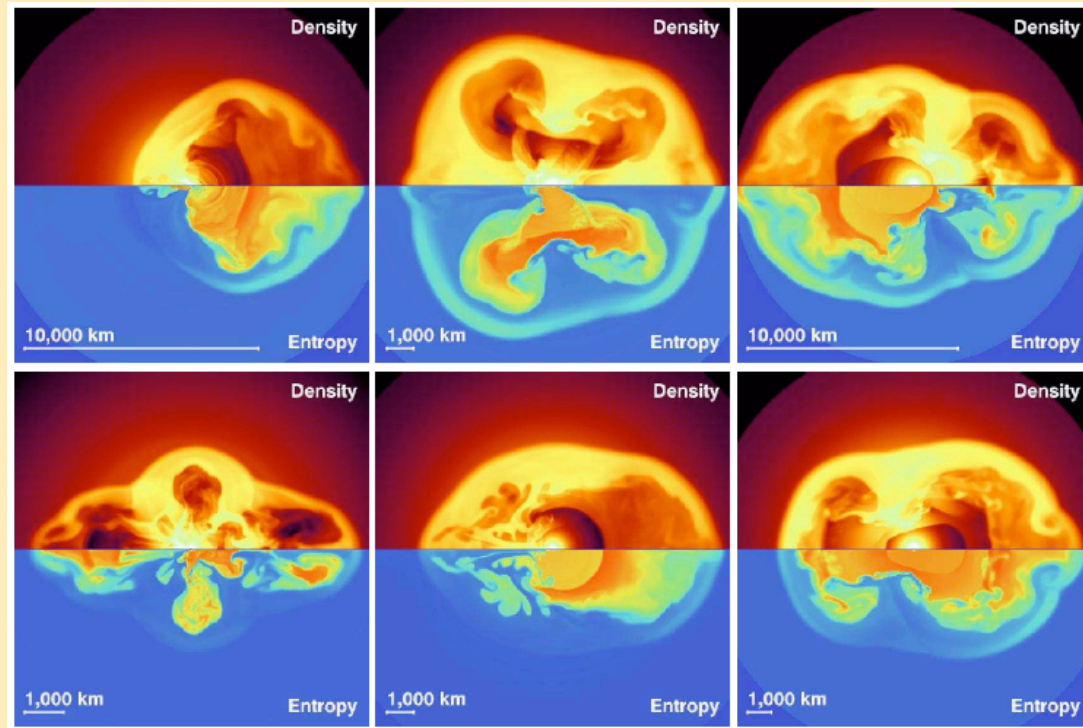
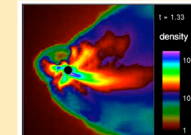


The basics of the Advective-Acoustic Cycle



Janka et al. (2004)



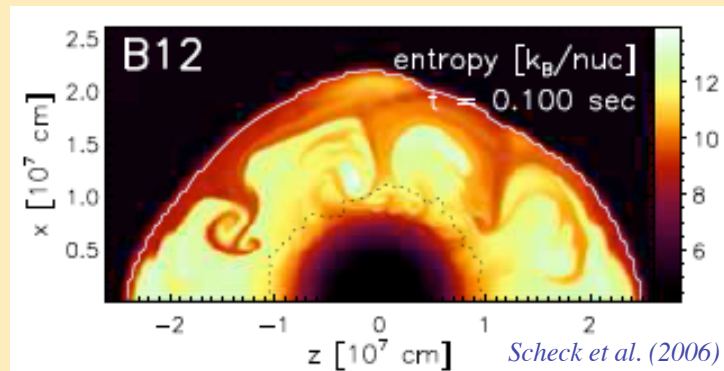
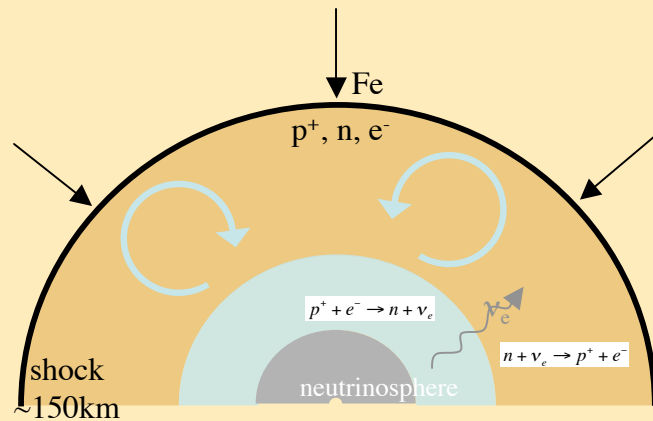
Chanaud & Powell (1965)

Thierry Foglizzo, Pascal Galletti (CEA Saclay)
Thomas Janka, Leonhard Scheck (MPA Garching)

Outline

1. Instability of the stalled accretion shock during core collapse
2. The advective-acoustic cycle: a new instability ?
3. Understanding simple toy models
 - why is there an advective-acoustic coupling ?
 - why a low frequency, low l instability ?
 - why transverse rather than radial ?
4. Conclusion: back to the core-collapse problem

Instabilities during the phase of stalled accretion shock



- Convection in the gain region, low l
(Herant, Benz & Colgate 1992)

- $l=1,2$ SASI in an adiabatic flow:
vortical-acoustic cycle (Blondin, Mezzacappa & DeMarino 2003)
or purely acoustic mechanism (Blondin & Mezzacappa 2006) ?

- Neutron star kick resulting from the $l=1$ instability of
convection and/or **vortical-acoustic cycle**
(Scheck et al. 2004, Janka et al. 2004, Scheck et al. 2006)

- New explosion mechanism driven by acoustic waves, initiated
by the **advective-acoustic cycle** (Burrows et al. 2005)

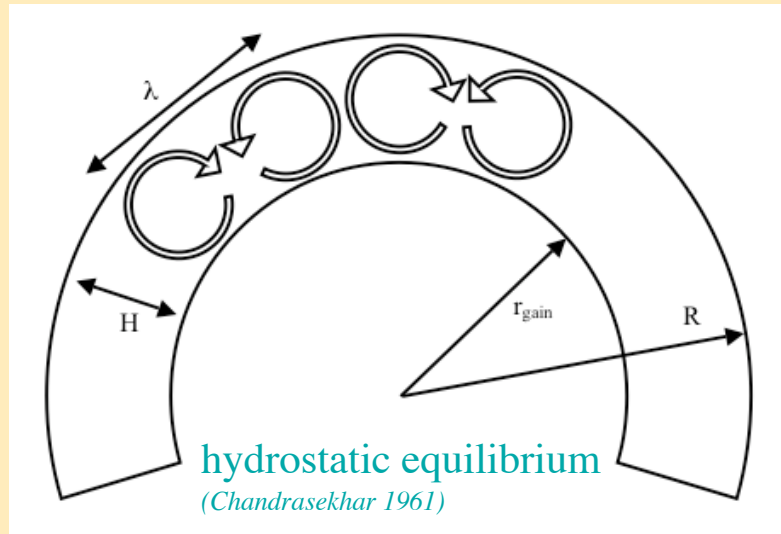
convection ?

