

VORTICITY BANDING IN SHEAR THICKENING SUSPENSIONS

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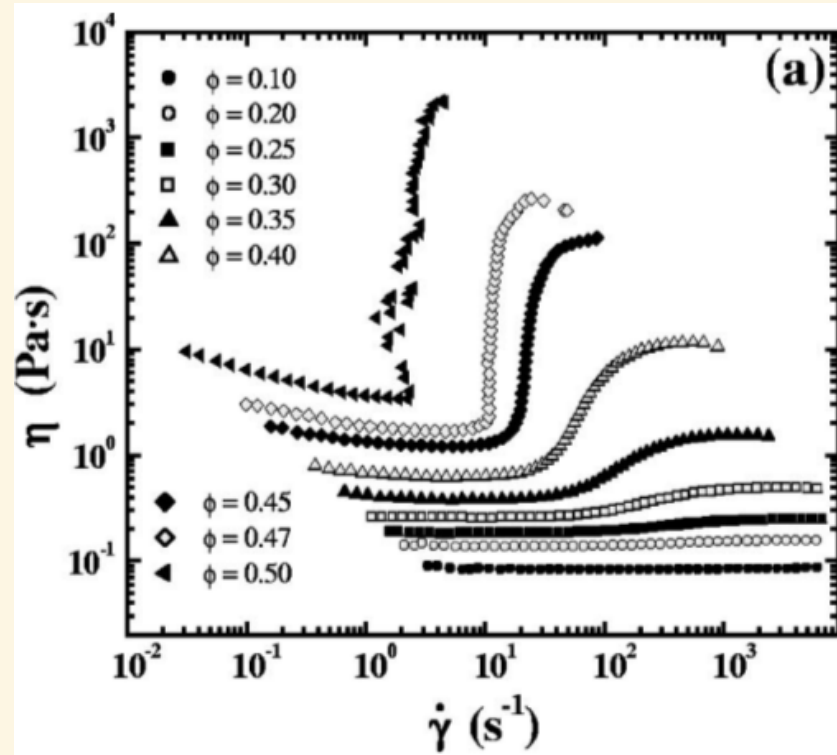


Mike Cates
DAMTP, Cambridge

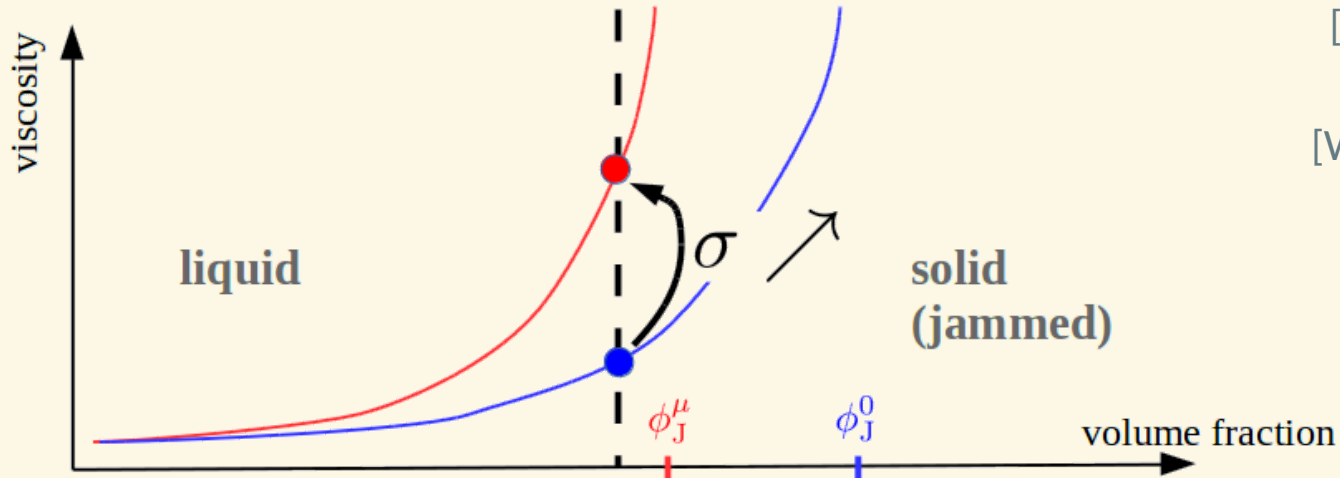
SHEAR THICKENING

[Egres & Wagner, JOR 2005]

~500nm calcium carbonate + polymer brush in PEG 200



THICKENING SCENARIO

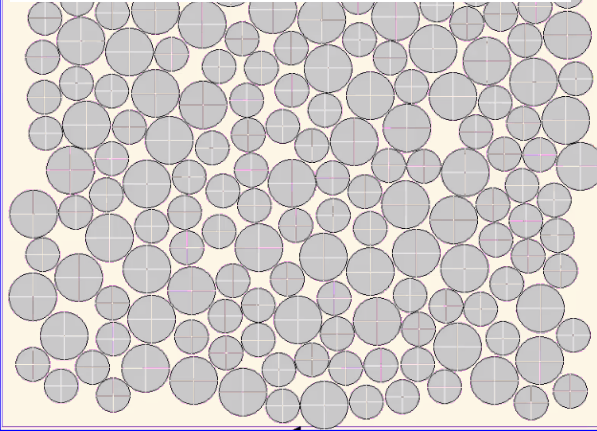


[Fernandez et al, PRL 2013]
[Seto et al, PRL 2013]
[Heussinger, PRE 2013]
[Wyart and Cates PRL 2013]
[Mari et al, JOR 2014]

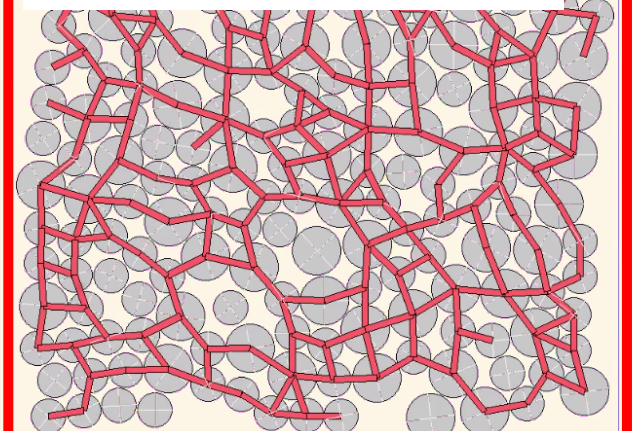
- Frictional contacts
- Repulsive force, stress scale

$$\sigma^* = \frac{\text{force}}{\text{radius}^2}$$

Low stress
lubricated contacts

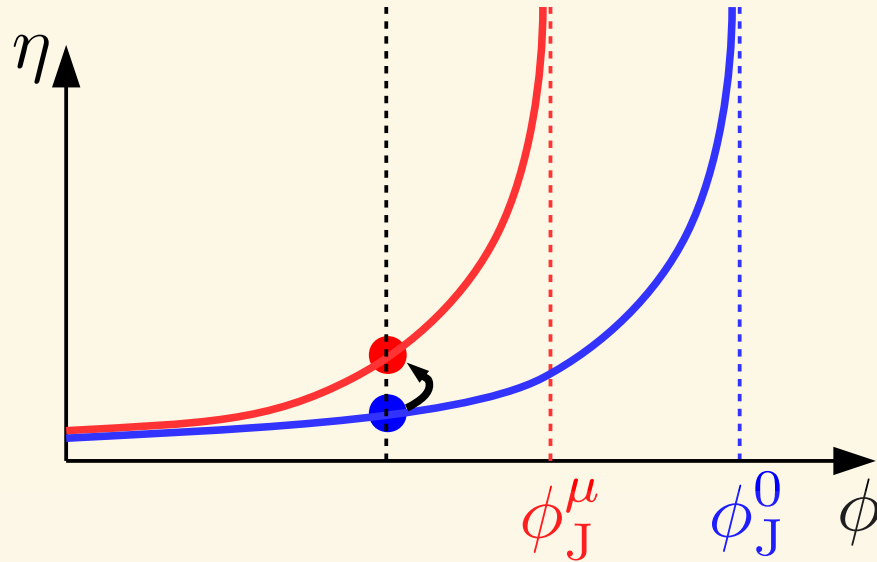


High stress
frictional contacts

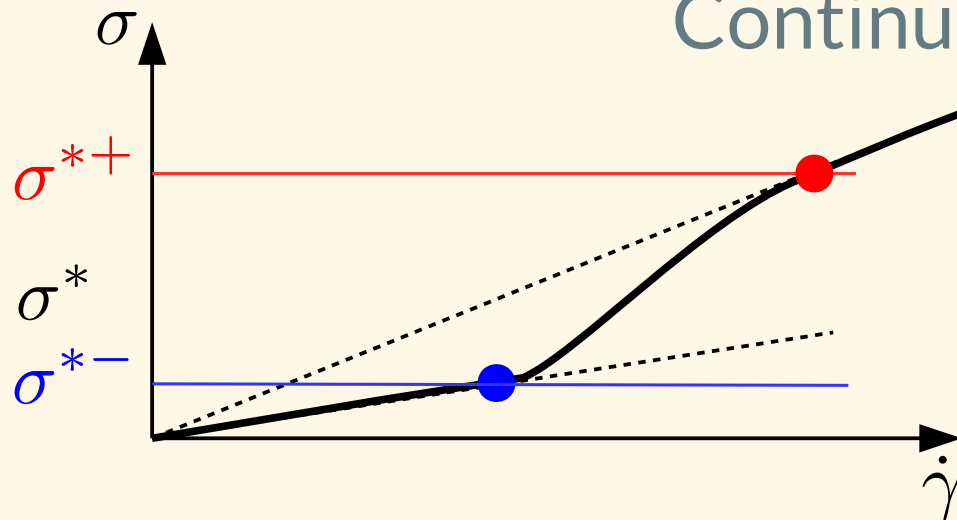


THICKENING SCENARIO

[Wyart & Cates, PRL 2014]

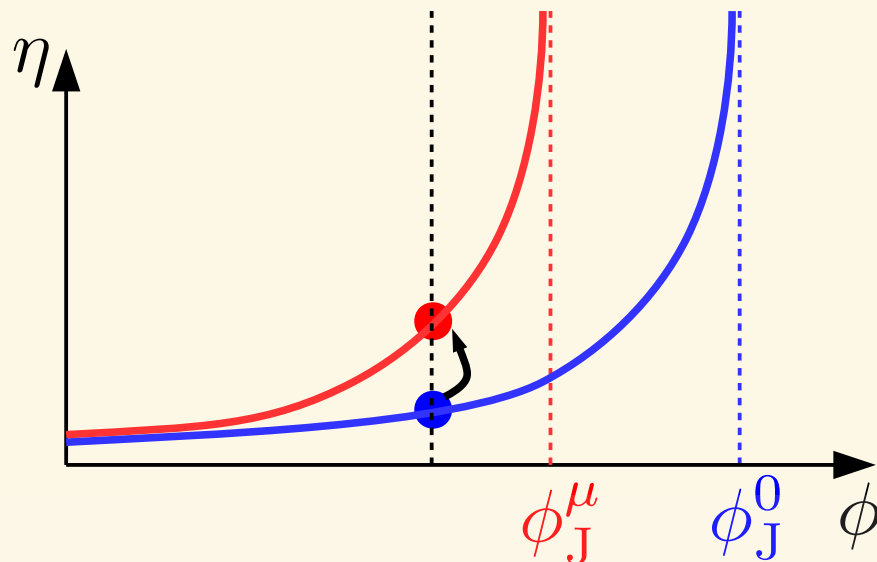


Continuous Shear Thickening

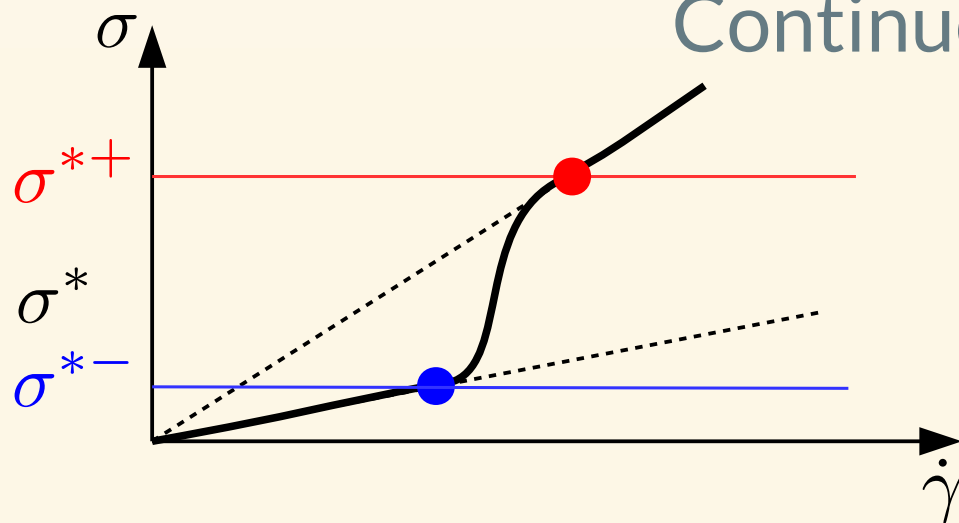


THICKENING SCENARIO

[Wyart & Cates, PRL 2014]

