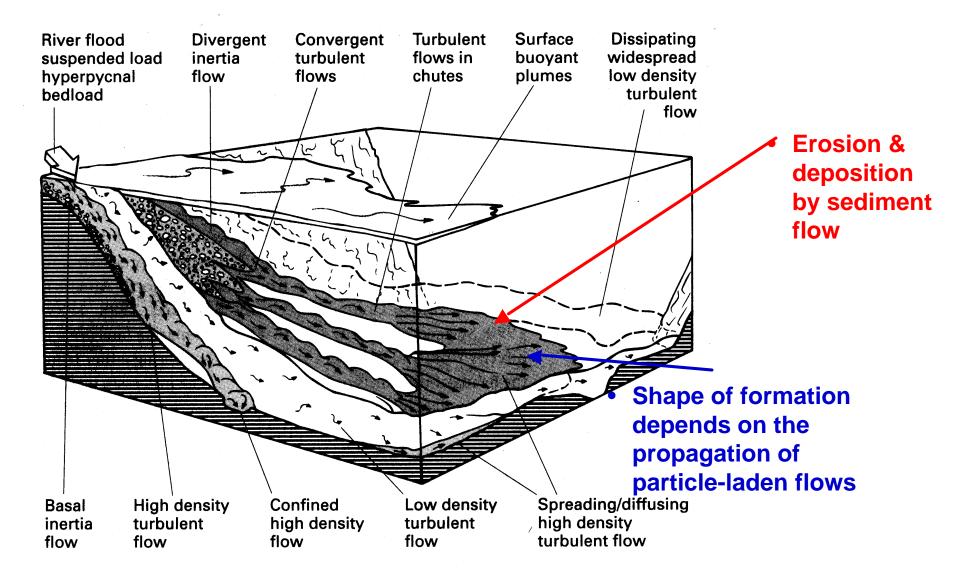
# Gravitational Transport of Grains

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ExxonMobil: Thomas Halsey Sandia National Labs: Gary Grest Leo Silbert (now at Chicago) James Landry (now at BAE) Steven Plimpton

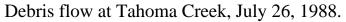
June 20, 2005 Granular Physics Conference KITP, Santa Barbara, CA

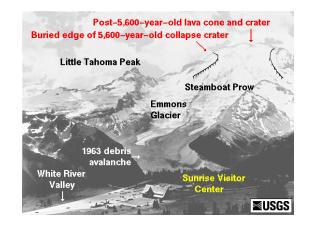
#### Formation of Off-Shore Reservoirs from Sediments

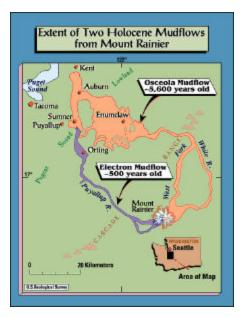


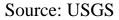
# **Debris Flows - Mt. Rainier**







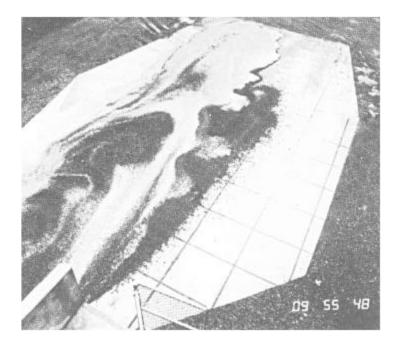




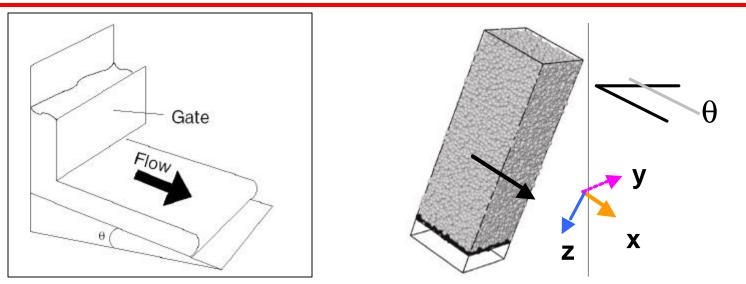
#### **Debris Flow Flume**



 R.M. Iverson, J.E. Costa, and R.G. LaHusen, 1992,
 H.J. Andrews Experimental Forest, Oregon: USGS