SASI 2003 ?

SASI 2006 ?

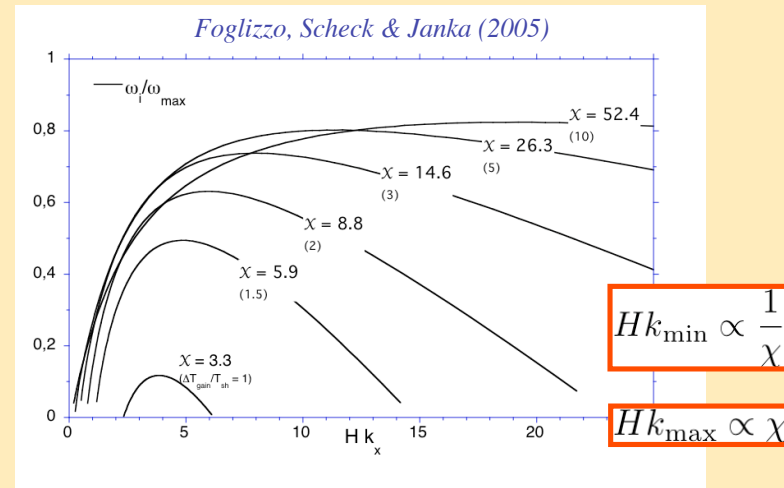
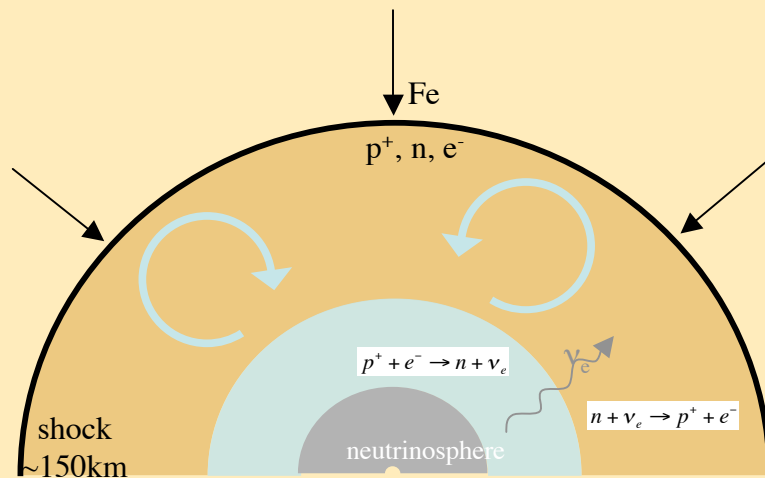
advective-acoustic cycle ?

Contribution of the convective instability to a mode $l=1$?



$$\frac{H\omega_{\text{buoy}}}{v} \sim \left(\frac{GM}{r_{\text{sh}} v_2^2} \right)^{\frac{1}{2}} \left(\frac{H}{r_{\text{sh}}} \right)^{\frac{1}{2}}$$

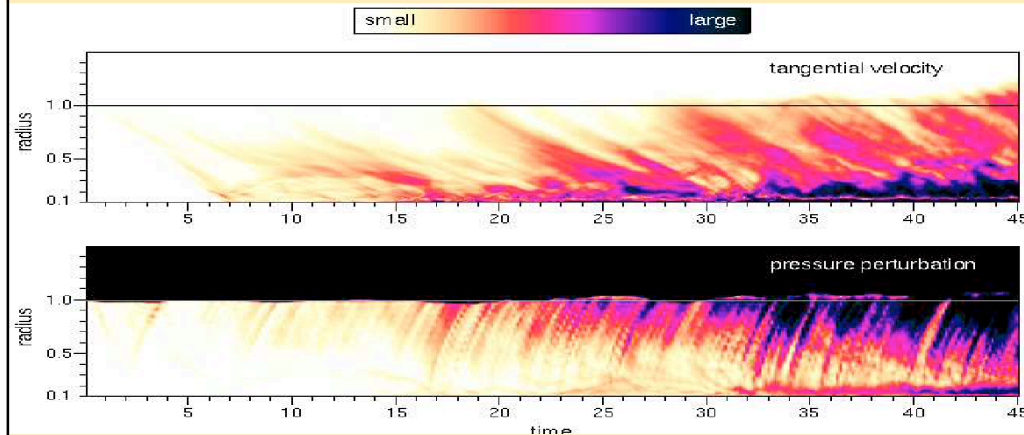
$$\sim 3.1 \left(\frac{v_1}{7v_2} \right) \left(\frac{H}{0.4r_{\text{sh}}} \right)^{\frac{1}{2}}$$



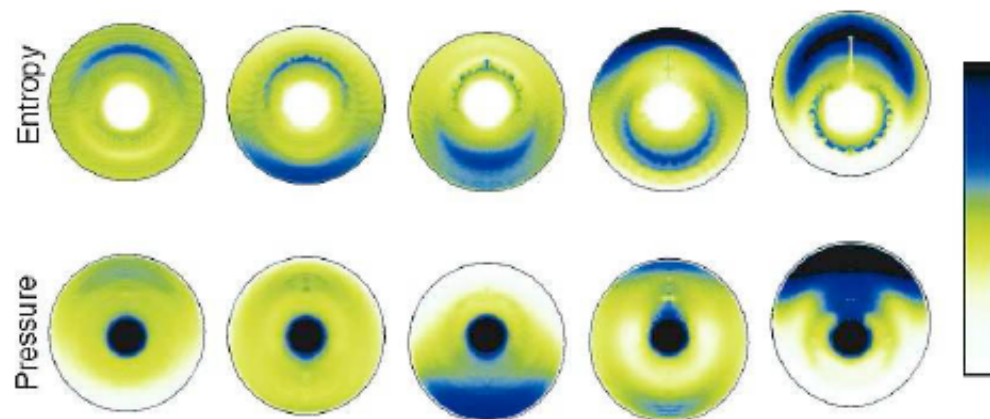
$$\chi \equiv \int_{z_{\text{sh}}}^{z_{\text{gain}}} \omega_{\text{buoy}} \frac{dz}{v}$$