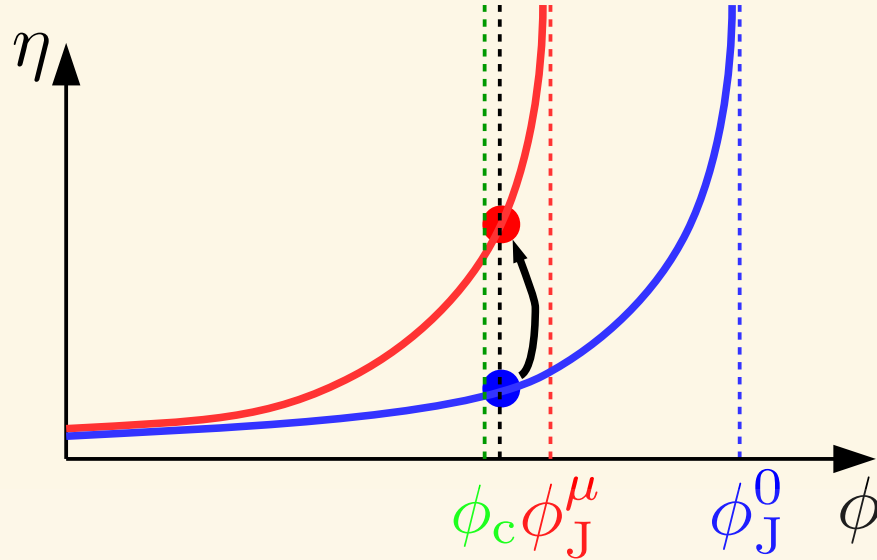


Continuous Shear Thickening

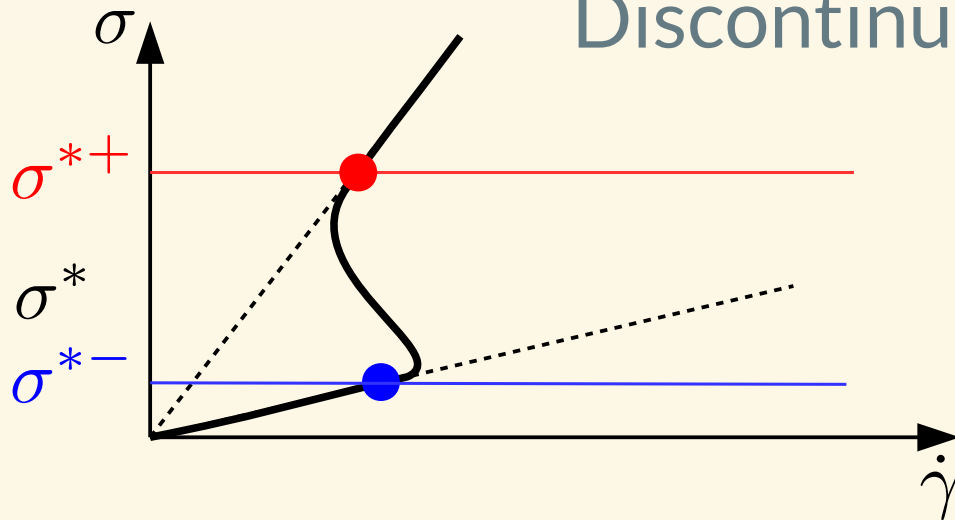


THICKENING SCENARIO

[Wyart & Cates, PRL 2014]

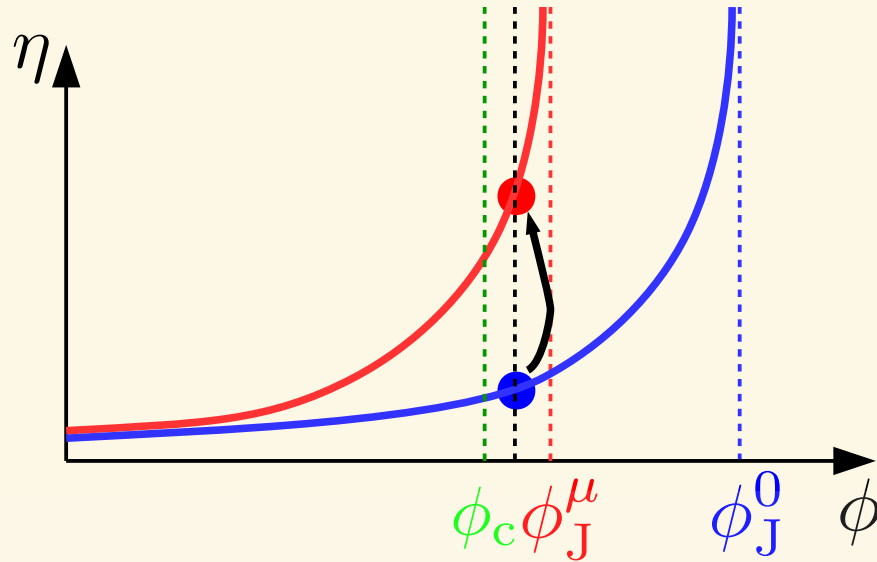


Discontinuous Shear Thickening

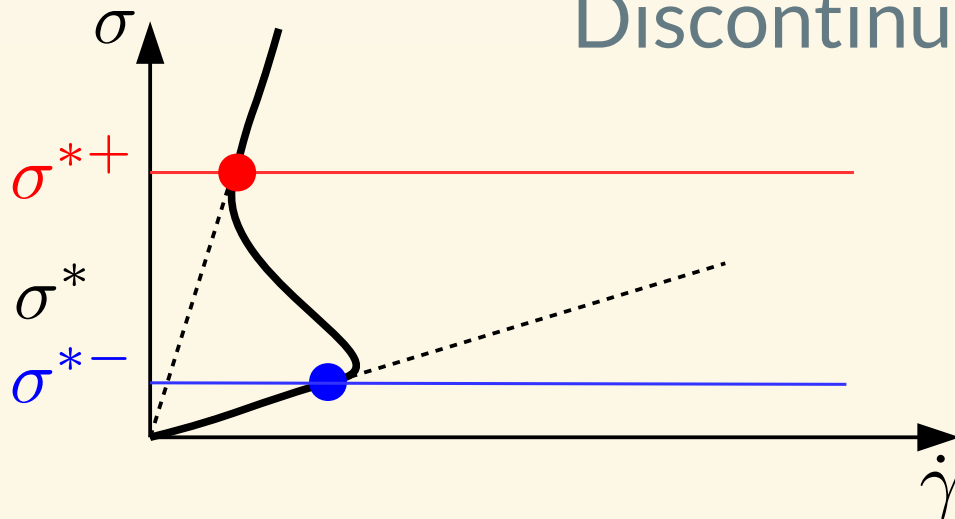


THICKENING SCENARIO

[Wyart & Cates, PRL 2014]

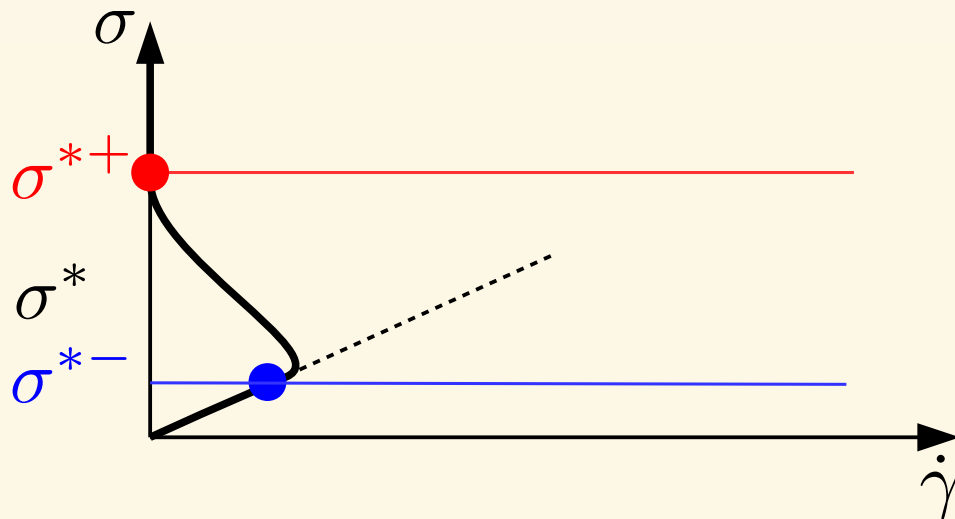
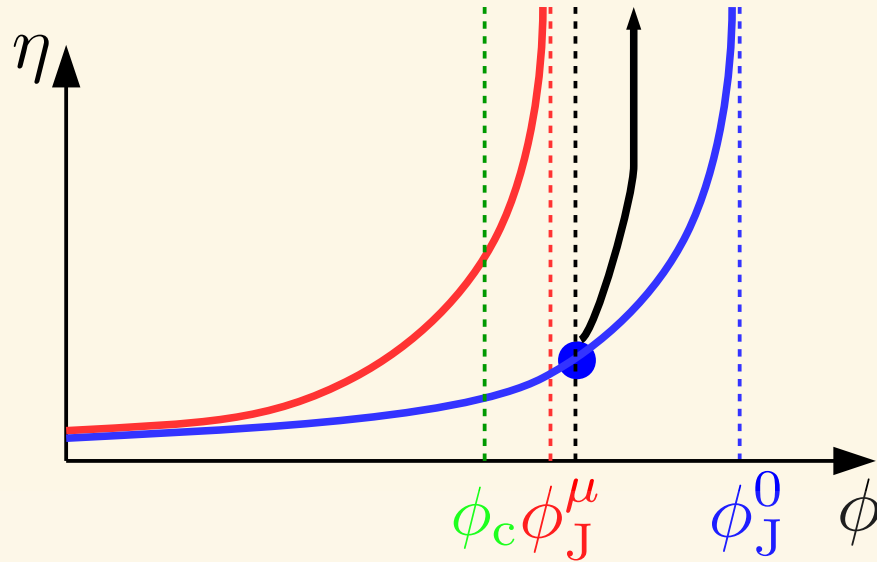