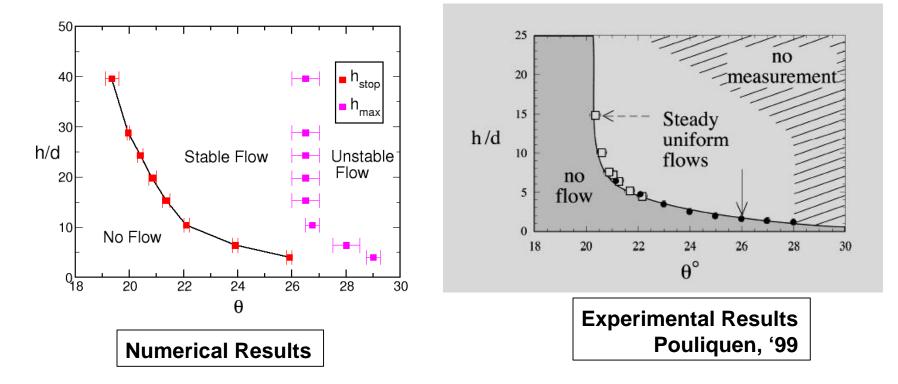


# **Chute Flow**



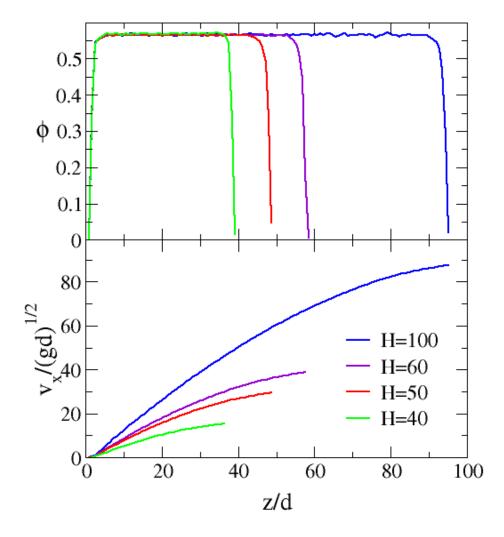
- Study chute flow -- flow of a dry granular medium down an inclined plane
- Fundamental geometry for geophysical applications
  - Debris flows
- Concentrate mainly on three dimensions
  - Two-dimensional variation of parameters
  - In 2-d, crystallization creates significant hysteresis, boundary effects

## Phase Diagram for Flow



- Phase diagram shows three regions:
  - No flow
  - Stable flow
  - Accelerating (unstable) flow
- For h large, angle of repose is ~19.5°

### **Kinematics of Chute Flow**



- Constant density profile
  observed with depth
  - Density drops near surface
- Velocity obeys 3/2 power law with depth
  - Best fit to power law with exponent of 1.52
  - Agrees with Bagnold scaling (next slide)
- Other kinematic variables also suggest inverse strain rate as only apparent time scale
- Normal stresses in shear plane approximately equal

$$\boldsymbol{S}_{xx} \approx \boldsymbol{S}_{zz} > \boldsymbol{S}_{yy}$$

#### Viscosity Length and Bagnold Rheology

• Typically for liquid-like shear flow, we expect shear stress to obey

$$\boldsymbol{s}_{xz} = \boldsymbol{r}\boldsymbol{n}\boldsymbol{g}$$

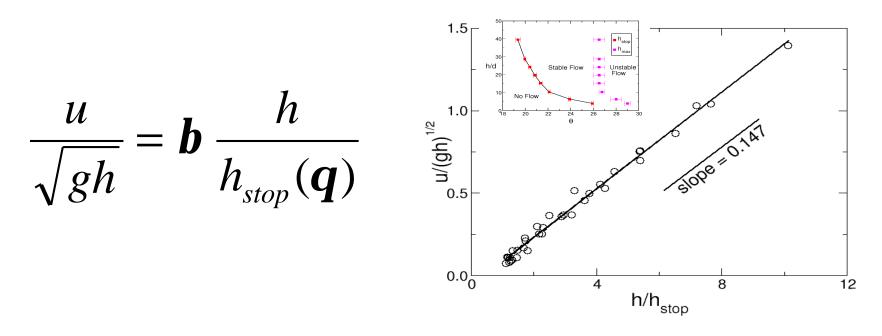
• On dimensional grounds, define viscosity length scale  $l_{v}(\rho)$ 

$$\boldsymbol{n} \equiv l_{\boldsymbol{n}}^2 \, \boldsymbol{\dot{g}}$$

• For chute flow, if  $\rho$  = const, "Bagnold rheology"