$$\chi \sim 3$$

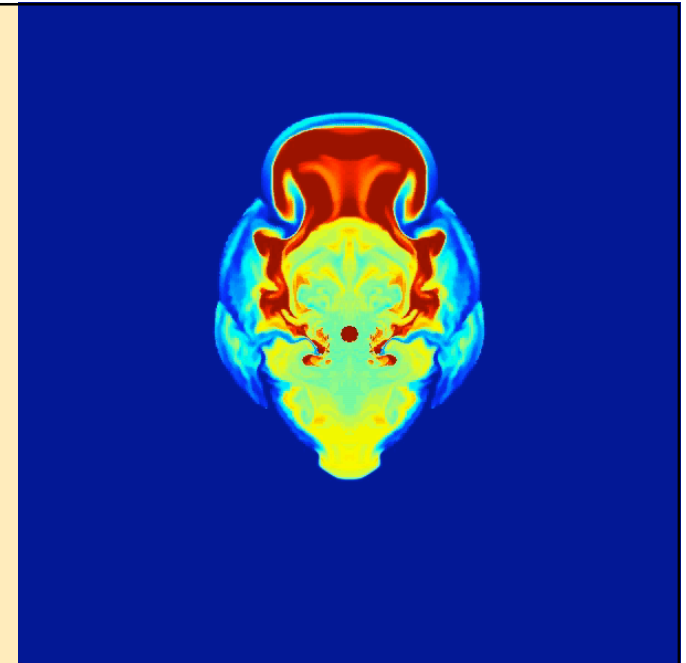
Asymmetry without convection: adiabatic simulation of a stalled accretion shock on a neutron star



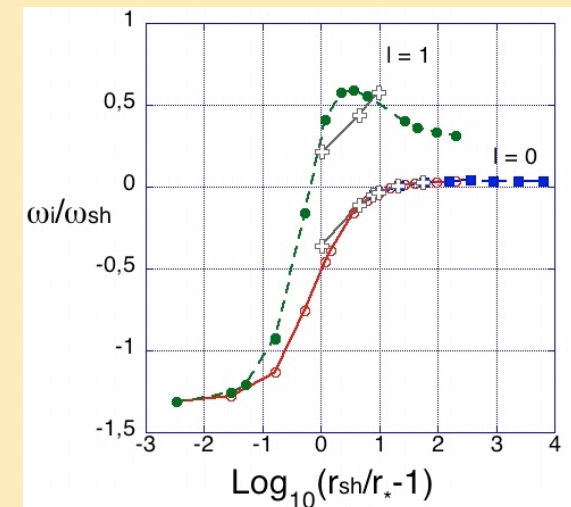
Evidence for a vortical-acoustic cycle (*Blondin, Mezzacappa & DeMarino 2003*)



A purely acoustic cycle ? (*Blondin & Mezzacappa 2005*)



Linear stability analysis



$l=0$: Houck & Chevalier (1992)
 $l=0,1$: Galletti (PhD Thesis 2005)
 Blondin & Mezzacappa (2005)

Outline

1. Instability of the stalled accretion shock during core collapse

2. The advective-acoustic cycle: a new instability ?

3. Understanding simple toy models

- why is there an advective-acoustic coupling ?
- why a low frequency, low l instability ?
- why transverse rather than radial ?

4. Conclusion: back to the core-collapse problem



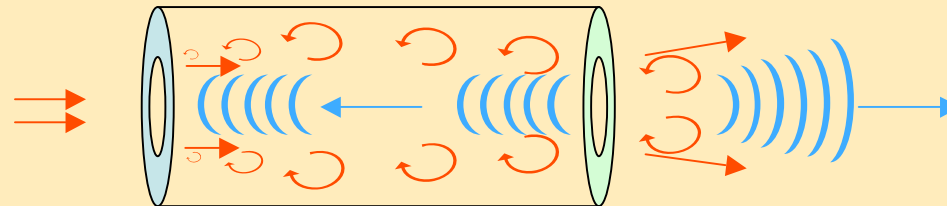
vibrations in Ariane 5:
segmented solid propergol
Mettenleiter, Haile & Candel (2000)
J. of Sound and Vibration 230, 761

impinging shear layers
Rockwell, D. 1983, AIAA J., 21, 645

Aero-acoustic instabilities

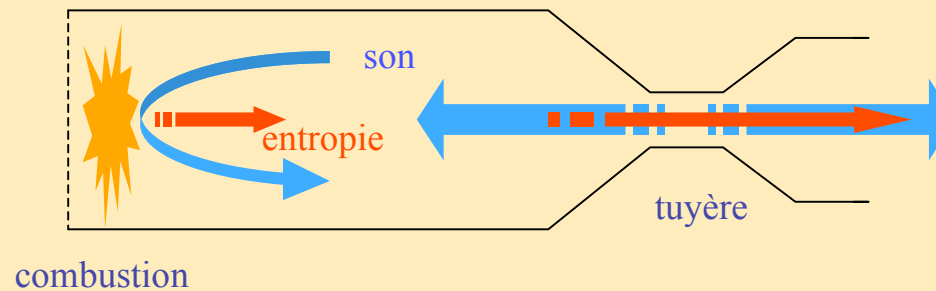
- advected perturbations
- acoustic feedback