Discontinuous Shear Thickening



THICKENING SCENARIO

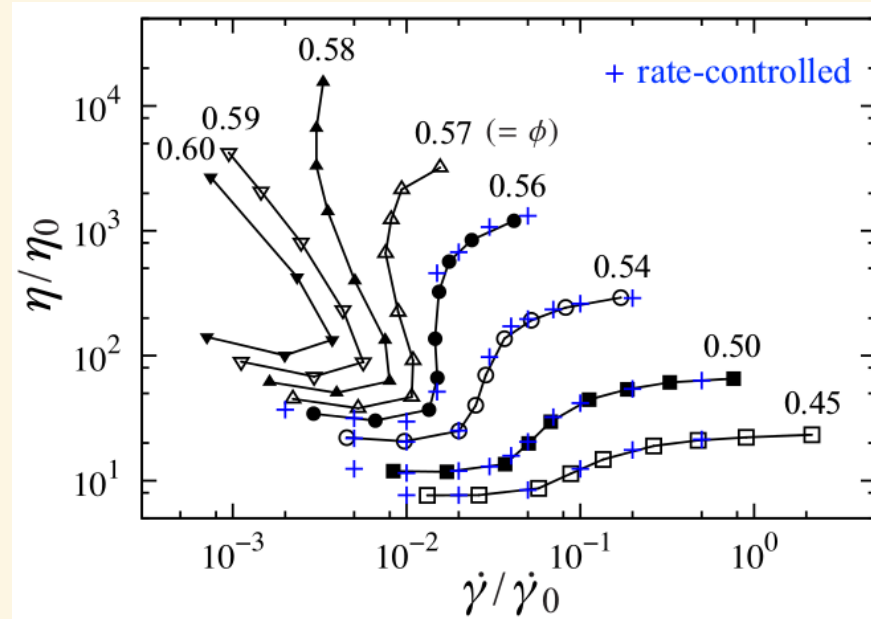
[Wyart & Cates, PRL 2014]



Shear Jamming

STRESS-CONTROLLED SIMULATIONS

[Mari, Seto, Morris & Denn, PRE 2015]



Non-monotonic flow curves:

- S-shaped (discontinuous thickening)
- Arches (shear jamming)

WYART-CATES MODEL

[Wyart & Cates, PRL 2014]

"Minimal constitutive model" with qualitative features of ST:

$$\sigma = \eta(\phi, f)\dot{\gamma}$$

$$\eta(\phi, f) = \eta_0(\phi_J(f) - \phi)^{-2}$$

$$\phi_J(f) = f\phi_J^\mu + (1 - f)\phi_J^0$$

$$f = f(\sigma)$$

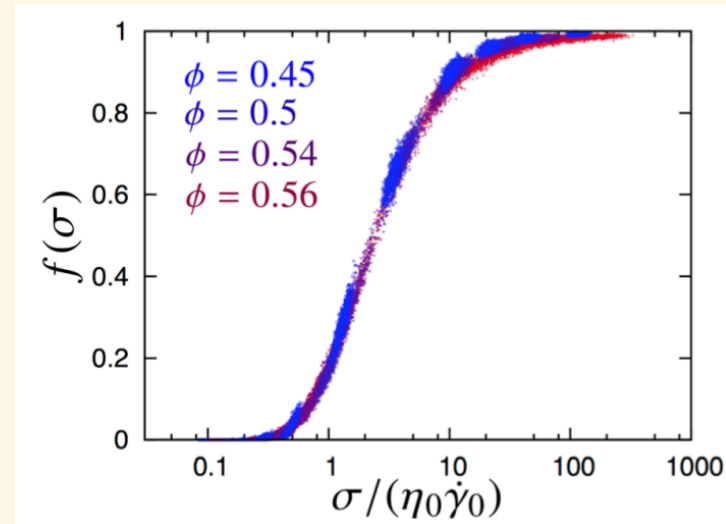
In practice,

$$f(\sigma) \approx \exp(-C\sigma^*/\sigma)$$

f : "fraction of frictional contacts"

$f = 0$: only lubricated contacts

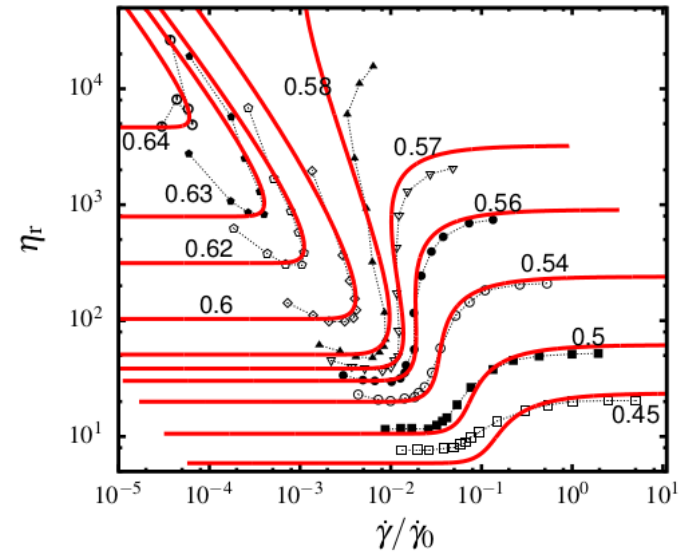
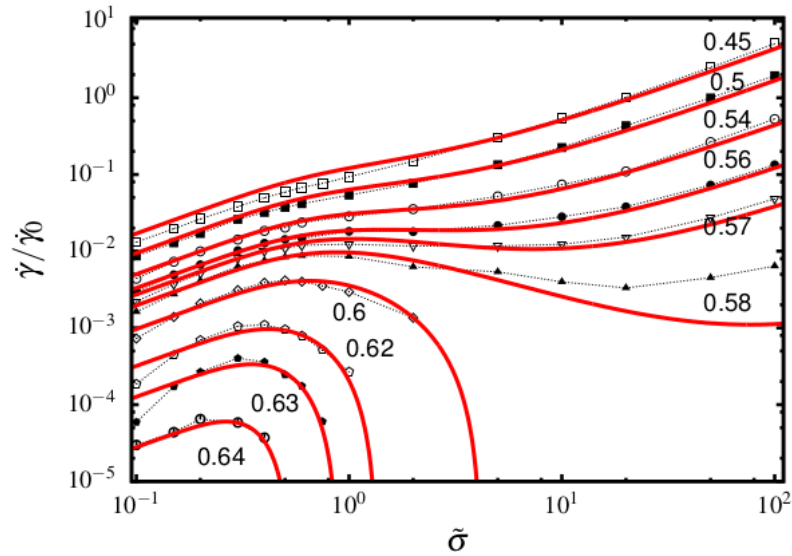
$f = 1$: only frictional contacts



WYART-CATES MODEL

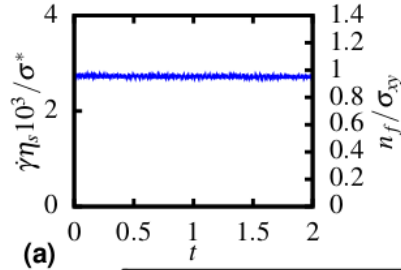
[Singh, Mari, Morri & Denn, JoR 2018]

Comparison with simulations

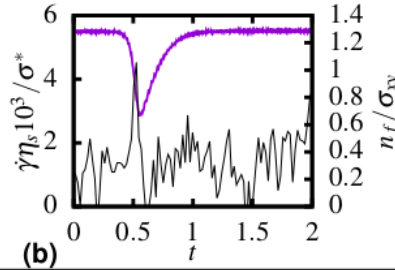


FLOW INSTABILITIES

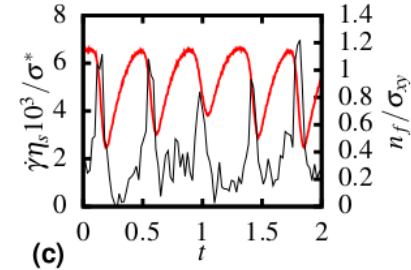
[Hermes et al, 2015]



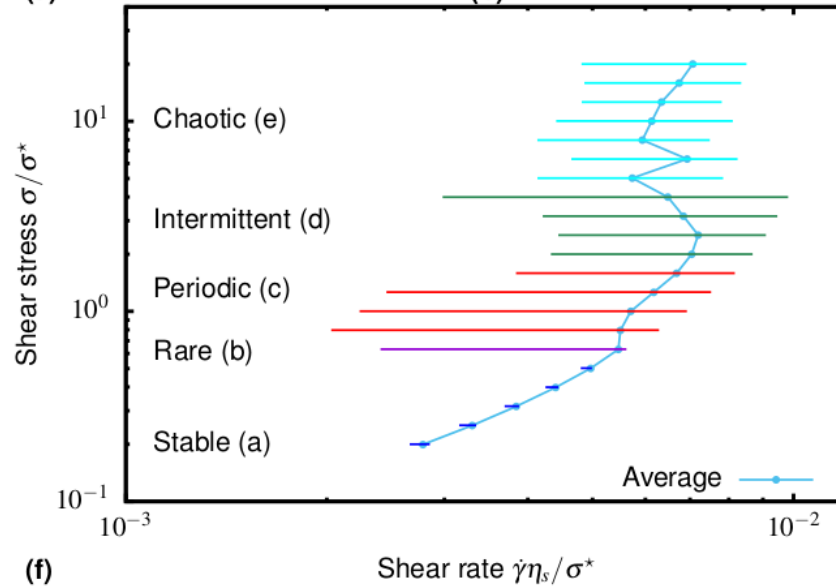
(a)



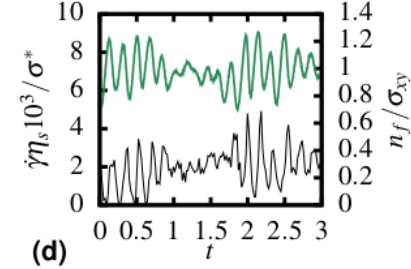
(b)



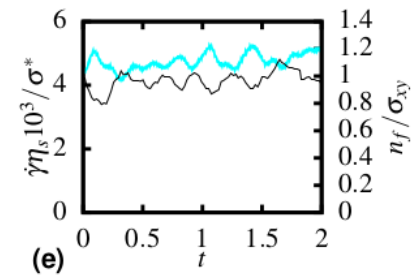
(c)



(f)

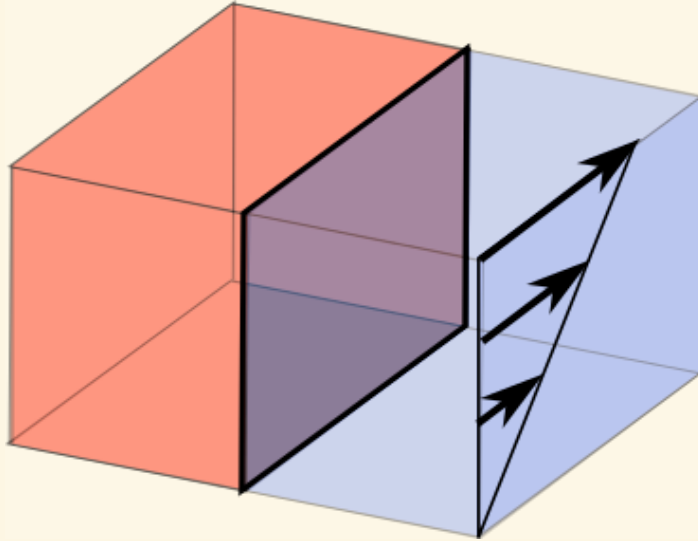


(d)



(e)

