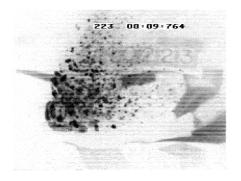
Fragmentation of Planetesimals

Ongoing Work on Planetesimal Coagulation (in collaboration with S.Ida, Tokyo, Japan)

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Characteristics of a Collision

- ullet Mass of the largest fragment M_L , or dimensionless: $f_l=rac{M_L}{M}.$
- Technical terms: $f_l < \frac{1}{2}$: Fragmentation, otherwise: Cratering.

 The case $f_l = \frac{1}{2}$ refers to critical fragmentation.
- Energy/Volume S which yields $f_l=\frac{1}{2}$ (without reaccumulation). This is called *Impact strength*.
- $f_{\rm KE}:=2E_{\rm kin}^{\rm frag}/E_{\rm kin}$: Fraction of the impact energy that is converted into the kinetic energy of the fragments.

Fragment size distribution:

- $N_m(m)$: Number of all fragments with a mass $m_i > m$.
- $N_D(D)$: Number of all fragments with a diameter $D_i \geq D$. If all fragment masses m_i are sorted in decreasing order, starting with i = 1, then $N_m(m_i) = i$ holds.
- ullet Velocity distribution N(v): Number of all Fragments with $v_i \geq v$.

Experimental Results

ullet Impact strength S:

$$S = S_0 \left(\frac{R}{1\text{m}}\right)^{-0.24} (1 + 1.6612 \times 10^{-7} \left(\frac{R}{1\text{m}}\right)^{1.89})$$

$$S_0 = 1.726 \times 10^6 \text{ Jm}^{-3}$$

(House and Holsapple 1990)

• Largest fragment :

$$M_L = M - lpha_m E_{ ext{kin}} \quad ext{for } (M - M_L) \ll M$$
 $M_L = rac{1}{2} M \left(rac{
ho E_{ ext{kin}}}{2SM}
ight)^{-K} \quad ext{for } M_L \leq rac{1}{2} M$

Reasonable choice: K = 1.24 (Fujiwara et al. 1977)

• Common fragment size distribution :

$$N(\geq m) = \left\{ egin{array}{ll} c \, m^{-b} & {
m for} & m \leq M_L \\ 0 & {
m otherwise}. \end{array} \right.$$

Conditions to determine c and b:

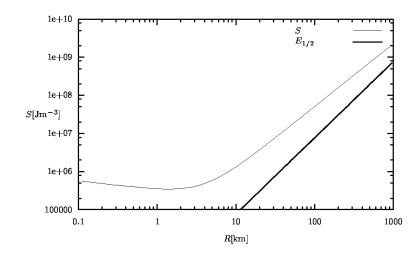
$$M = \int_0^{M_L} \left| \frac{\mathrm{d}N(x)}{\mathrm{d}x} \right| x dx$$
 $N(M_L) = 1$

• Energy partition coefficient:

$$f_{
m KE} = 2 rac{E_{
m kin}^{
m frag}}{E_{
m kin}} pprox 0.01$$
 for lab experiments.

• Velocity distribution:

$$< v>_m = V_0 \left(\frac{m}{M}\right)^{-k}$$



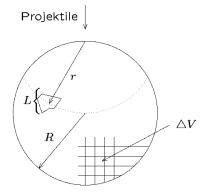
The impact strength used in this work. As a comparison the minimal energy $E_{1/2}$ is given, which is necessary to remove one half of the target mass (solely due to gravitation).

Semiempirical Fragmentation Model

- ullet It is not a calculation based on first principles (like SPH) \to the model needs to be gauged with experiments and/or more sophisticated simulations.
- Can be easily adapted to new parameters within the limits of this model.
- Fast calculation allows for the scanning of a large parameter space.

The model is derived from the observation, that fragment size increases with increasing distance to the impact site.

$$L(r) = CR\left(\frac{r}{R}\right)^n , C > 0 , n > 0$$

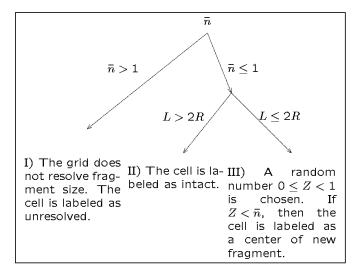


Numerical Decomposition

The mean number of fragments in a subvolume ΔV is:

$$\bar{n}(r) = \frac{\Delta V}{L(r)^3}$$

Each grid cell is subject to a case distinction:



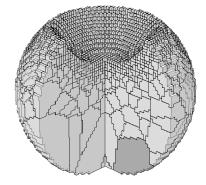
Non-labeled cells are assigned to the nearest center (Voronoi-Decomposition).

Integration of Physics:

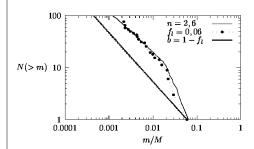
- **Input**: Radius R, Density ρ , Impact strength S(R), kinetic energy of the projectil E_{kin} and f_{KE} .
- The exponent n is regarded as a material property. (arises from comparison with experimental results)
- The parameter C depends solely on f_l for a fixed material: $C = f(f_l, n)$.
- \bullet f_l is calculated as follows:

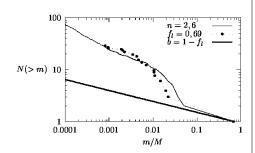
$$\epsilon := rac{
ho E_{
m kin}}{2SM} \ f_l(\epsilon) = \left\{ egin{array}{ll} 1 - rac{1}{2}\epsilon & {
m for} & \epsilon < 1 \ rac{1}{2}\epsilon^{-K} & {
m otherwise}. \end{array}
ight.$$

• Use f_{KE} to calculate E_{kin}^{frag} .