• vortical-acoustic cycle



whistling kettle
Chanaud & Powell (1965)
J. Acoust.Soc. Am. 37, 902

• entropic-acoustic cycle

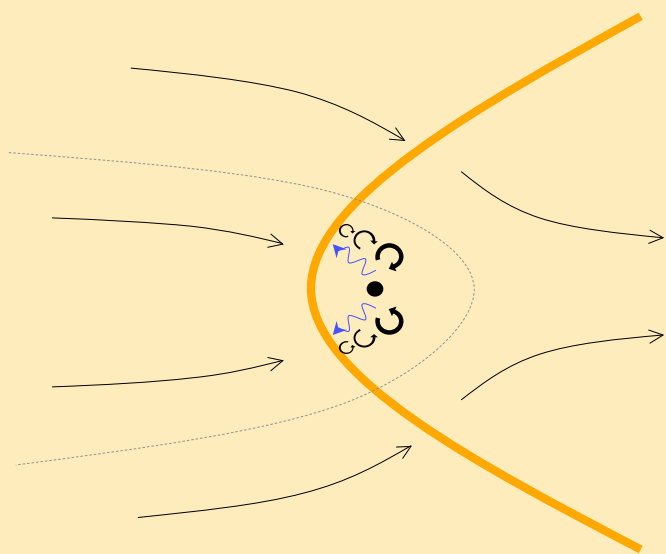


rumble instability of ramjet combustors

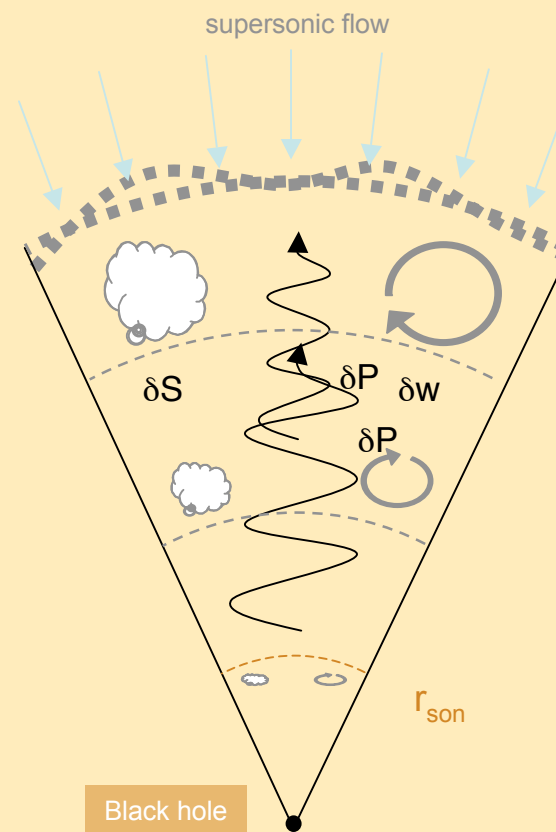
Abouseif, Keklak & Toong (1984)
Combustion Science and Technology, 36, 83

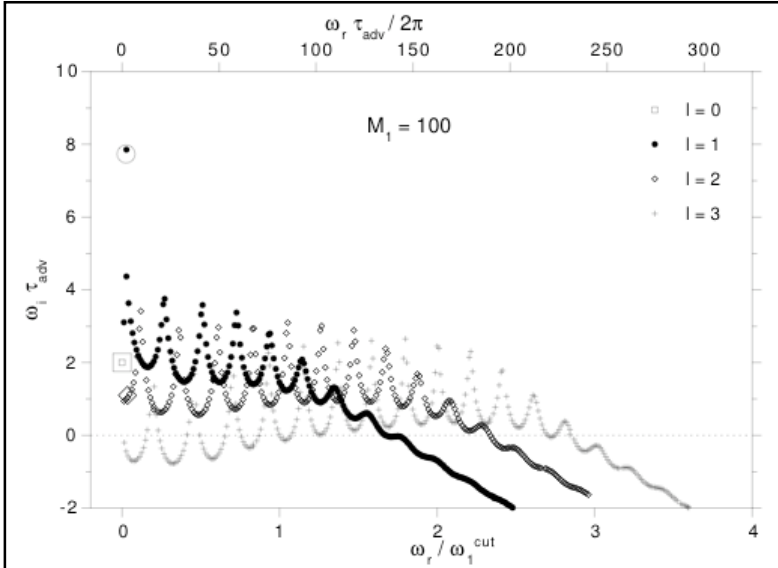
Analytical study of the advective-acoustic coupling in a radial, accelerated flow

Foglizzo (2001, 2002), Foglizzo, Galletti & Ruffert (2005)

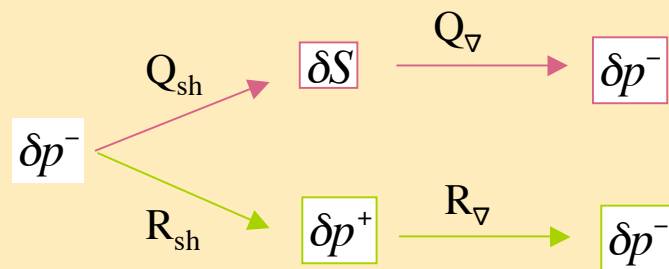


Bondi-Hoyle-Lyttleton accretion; unstable





isothermal flow (Foglizzo 2002)



advective-acoustic cycle

efficiency $Q \equiv Q_{sh} Q_{\nabla}$
duration τ_Q

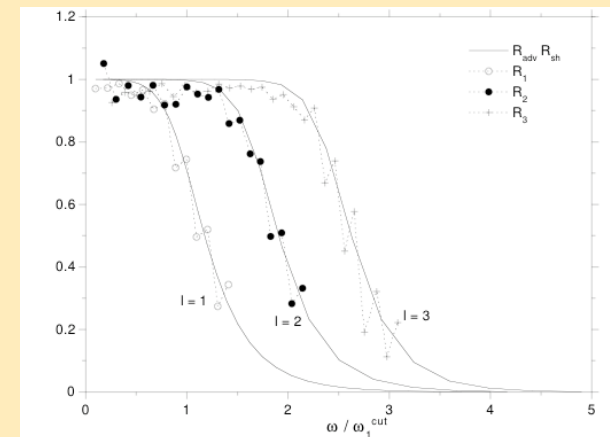
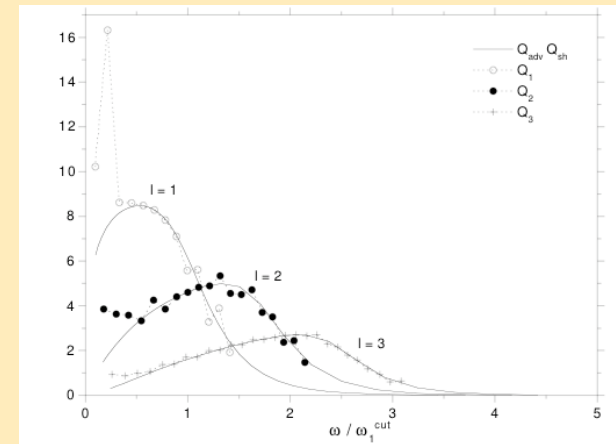
purely acoustic cycle

efficiency $\mathcal{R} \equiv \mathcal{R}_{sh} \mathcal{R}_{\nabla}$
duration $\tau_{\mathcal{R}}$

$$Q e^{i\omega \tau_Q} + \mathcal{R} e^{i\omega \tau_{\mathcal{R}}} = 1$$

Beyond the eigenspectrum

- identification of the 2 cycles (Q, τ_Q) and ($\mathcal{R}, \tau_{\mathcal{R}}$)