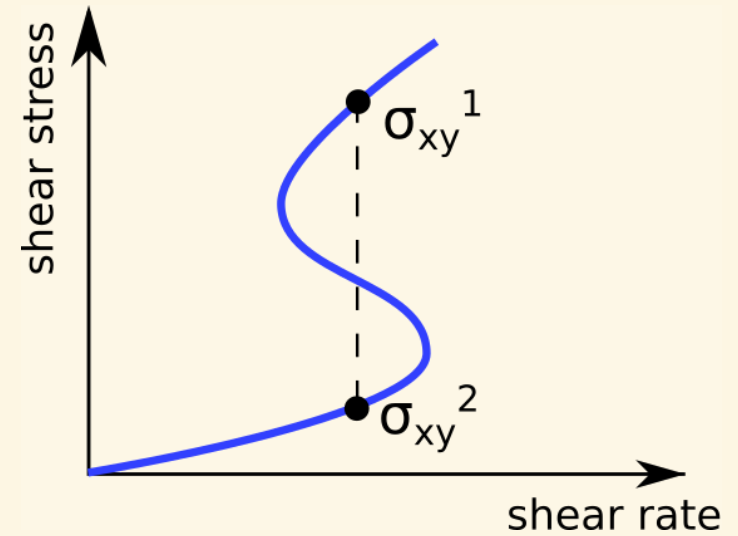
STEADY VORTICITY BANDING



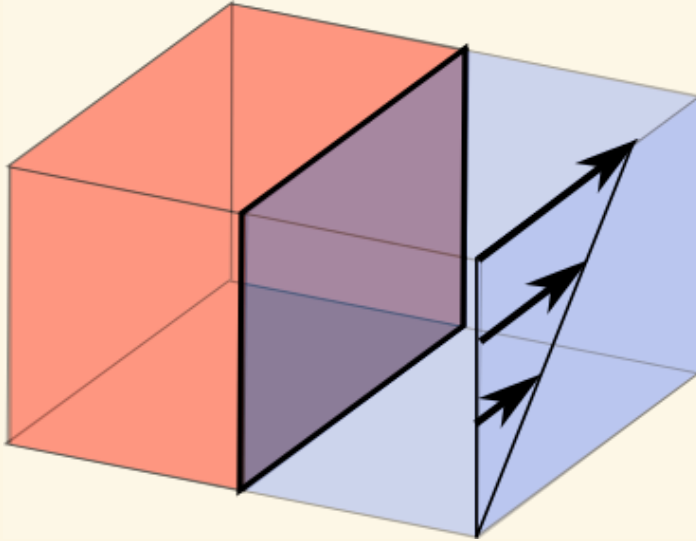
At the interface:

$$\sigma_{zz}^{(1)} = \sigma_{zz}^{(2)}$$

$$\dot{\gamma}^{(1)} = \dot{\gamma}^{(2)}$$



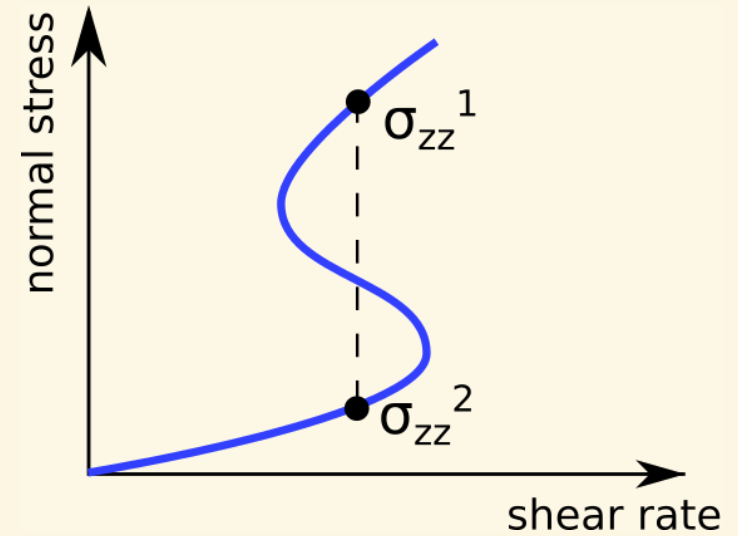
STEADY VORTICITY BANDING



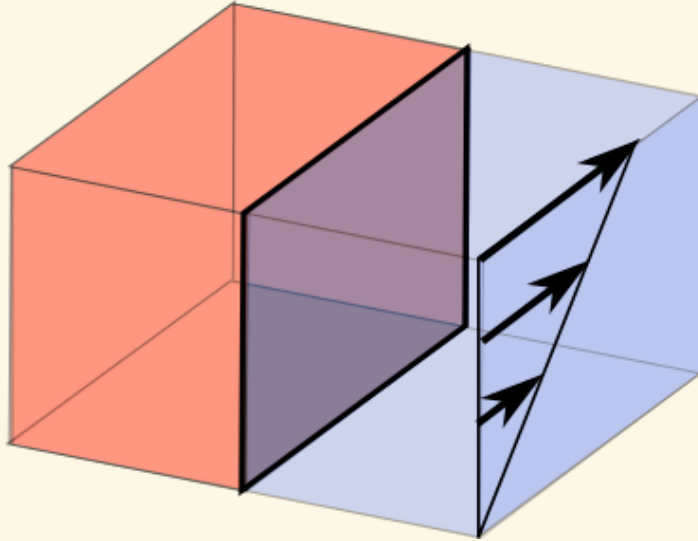
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STEADY VORTICITY BANDING

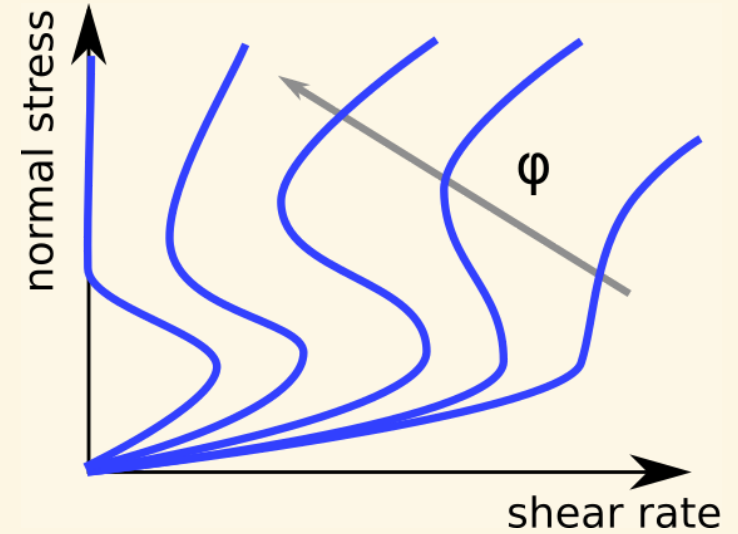


Impossible!

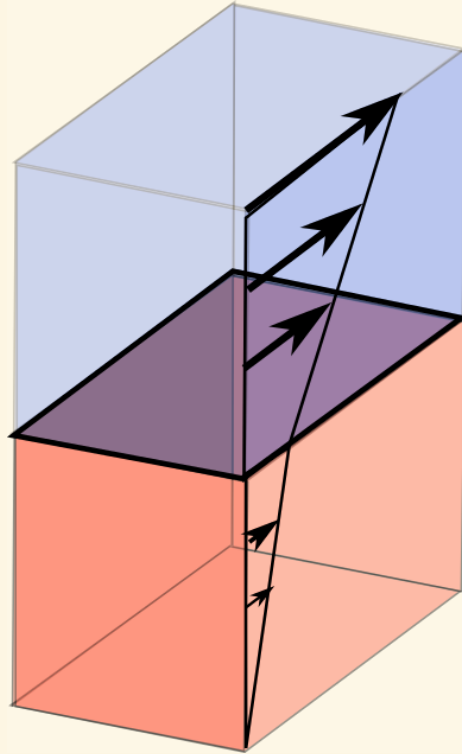
At the interface:

$$\sigma_{zz}^{(1)} = \sigma_{zz}^{(2)}$$

$$\dot{\gamma}^{(1)} = \dot{\gamma}^{(2)}$$



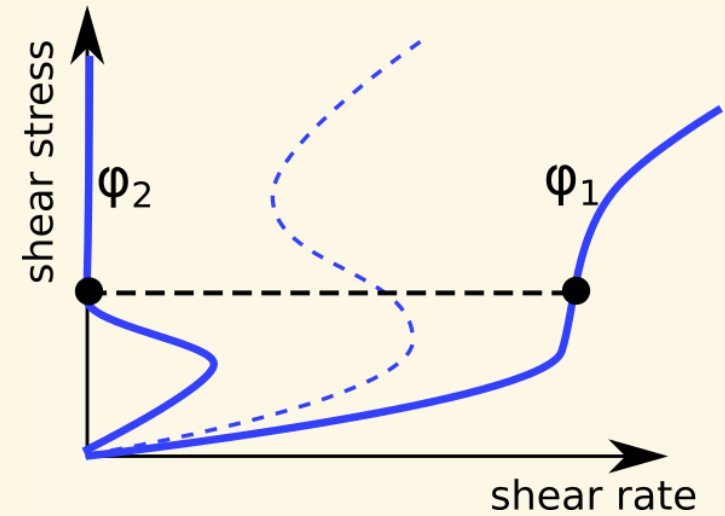
STEADY GRADIENT BANDING



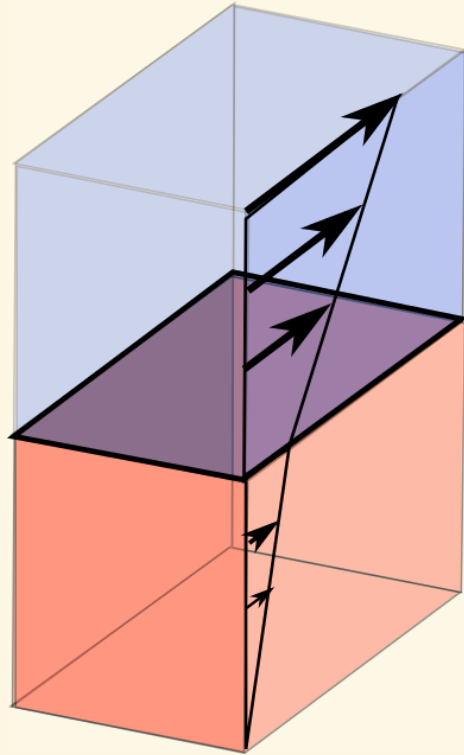
At the interface:

$$\sigma_{xy}^{(1)} = \sigma_{xy}^{(2)}$$

$$\sigma_{yy}^{(1)} = \sigma_{yy}^{(2)}$$



STEADY GRADIENT BANDING



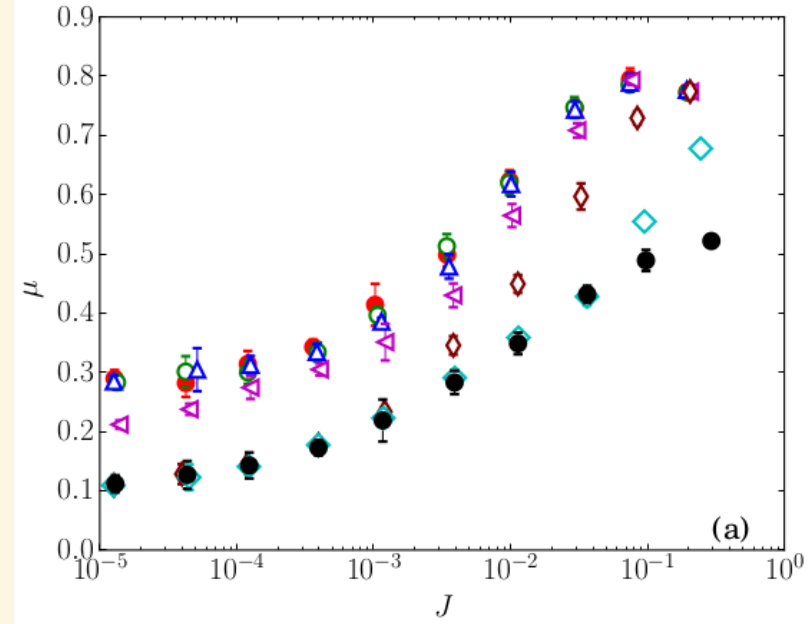
Impossible!