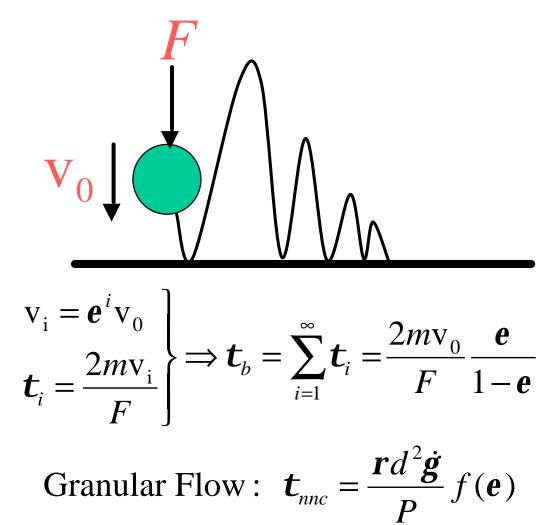
$$\boldsymbol{s}_{xz} = \boldsymbol{r}gz\sin\boldsymbol{q} = \boldsymbol{r}l_n^2 \dot{\boldsymbol{g}}^2 \Longrightarrow \begin{cases} \partial_z \mathbf{v}_x = A_{Bag}\sqrt{z} \\ A_{Bag} = \frac{\sqrt{g}\sin\boldsymbol{q}}{l_n} \end{cases}$$

#### **Pouliquen Flow Rule**



- Pouliquen flow rule summarizes much of the phenomenology of chute flows
  - Relates average velocity *u* to depth *h*
  - Connects depth of arresting pile  $h_{stop}(\theta)$  with rheology  $(l_v)$
  - Unstable flow line is approximately independent of flow depth

# Inelastic Collapse of Nearest Neighbors



- Inelastic ball (ε < 1) pushed to a surface with force F comes to rest in finite time τ<sub>h</sub>
- In dense granular media, depletion force

$$F \sim P / d^2$$

• Initial collision velocity

$$\mathbf{v}_0 \sim d\dot{\mathbf{g}}$$

 Expect more complicated dependence on E in granular flow due to disorder, friction, angular averaging and presence of other neighbors

#### **Correlated Motion of Grains**

 Anticipate that neighboring particle motions will become correlated if they collide sufficiently many times before shearing off:

$$\boldsymbol{t}_{nnc} = \frac{\boldsymbol{r}d^{2}\boldsymbol{\dot{g}}}{P}f(\boldsymbol{e}) < \boldsymbol{\dot{g}}^{-1}$$

- Time for a correlated region surrounded by constant pressure *P* to grow to size *l* :
- Characteristic correlation length  $l_e$ due to cutoff time imposed by strain rate, given initial collision velocity :

$$\boldsymbol{t}_{c}(l,P) \sim \left(\frac{l}{d}\right)^{2} \boldsymbol{t}_{nnc} = \frac{\boldsymbol{r}l^{2}\boldsymbol{\dot{g}}}{P} f(\boldsymbol{e})$$

$$\widetilde{a} \, \frac{\boldsymbol{r} l_e^2 \boldsymbol{\dot{g}}}{P} f(\boldsymbol{e}) = \boldsymbol{\dot{g}}^{-1}$$

(

• We postulate that apart from finite-size corrections, the viscosity length scale is set by the characteristic correlation length:

$$l_{\mathbf{n}}^2 = l_e^2 (1 + \widetilde{b} \, \frac{d}{l_e} + \dots)$$

• Solving for  $l_e$  and  $\dot{\boldsymbol{g}}$ 

$$l_e = \frac{\widetilde{b} d \tan \boldsymbol{q}_R}{\tan \boldsymbol{q} - \tan \boldsymbol{q}_R} \sim \frac{d}{\boldsymbol{q} - \boldsymbol{q}_R}, \quad \tan \boldsymbol{q}_R = [\widetilde{a} f(\boldsymbol{e})]^{-1}$$

and

$$\dot{\boldsymbol{g}} = A_{Bag}\sqrt{z}, \quad A_{Bag} = \frac{\sqrt{g\sin\boldsymbol{q}_R}}{l_e} \sim \frac{\sqrt{g}}{d}(\boldsymbol{q}-\boldsymbol{q}_R)$$