Outline

1. Instability of the stalled accretion shock during core collapse

2. The advective-acoustic cycle: a new instability ?

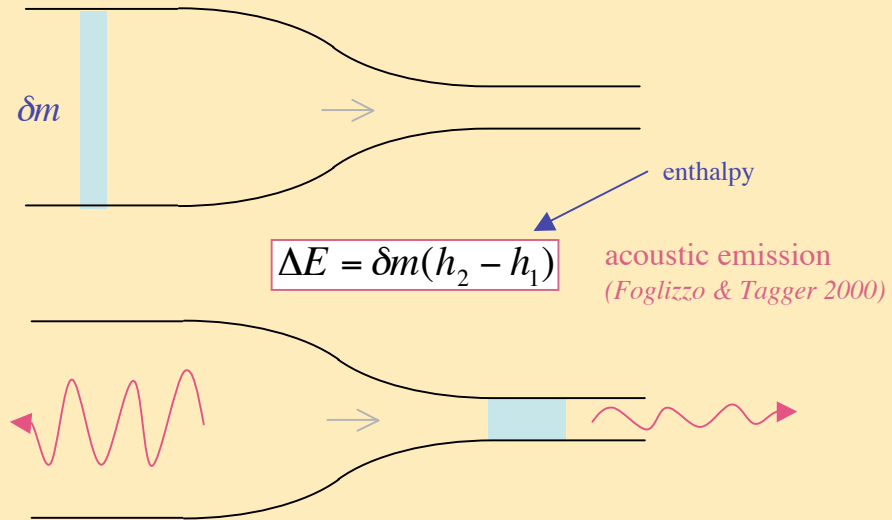
3. Understanding simple toy models

- why is there an advective-acoustic coupling ?
- why a low frequency, low l instability ?
- why transverse rather than radial ?

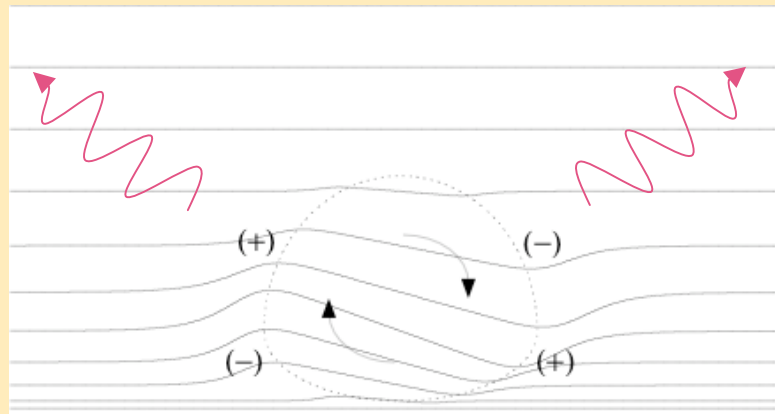
4. Conclusion: back to the core-collapse problem

Advection-acoustic coupling: hand waving

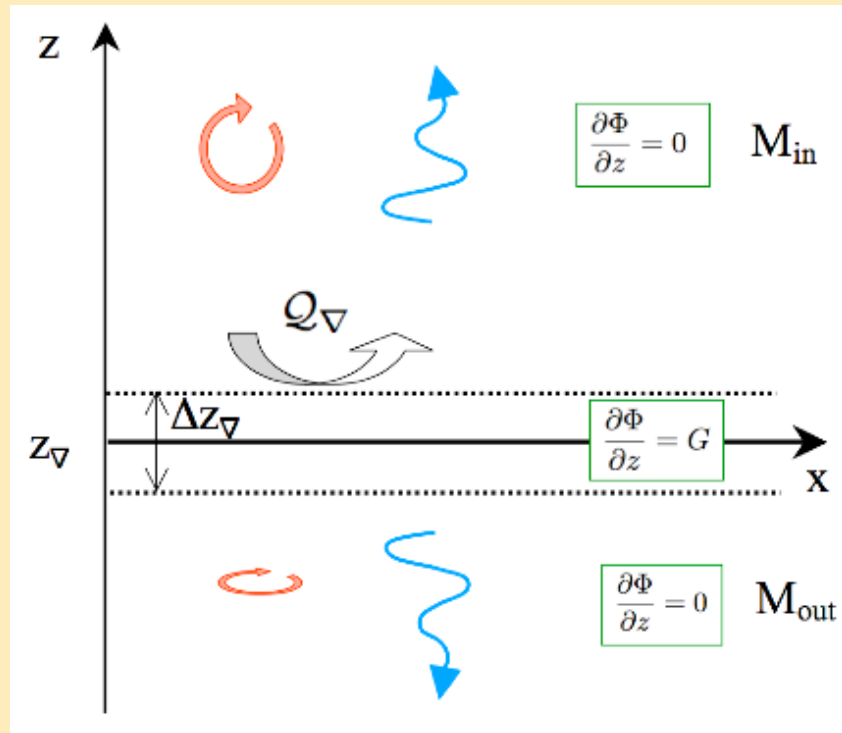
advection of entropy



advection of vorticity



Advection-acoustic coupling: illustrative simulations



2 isothermal simulations (thanks to F. Masset)

-> accelerated flow ($M_{in}=0.1, M_{out}=0.7$)

$$\omega < k_x c (1 - \mathcal{M}_{out}^2)^{\frac{1}{2}} < k_x c (1 - \mathcal{M}_{in}^2)^{\frac{1}{2}}$$

in: evanescent
out: evanescent

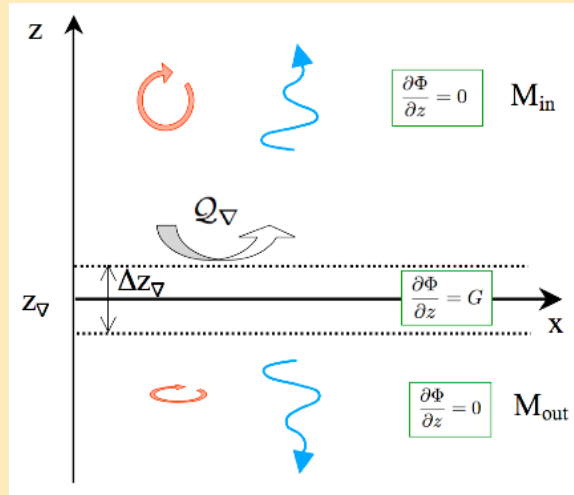
-> decelerated flow ($M_{in}=0.7, M_{out}=0.1$)

$$k_x c (1 - \mathcal{M}_{in}^2)^{\frac{1}{2}} < \omega < k_x c (1 - \mathcal{M}_{out}^2)^{\frac{1}{2}}$$

in: propagate
out: evanescent

propagating wave: $\omega > k_x c (1 - \mathcal{M}^2)^{\frac{1}{2}}$
evanescent wave: $\omega < k_x c (1 - \mathcal{M}^2)^{\frac{1}{2}}$

$$\left(\begin{aligned} \omega^2 &= (k_x^2 + k_z^2) c^2 \\ k_z^2 &= \frac{\omega^2}{c^2} - k_x^2 \end{aligned} \right)$$