At the interface:

$$\sigma_{xy}^{(1)} = \sigma_{xy}^{(2)}$$

$$\sigma_{yy}^{(1)} = \sigma_{yy}^{(2)}$$

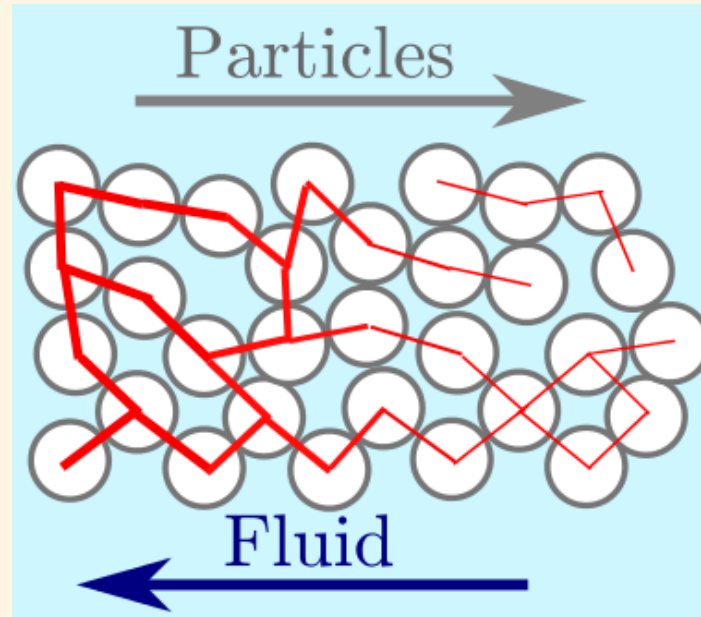
[Dong & Trulsson, Phys. Rev. Fluids 2017]



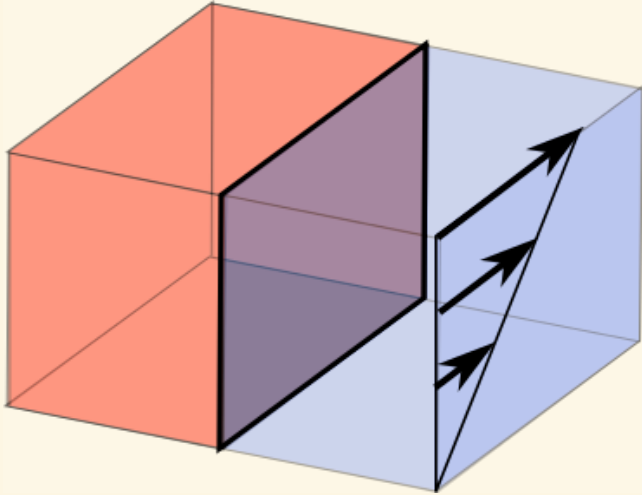
BANDING AND PARTICLE MIGRATION

Suspension balance model [Nott & Brady, JFM 1994]:

$$\nabla \cdot \Sigma^p = \phi R(\phi)(\mathbf{v}^p - \mathbf{v}^{p+f})$$



VORTICITY INSTABILITY MODEL



Reducing the problem to 1d

$$\Sigma \rightarrow \sigma_{zz} \equiv \sigma$$

$$\mathbf{v} \rightarrow v_z \equiv v$$

Conservation relations

Mass conservation:

$$\partial_t \phi + \partial_z (\phi v) = 0$$

Momentum conservation:

$$\partial_z \sigma = -R \phi v$$

Stress control:

$$L_z^{-1} \int dz \sigma = \bar{\sigma}$$

Constitutive model:

Wyart-Cates + linear response:

$$\sigma = \eta(\phi, f) \dot{\gamma}$$

$$\eta(\phi, f) = \eta_0 (\phi_J(f) - \phi)^{-2}$$

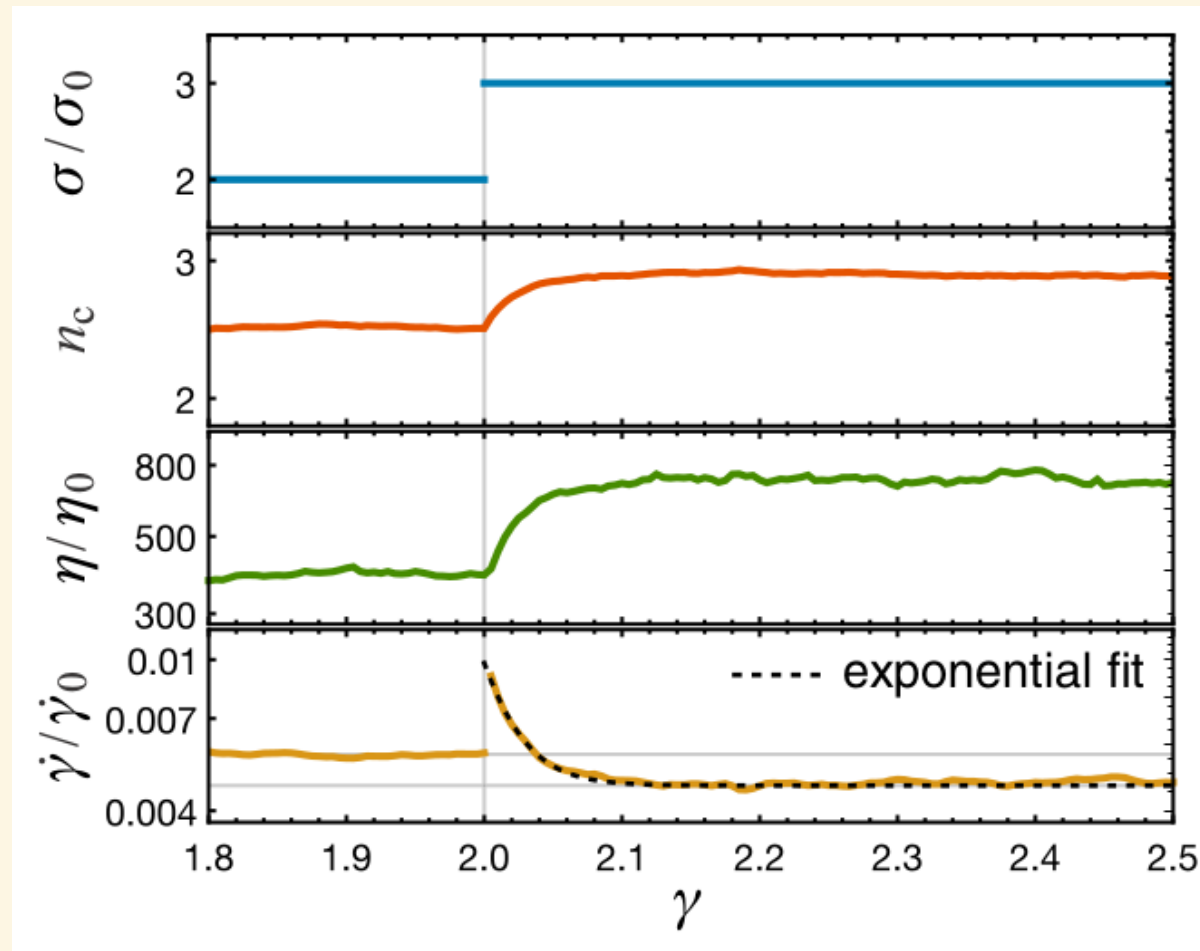
$$\phi_J(f) = f \phi_J^\mu + (1 - f) \phi_J^0$$

$$\partial_t f = -\dot{\gamma} \gamma_0^{-1} [f - f^*(\sigma)]$$

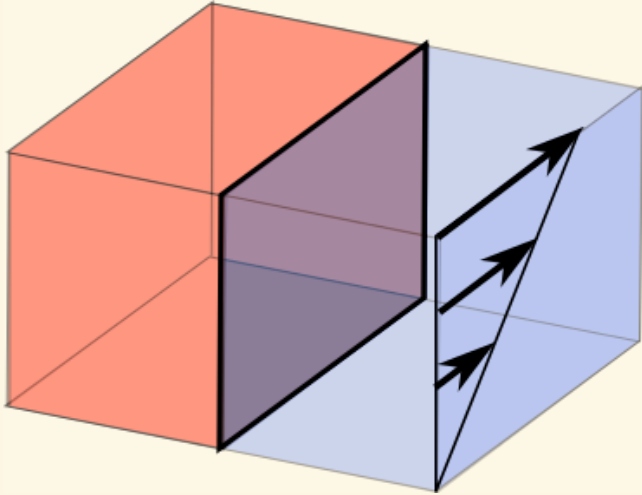
$$f^*(\sigma) = \exp(-\sigma^* / \sigma)$$

LINEAR RESPONSE OF THE MICROSTRUCTURE

[Mari, Seto, Morris & Denn, PRE 2015]



VORTICITY INSTABILITY MODEL



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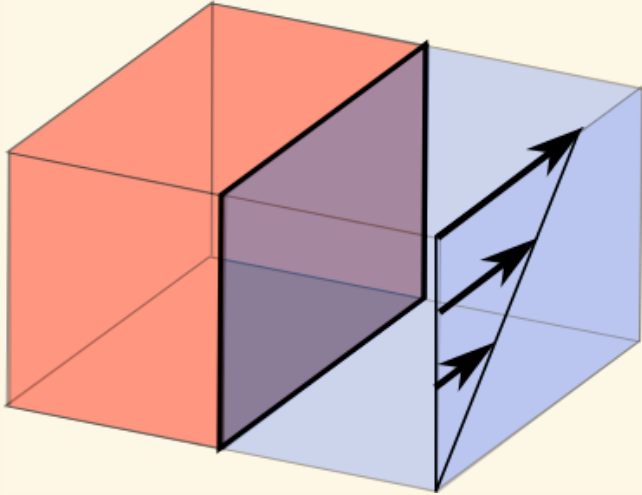
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$$\partial_t f = -\dot{\gamma} \gamma_0^{-1} [f - f^*(\sigma)]$$

$$f^*(\sigma) = \exp(-\sigma^* / \sigma)$$

VORTICITY INSTABILITY MODEL



Reducing the problem to 1d

$$\Sigma \rightarrow \sigma_{zz} \equiv \sigma$$

$$\mathbf{v} \rightarrow v_z \equiv v$$

Coupled dynamical equations

$$\partial_t \phi = R^{-1} \partial_z^2 \sigma$$

$$\partial_t f = -\dot{\gamma} \gamma_0^{-1} [f - f^*(\sigma)]$$

Coupling through:

$$\sigma = \eta(\phi, f) \dot{\gamma}$$

$$\eta(\phi, f) = \eta_0 (\phi_J(f) - \phi)^{-2}$$

$$\phi_J(f) = f \phi_J^\mu + (1 - f) \phi_J^0$$

$$f^*(\sigma) = \exp(-\sigma^* / \sigma)$$

$$L_z^{-1} \int dz \sigma = \bar{\sigma}$$

VORTICITY INSTABILITY MODEL

Non-dimensionalize with units:

- Time η_0 / σ^*
- Length L_z
- Stress σ^*

Change of variables:

- $t \rightarrow s = \gamma_0^{-1} t$
- $R \rightarrow \alpha = \gamma_0^{-1} R$

Coupled dynamical equations

$$\partial_s \phi = \alpha^{-1} \partial_z^2 \sigma$$

$$\partial_s f = -\dot{\gamma} [f - f^*(\sigma)]$$

Coupling through:

$$\sigma = \eta(\phi, f) \dot{\gamma}$$

$$\eta(\phi, f) = (\phi_J(f) - \phi)^{-2}$$

$$\phi_J(f) = f \phi_J^\mu + (1 - f) \phi_J^0$$

$$f^*(\sigma) = \exp(-1/\sigma)$$

$$\int dz \sigma = \bar{\sigma}$$

3 parameters: $\bar{\phi}, \bar{\sigma}, \alpha = L_z^2 R / (\gamma_0 \eta_0) \gg 1$

