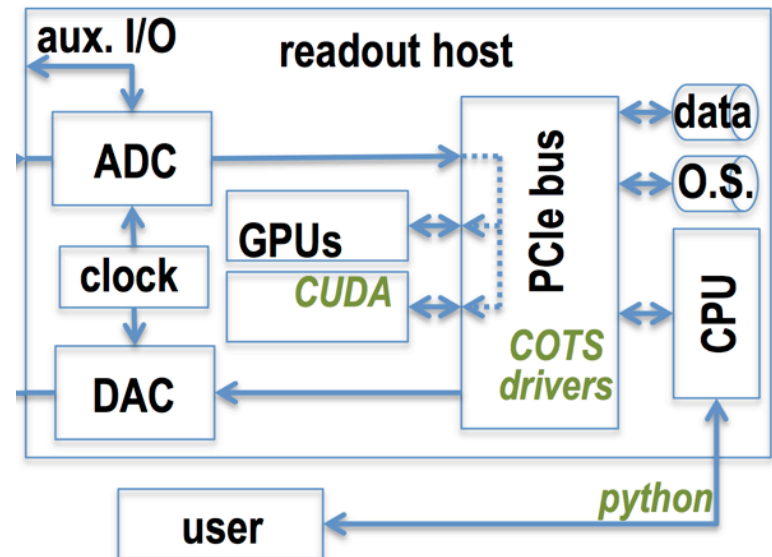
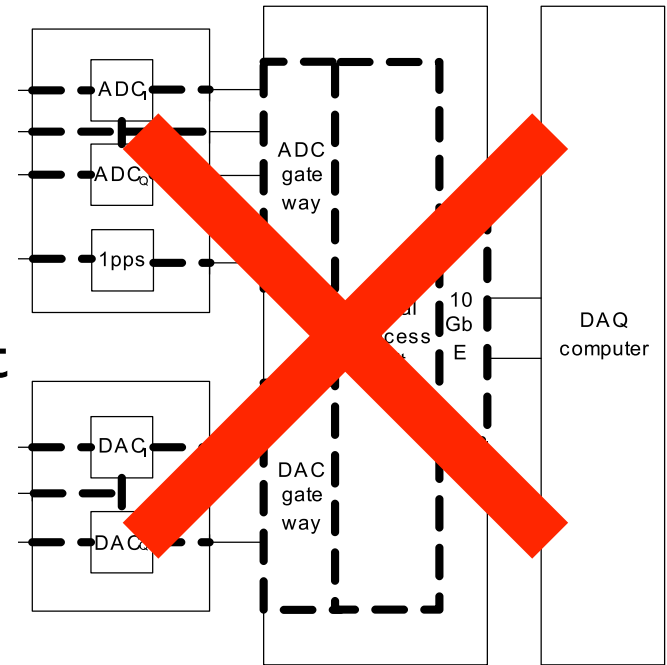
Special-purpose hardware (even ROACH)
 Changes to multiplexing algorithm require firmware changes

Multiple layers of software/firmware

- Firmware for FPGA
- Linux system for PowerPC
- Linux system for DAQ computer

JPL developing GPU-based system programmable in C++ and Python

Commercial off-the-shelf hardware
 Flexible multiplexing algorithms
 Easier user interface



O'Brient/Dowell/Steinbach

Plans

Near-term

Have device with Al KID films in hand

Characterize at sub-Kelvin temperatures

RF performance, kinetic inductance fraction

expose to ^{55}Fe and ^{129}I x-rays to measure energy resolution, do position reconstruction and energy correction

Mid-term

Refine design

Scale up to thick (100 g Si) substrates

Long-term

Revisit design with focus on single-resonator energy resolution for sub-eV depositions