Compact approximation

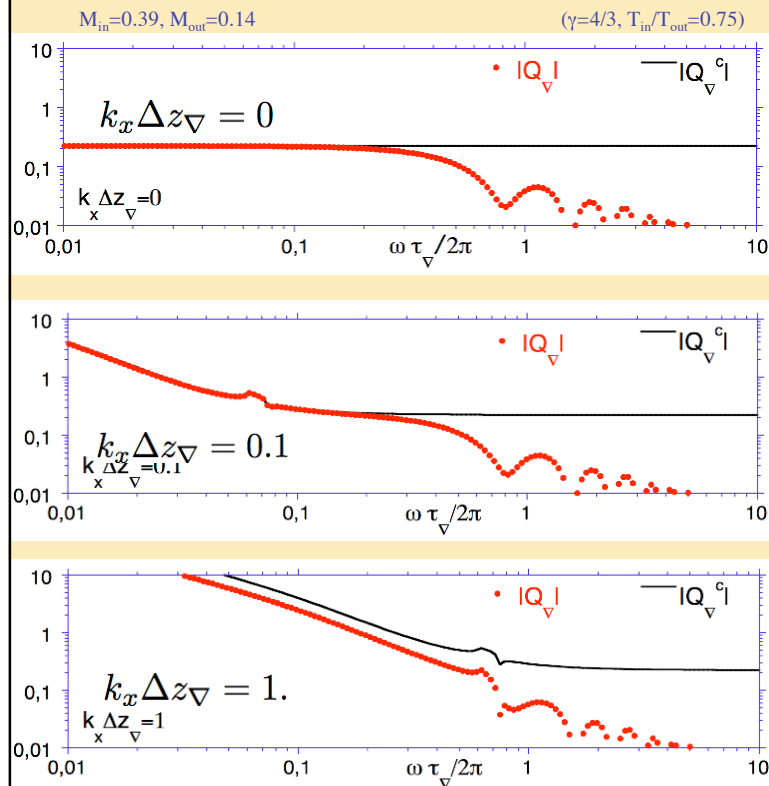
$$\Delta z_{\nabla} \rightarrow 0$$

scale free

$$\tau_{\nabla} \equiv \int_{z_{\nabla} - \frac{\Delta z_{\nabla}}{2}}^{z_{\nabla} + \frac{\Delta z_{\nabla}}{2}} \frac{dz}{|v|}$$

validity of the compact approximation

$$\left\{ \begin{array}{l} \tau_{\nabla} \ll \frac{2\pi}{\omega} \\ k_x \Delta z_{\nabla} \ll 1 \end{array} \right.$$



$$Q_{\nabla}^c = \frac{\mathcal{M}_{\text{out}} + \mu_{\text{out}}}{1 + \mu_{\text{out}} \mathcal{M}_{\text{out}}} \frac{1}{\mu_{\text{out}} \frac{c_{\text{in}}^2}{c_{\text{out}}^2} + \mu_{\text{in}} \frac{\mathcal{M}_{\text{out}}}{\mathcal{M}_{\text{in}}}} \left[1 - \frac{c_{\text{in}}^2}{c_{\text{out}}^2} + \frac{k_x^2 c_{\text{in}}^2}{\omega^2} (\mathcal{M}_{\text{in}}^2 - \mathcal{M}_{\text{out}}^2) \right]$$

$$\mu^2 \equiv 1 - \frac{k_x^2 c^2}{\omega^2} (1 - \mathcal{M}^2)$$

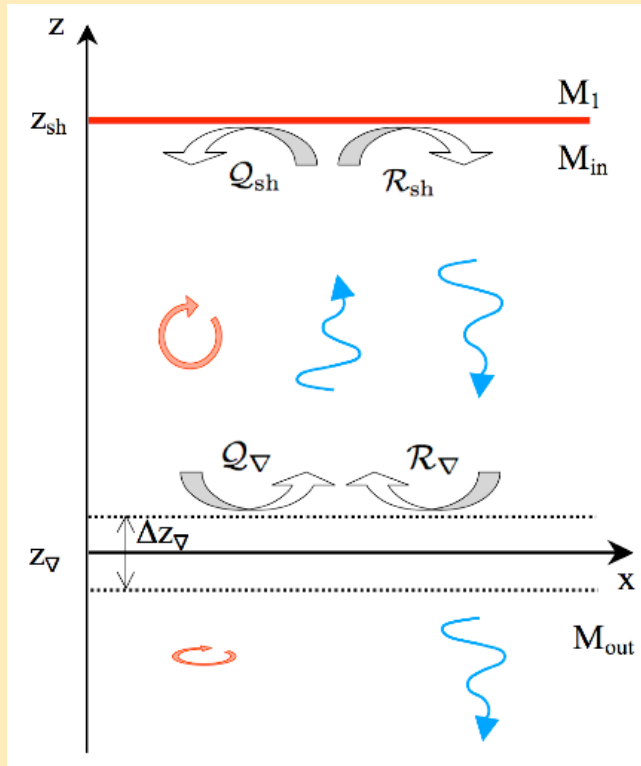
longitudinal

transverse

cut-off frequency $\omega_{\nabla} \equiv \frac{1}{\tau_{\nabla}}$

-> analytical upper bound of the coupling efficiency

The simplest example of an advective-acoustic instability



$$\tau_Q \equiv \frac{1 + \mu_{in} \mathcal{M}_{in} \frac{z_{sh} - z_v}{|v_{in}|}}{1 - \mathcal{M}_{in}^2}$$