VORTICITY INSTABILITY MODEL

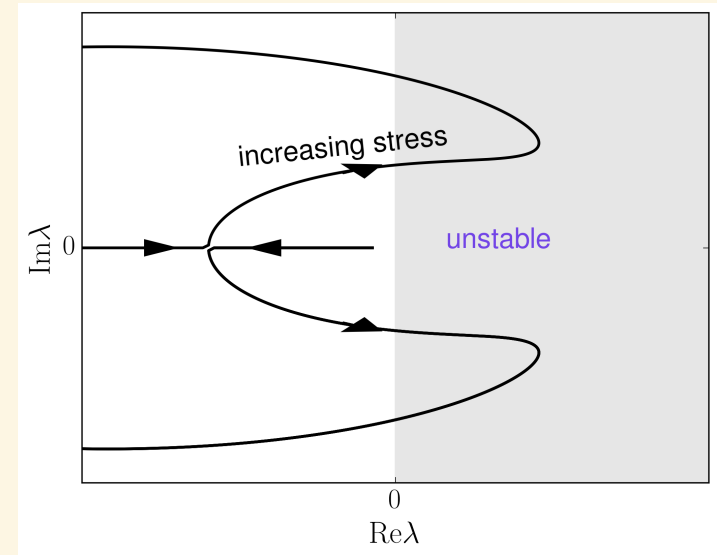
Linear stability analysis:

$$X = X_0 + \delta X e^{ikz + \lambda t}$$

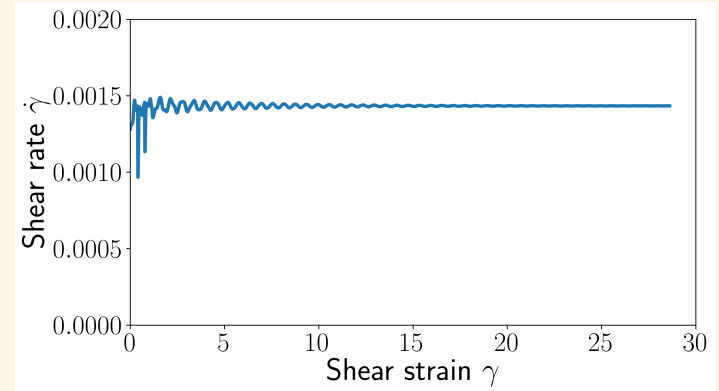
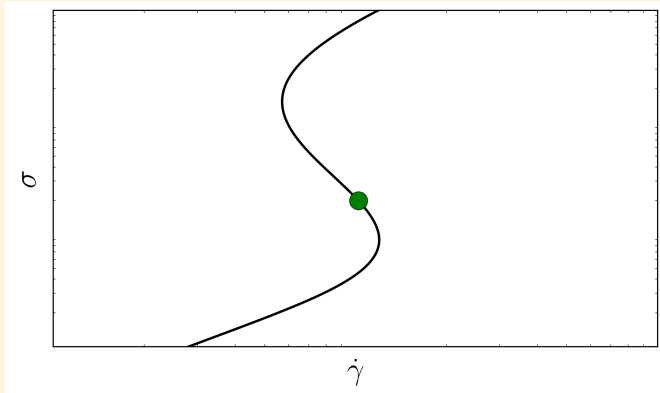
Unstable when $\eta \partial_\sigma \dot{\gamma} < -\frac{k^2}{\phi \alpha} \partial_\phi \eta$

Hopf bifurcation, $\text{Re}\lambda > 0$ and
 $\text{Im}\lambda \neq 0$

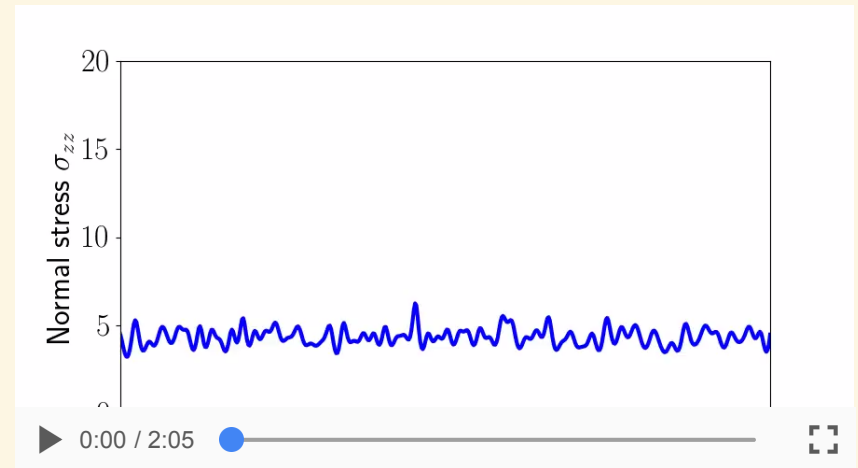
Instability towards *traveling bands*

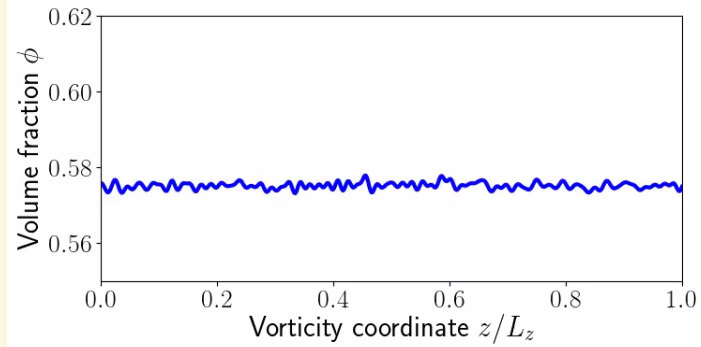
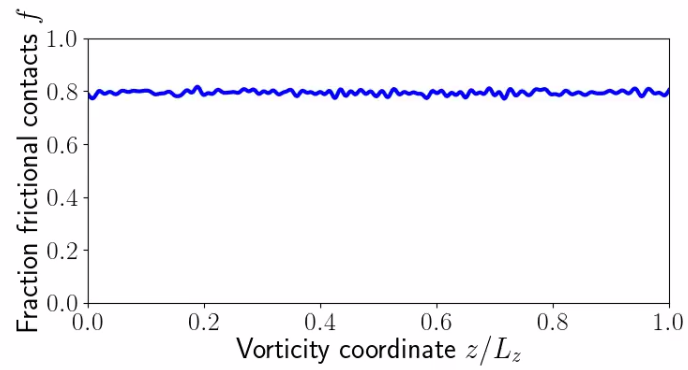
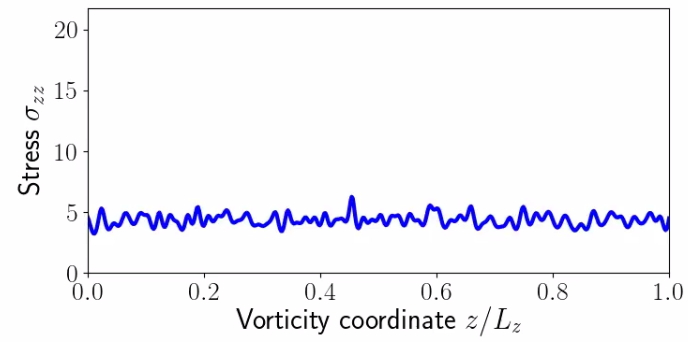


TRAVELING BANDS



Stress field along vorticity

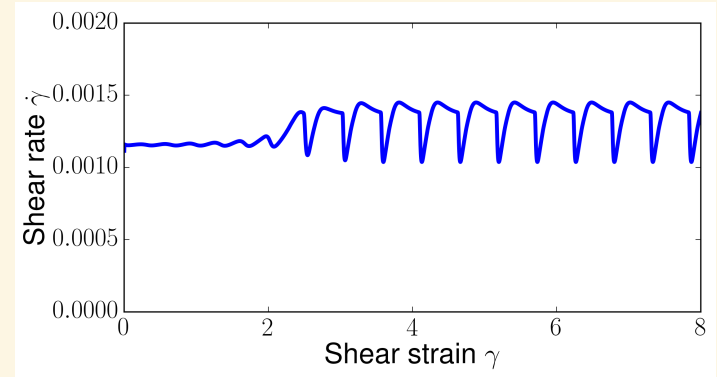
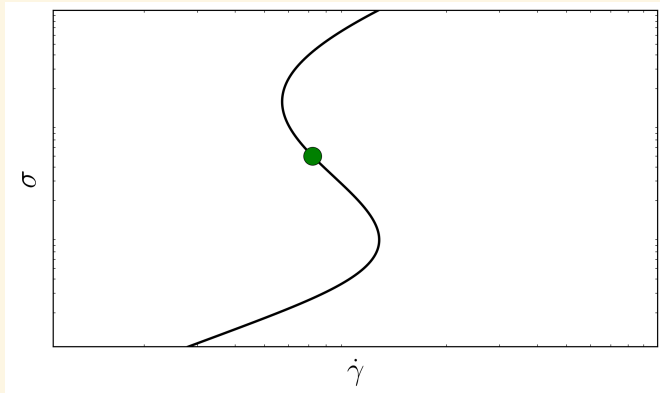




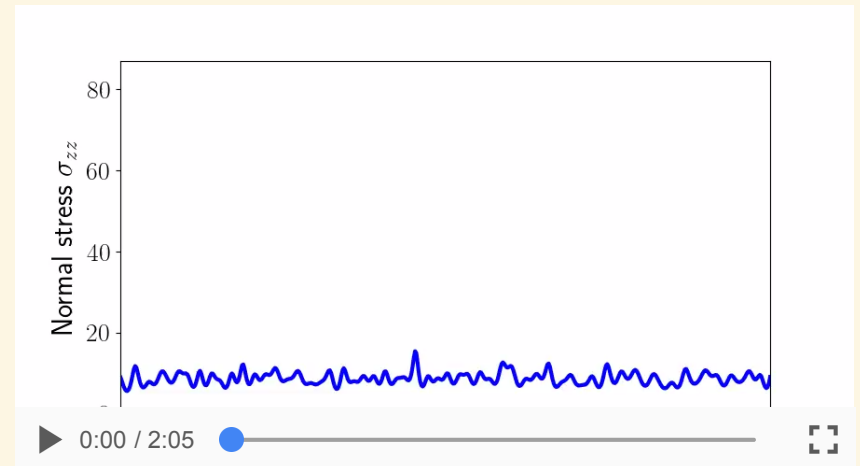
0:00 / 2:05

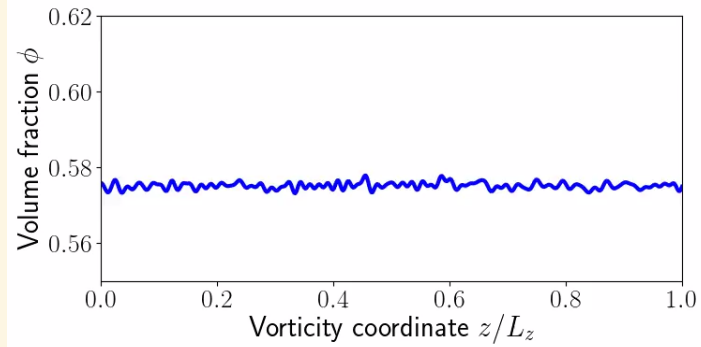
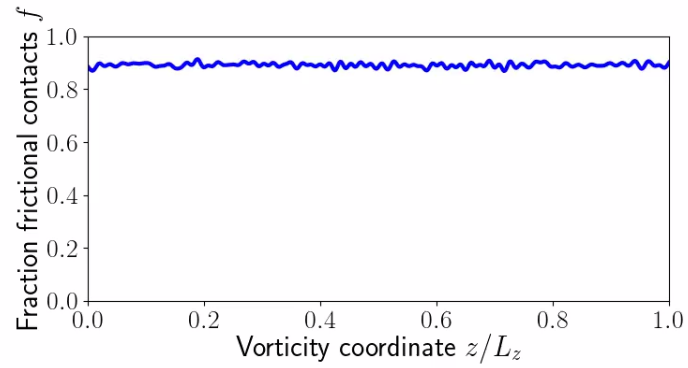
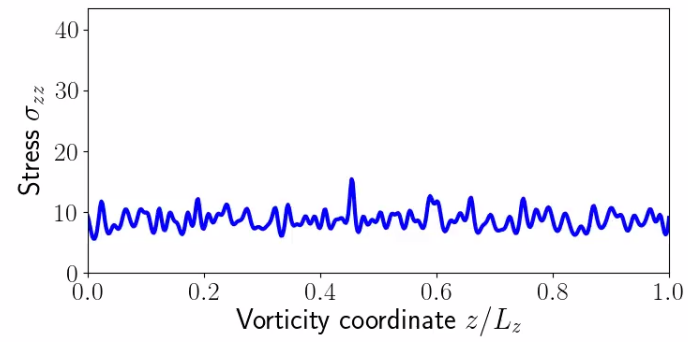