# **Phase Diagram**

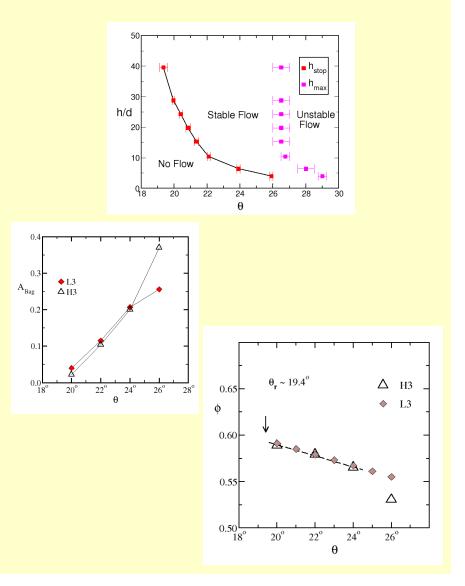
- Expect rheology to break down if cluster size is comparable to total flow depth (flow arrest), or size of one particle (unstable flow)
- Predicts Pouliquen flow rule with

$$h_{stop} \propto \frac{d \tan \boldsymbol{q}_R}{\tan \boldsymbol{q} - \tan \boldsymbol{q}_R}$$

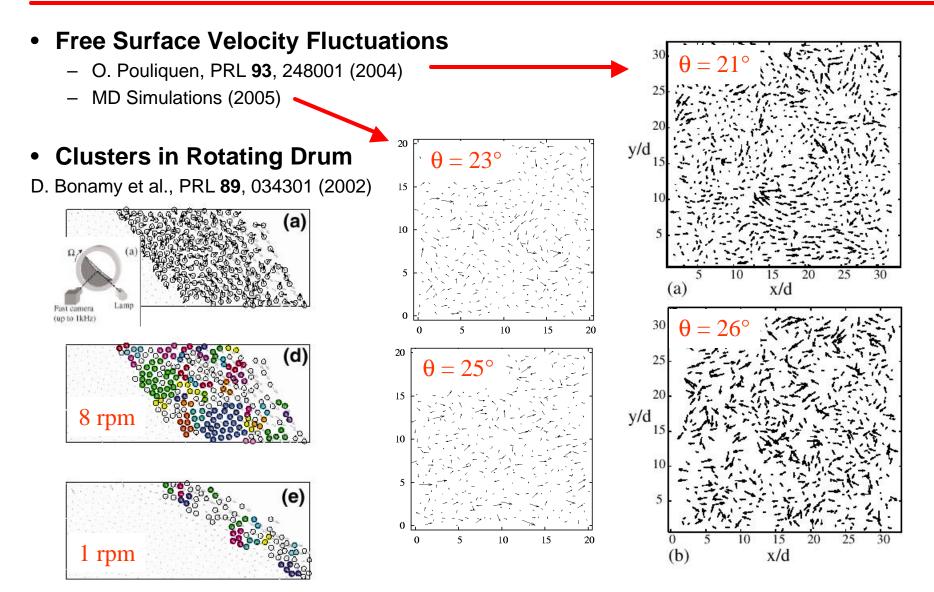
 Also predicts depth-independent unstable flow criterion-correlated motion a <u>necessity</u> for stable flow

 $\mathbf{r}_{c}-\mathbf{r}\sim l_{e}^{-1}$ 

- Predicts A<sub>Bag</sub> linear in tilt angle
- Consistent with



# **Evidence of Correlated Motion**



# Summary

- Chute flow obeys "Granular Liquid" kinematics with Bagnold rheology
- Hypothesis of correlated motion accounts semi-quantitatively for notable aspects of phenomenology
  - ✓ Velocity profile with depth, tilt angle
  - ✓ Pouliquen flow rule
  - ✓ Phase diagram
- Recent hints on the nature of the correlated motions
  - **? Kinetic theory incorporating velocity correlations**
- Next Challenge: Underwater flows through implementation of lubrication forces