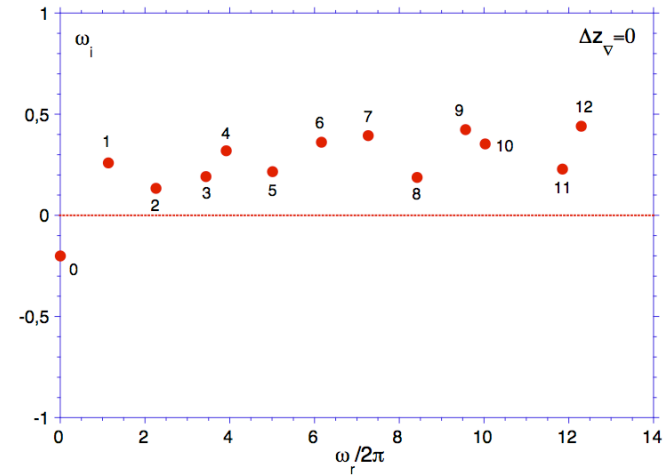
$$\tau_R \equiv \frac{2\mu_{in} \frac{z_{sh} - z_v}{c_{in}}}{1 - \mathcal{M}_{in}^2}$$

$$\mathcal{Q}_c \equiv \frac{\frac{4\mu_{in}(1 - \mathcal{M}_{in}^2)(1 - \frac{1}{\mathcal{M}_1^2})}{\mu_{out} \frac{c_{in}^2}{c_{out}^2} + \mu_{in} \frac{\mathcal{M}_{out}}{\mathcal{M}_{in}}} \mathcal{M}_{out} + \mu_{out}}{1 + \mu_{out} \mathcal{M}_{out}} \left[\frac{1 - \frac{c_{in}^2}{c_{out}^2} + \frac{k_x^2 c_{in}^2}{\omega^2} (\mathcal{M}_{in}^2 - \mathcal{M}_{out}^2)}{(\gamma + 1)(1 - \mu_{in} \mathcal{M}_{in})(\mu_{in}^2 + 2\mu_{in} \mathcal{M}_{in} + \mathcal{M}_1^{-2})} \right]$$

-parallel adiabatic flow, localized coupling ($\gamma, \mathcal{M}_1, \Delta\Phi, \Delta z_\nabla$)
 -2-D perturbations ω, k_\perp

$$\mathcal{M}_1=5, \gamma=4/3, T_{in}/T_{out}=0.75$$

$$(\mathcal{M}_{in}=0.39, \mathcal{M}_{out}=0.14)$$

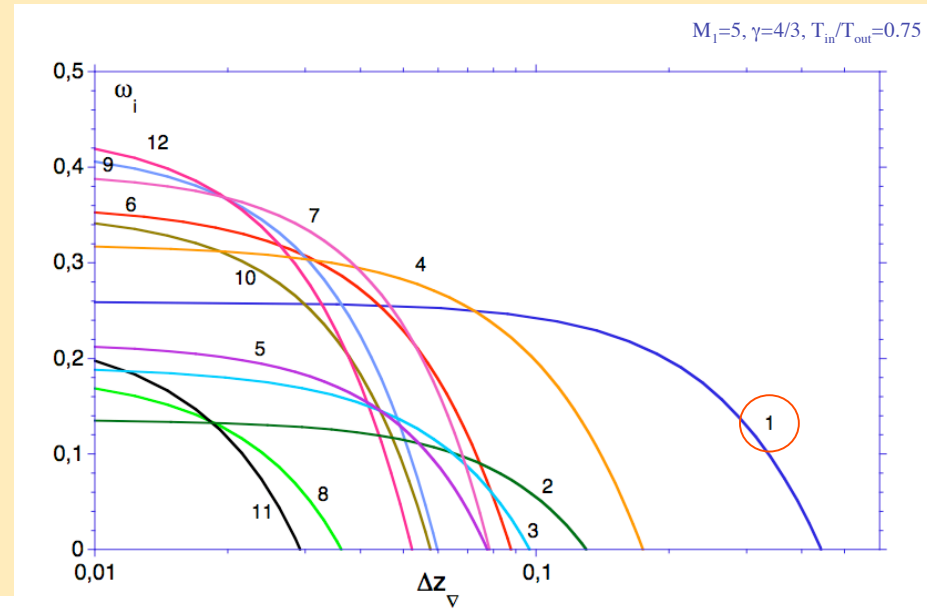
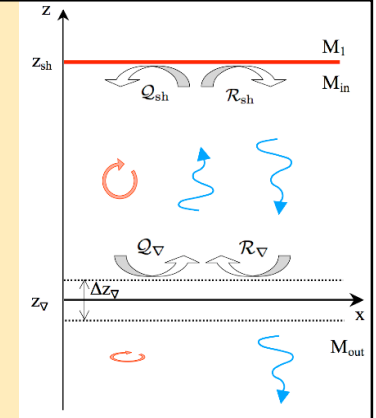


$$\mathcal{Q}e^{i\omega\tau_Q} + \mathcal{R}e^{i\omega\tau_R} = 1$$

$$\mu^2 \equiv 1 - \frac{k_x^2 c^2}{\omega^2} (1 - \mathcal{M}^2)$$

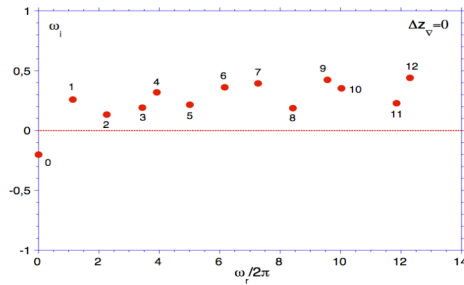
$$R = \frac{\mu_{out} \mathcal{M}_{in} c_{in}^2 - \mu_{in} \mathcal{M}_{out} c_{out}^2}{\mu_{out} \mathcal{M}_{in} c_{in}^2 + \mu_{in} \mathcal{M}_{out} c_{out}^2} \left(\frac{1 + \mu_{in} \mathcal{M}_{in}}{1 - \mu_{in} \mathcal{M}_{in}} \right) \frac{\mu_{in}^2 - 2\mu_{in} \mathcal{M}_{in} + \frac{1}{\mathcal{M}_1^2}}{\mu_{in}^2 + 2\mu_{in} \mathcal{M}_{in} + \frac{1}{\mathcal{M}_1^2}}$$

Effect of the size Δz_∇ of the coupling region

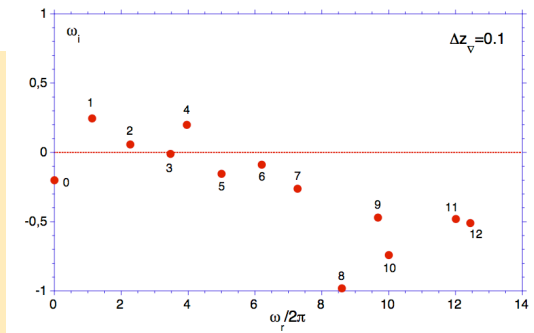


compact approximation confirmed

a possible benchmark test



a low frequency instability



$$k_x c (1 - \mathcal{M}^2)^{\frac{1}{2}} \leq \omega \ll \omega_\nabla$$

a low n_x instability

why not $n_x=0$?
why so much irregularity ?