TRAVELING BANDS



Stress field along vorticity

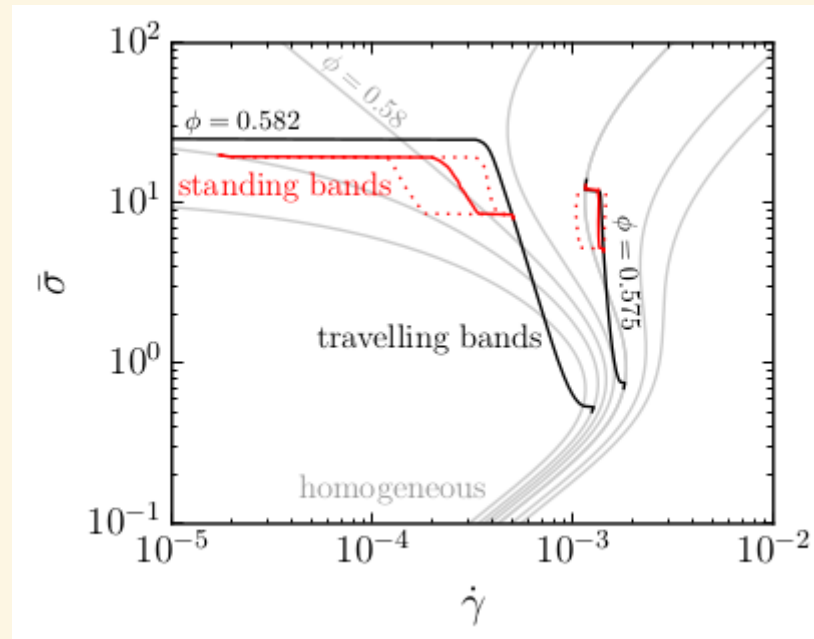




0:00 / 2:05



COMPOSITE FLOW CURVES

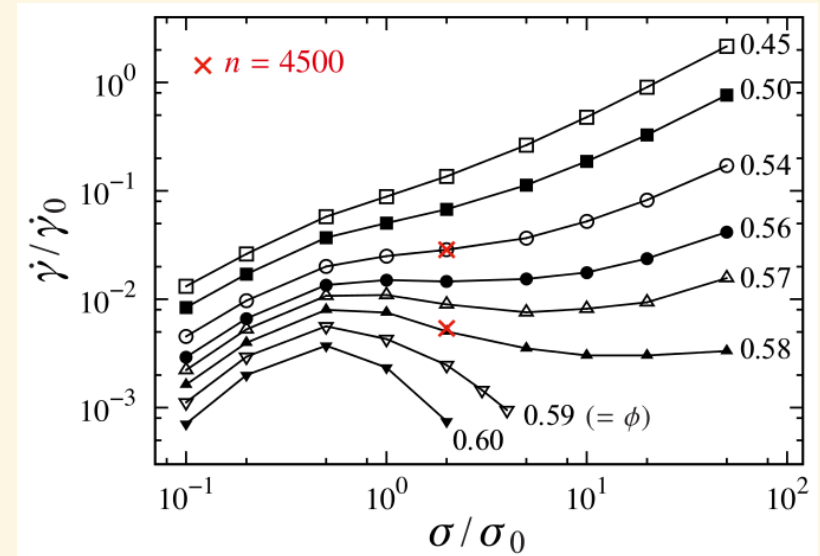


DEM + LUBRICATION SIMULATIONS

Instability for:

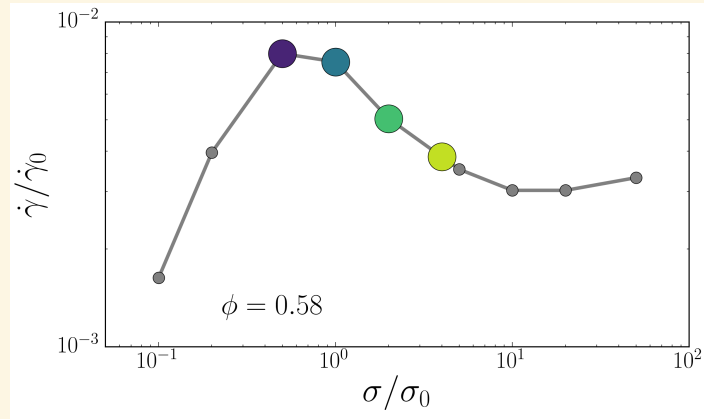
$$\eta \partial_{\sigma} \dot{\gamma} < -\frac{k^2 \gamma_0}{\phi \alpha} \partial_{\phi} \eta$$

Need $L_z/a \gtrsim 100$



Simulations with very large aspect ratio in favor of the vorticity

DEM + LUBRICATION SIMULATIONS



$$\sigma/\sigma^* = 0.5$$

▶ 0:00 / 0:09



$$\sigma/\sigma^* = 1$$

▶ 0:00 / 0:15



$$\sigma/\sigma^* = 2$$

▶ 0:00 / 0:04



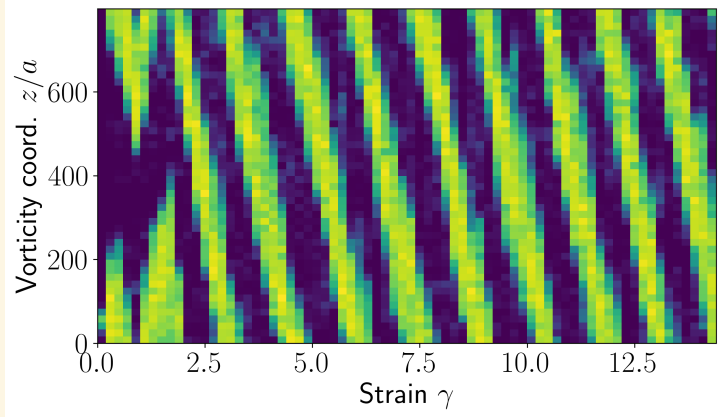
$$\sigma/\sigma^* = 4$$

▶ 0:00 / 0:01

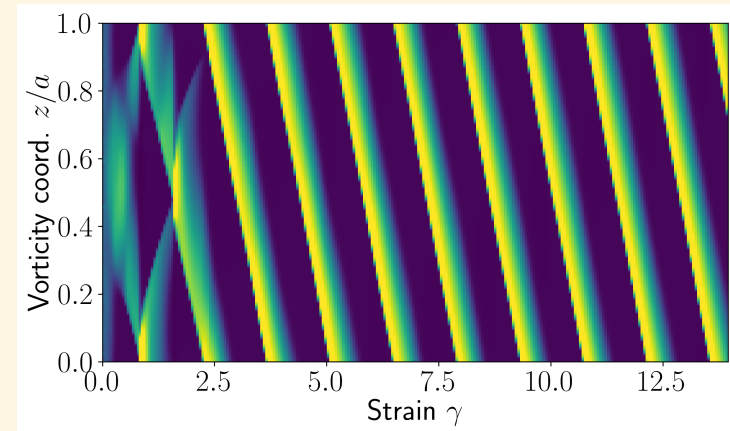
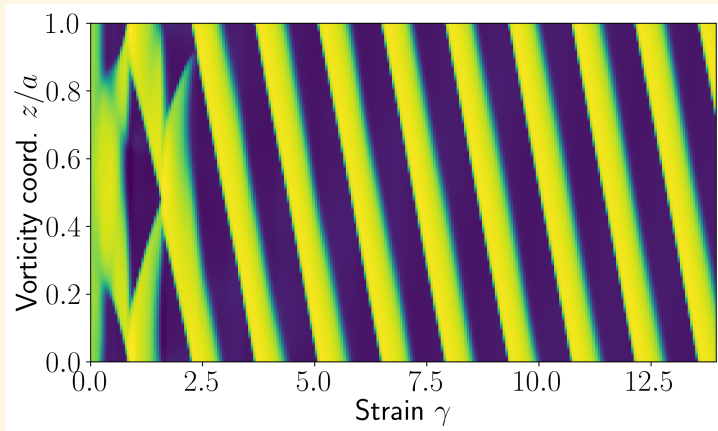
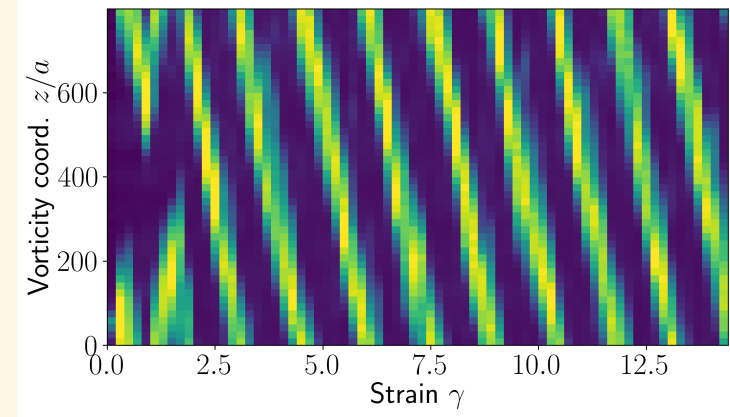