Section for $f_l=0.04$ and n=3. In this calculation $60\times60\times60$ grid cells were used.





Lab experiments with $f_l=0.06$ (left) and $f_l=0.69$ (right). The data is represented by a dotted line with black dots, the new model by a thin line. The thick line represents a simple power law.

(Data from Davis and Ryan 1990)

Velocity Distribution Models

- Direction: The velocity vectors point radially outwards in all models.
- Modulus:
 - 1. All Fragments have the same velocity $v_i = v_0$.
 - 2. Each Fragment has $v_i = C_v m_i^{-1/6}$. Fragments of the same mass have the same velocity.
 - 3. The fragment velocities are derived from a maxwell distribution. The mean square velocity is $v_0^2 \propto \left(m_i^{-k}\right)^2$.

$$p(v, v_0) = \frac{6\sqrt{3}}{\sqrt{2\pi}} \frac{v^2}{v_0^3} \exp(-\frac{3}{2} \frac{v^2}{v_0^2})$$

4. The fragment velocities are superimposed with a scatter of the form: $v_i = v_i^0(1 + R_v)$. R_v is gaussian distributed with a fixed dispersion 0.25 for all fragments.

$$p(x,\sigma) = \frac{1}{\sqrt{2\pi}\sigma} \exp(-\frac{x^2}{2\sigma^2})$$

If necessary, the velocities are rescaled to obtain the desired total kinetic energy $E_{\rm kin}^{\rm frag}$.

Numerical Integration

Equations of motion:

$$\frac{d^2\vec{x}_i}{dt^2} = \sum_{j \neq i} \frac{Gm_j(\vec{x}_j - \vec{x}_i)}{|\vec{x}_j - \vec{x}_i|^3}$$
 Sumation over j

Integrator: Second order Leapfrog-Method.

Collisions

- Fragments are regarded as spheres.
- Rotation of the fragments is neglected.
- No further fragmentation due to secondary collisions.
- The restitution parameter is $\alpha = 0.8$

Analysis

After the calculation all gravitationally bound fragments are merged into a "rubble pile". In the case of two bound fragments orbital parameters corresponding to an unperturbed keplerian orbit are calculated.

Ongoing Work on the Formation of protoplanets

Integrator: Nbody6++ with Hermite Scheme

Hermite Iteration

First step: Particle prediction:

$$x_p = x_0 + v_0 \Delta t + \frac{1}{2} a_0 (\Delta t)^2 + \frac{1}{6} \dot{a_0} (\Delta t)^3$$

$$v_p = v_0 + a_0 \Delta t + \frac{1}{2} \dot{a_0} (\Delta t)^2$$

Hermite Step:

$$v_c = v_0 + \frac{1}{2}(a_p + a_0)\Delta t - \frac{1}{12}(\dot{a_p} - \dot{a_0})(\Delta t)^2$$

$$x_c = x_0 + \frac{1}{2}(v_c + v_0)\Delta t - \frac{1}{12}(a_p - a_0)(\Delta t)^2$$

The iteration is achieved by recalculating $a_p, \dot{a_p}$ with x_c, v_c . Two iterations are sufficient in practice.

Additional Features of NBody6:

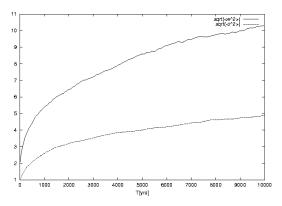
- Neighbor Scheme: Split force in irregular component (near neighbors) and regular component (distant particles and central force)
- $\bullet~$ KS (Kustaanheimo-Stiefel) Integration of close encounters.

Feasible is: (assuming an elapsed time of one week and 10,000 Orbits)

Hardware	Code	N
One GRAPE-6	NBODY4	70.000
GRAPE-6 (B) in Hydra-Cluster (ARI)	NBODY6++	300.000
Cray T3E - 10 Processors	NBODY6++	22.000
Cray T3E - 50 Processors	NBODY6++	50.000
Cray T3E - 100 Processors	NBODY6++	71.000
Cray T3E/512	NBODY6++	160.000

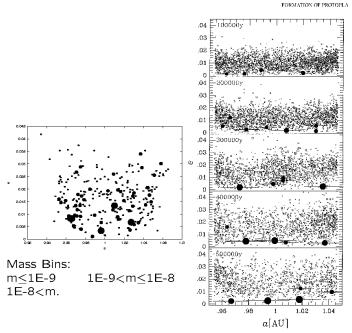
Direct simulation of planetesimals in a narrow ring (1 ± 0.04 AU).

Testing the Code



1000 collisionless particles, ,< a>=1 AU, $\Delta a=0.07$ AU, $\Sigma=10\frac{9}{\rm cm^2}.$ e,i in units of $\frac{r_{\rm HIII}}{< a>}$.

Including Collisions with F = 10.



(Kokubo & Ida 2000)

Including Collisions with F = 10.