Comparison of $n_x=0$ and $n_x>0$ modes

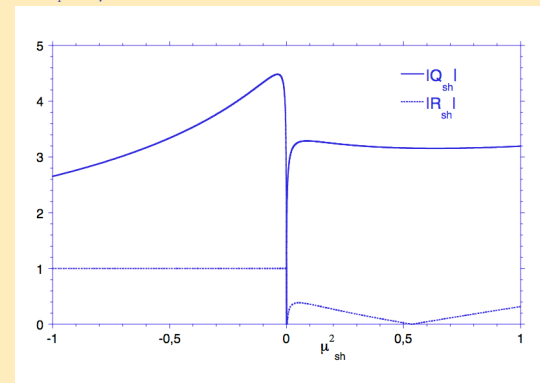
- no vorticity in 1-D: the instability of the mode $n_x=0$ relies only on temperature gradients
- transverse modes benefits from the vortical-acoustic coupling

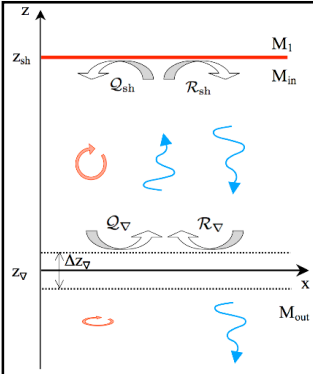
$$Q_c \equiv \frac{\frac{4\mu_{in}}{\mathcal{M}_{in}}(1 - \mathcal{M}_{in}^2)\left(1 - \frac{1}{\mathcal{M}_1^2}\right)}{\mu_{out}\frac{c_{in}^2}{c_{out}^2} + \mu_{in}\frac{\mathcal{M}_{out}}{\mathcal{M}_{in}}} \frac{\mathcal{M}_{out} + \mu_{out}}{1 + \mu_{out}\mathcal{M}_{out}} \left[\frac{1 - \frac{c_{in}^2}{c_{out}^2} + \frac{k_x^2 c_{in}^2}{\omega^2}(\mathcal{M}_{in}^2 - \mathcal{M}_{out}^2)}{(\gamma + 1)(1 - \mu_{in}\mathcal{M}_{in})(\mu_{in}^2 + 2\mu_{in}\mathcal{M}_{in} + \mathcal{M}_1^{-2})} \right]$$

At the shock, the coupling efficiency is also maximum for transverse perturbations:

$$\mu_{sh}^2 \propto \pm \frac{1}{\mathcal{M}_1^2}$$

$M_1=5, \gamma=4/3$





Contribution of the acoustic cycle

(Foglizzo 2002)

$$Qe^{i\omega T_Q} + Re^{i\omega T_R} = 1$$

global dispersion relation

The acoustic cycle alone is stable: $|\mathcal{R}| \leq 1$

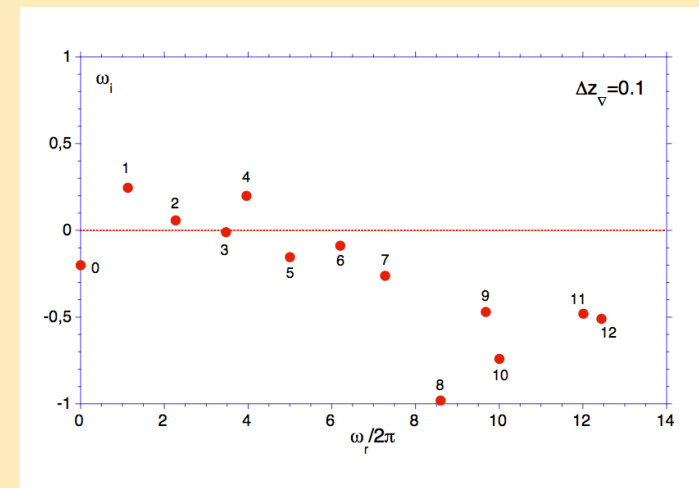
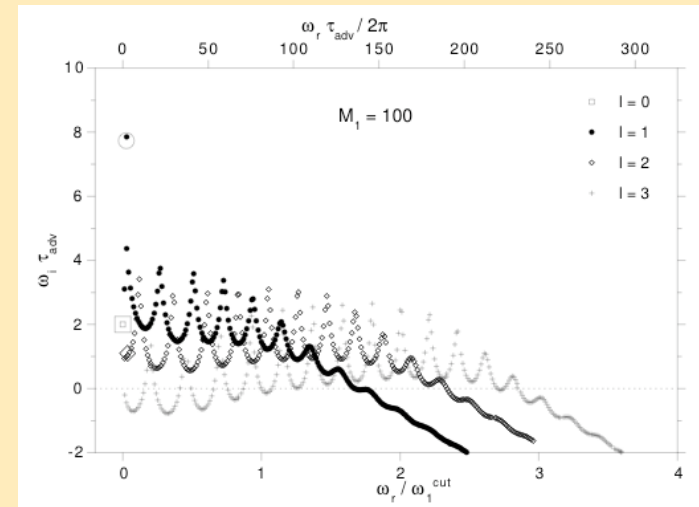
Its contribution can be either constructive or destructive

$$|Q| + |\mathcal{R}| < 1 \quad \text{stable}$$

$$|Q| - |\mathcal{R}| > 1 \quad \text{unstable}$$

$$\alpha \equiv \frac{|\mathcal{R}|}{|Q|^{\frac{\tau_R}{\tau_Q}}}$$

$$\frac{1}{\tau_Q} \log \{ (1 - \alpha) |Q| \} \leq \omega_i \leq \frac{1}{\tau_Q} \log \left\{ \frac{|Q|}{1 - \alpha} \right\}$$



->the stability threshold is very sensitive to geometrical factors

Outline

1. Instability of the stalled accretion shock during core collapse

2. The advective-acoustic cycle: a new instability ?

3. Understanding simple toy models

- why is there an advective-acoustic coupling ?
- why a low frequency, low l instability ?
- why transverse rather than radial ?

4. Conclusion: back to the core-collapse problem

Conclusion

Simple toy model of the advective-acoustic instability in a decelerated flow

- gradient cut-off -> low frequency

$$k_x c (1 - \mathcal{M}^2)^{\frac{1}{2}} \leq \omega \ll \omega_{\nabla}$$

- acoustic evanescence -> low n_x

- vorticity -> transverse rather than longitudinal

- acoustic cycle -> sensitive to geometrical parameters

Benchmark test for numerical simulations

- advection of vorticity, numerical viscosity ?

Relevance to the core-collapse problem ?

- gravity, geometry, photodissociation, heating, cooling

- detailed comparison with numerical simulations: ongoing effort (Blondin, Scheck et al. 2006)