COMPARISON WITH MODEL

Friction field

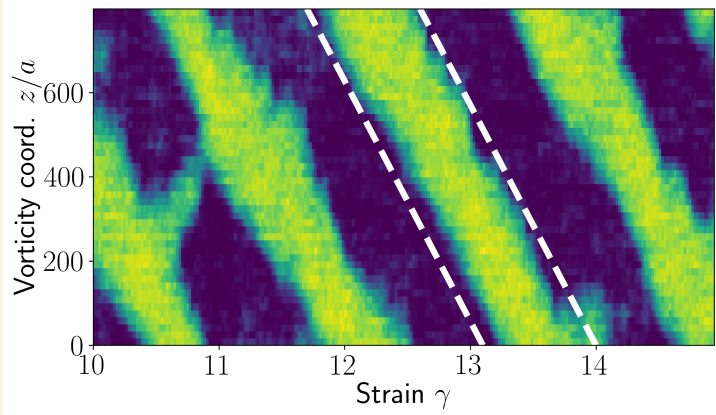


Stress field

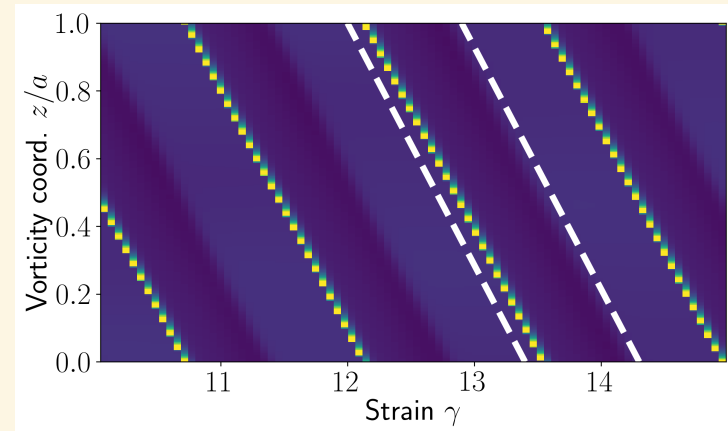
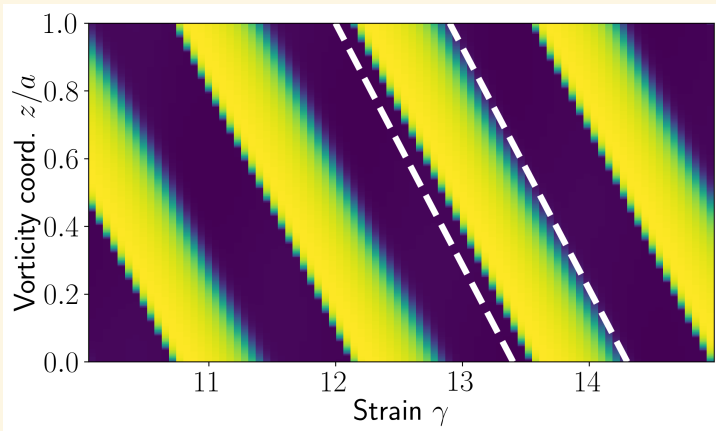
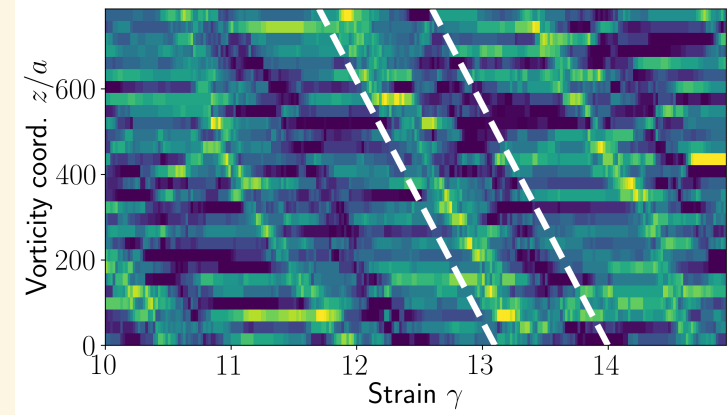


COMPARISON WITH MODEL

Friction field

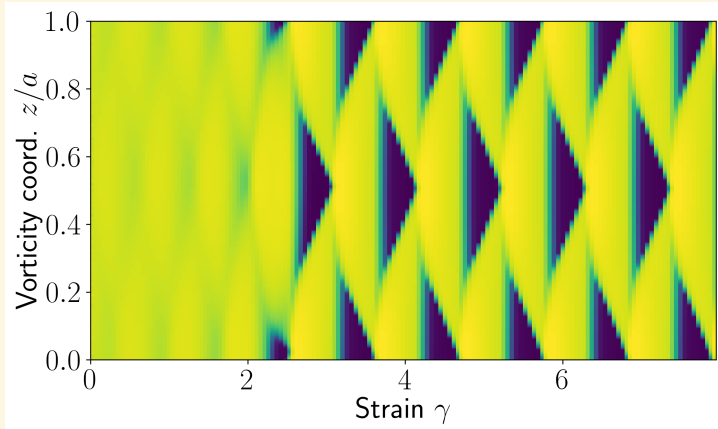
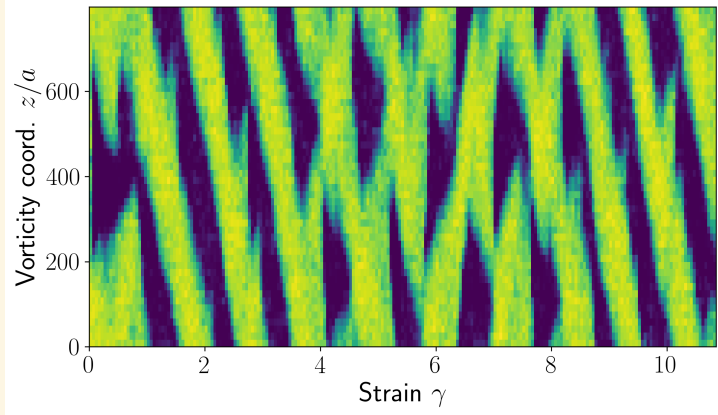


Volume fraction field

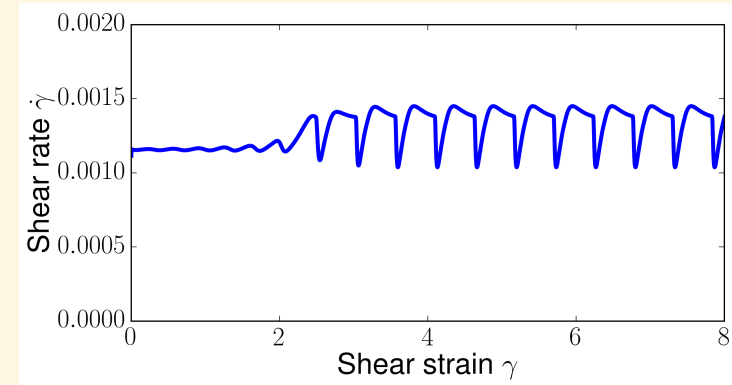
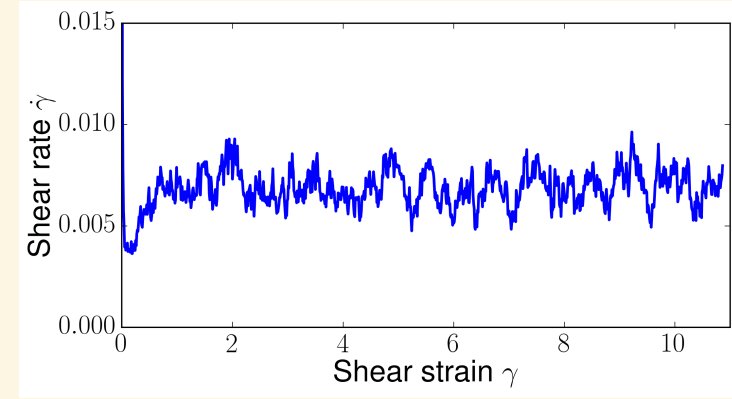


TWO-BAND STATE?

Friction field

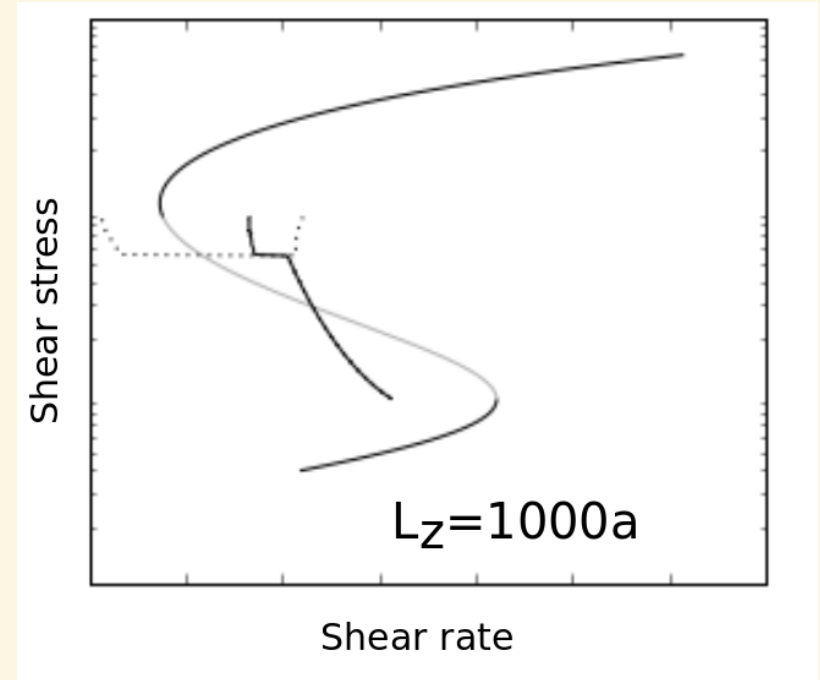
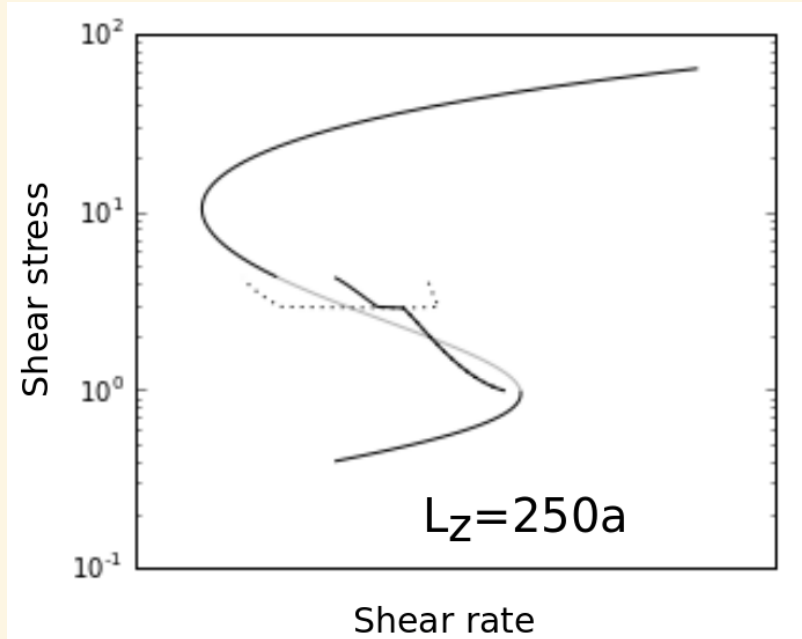


Strain rate



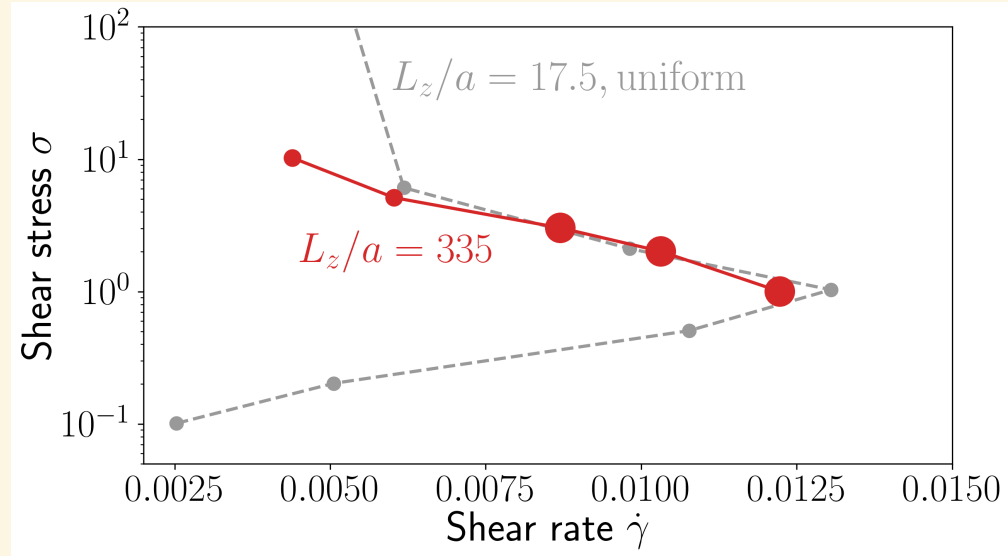
FLOW CURVES

Model



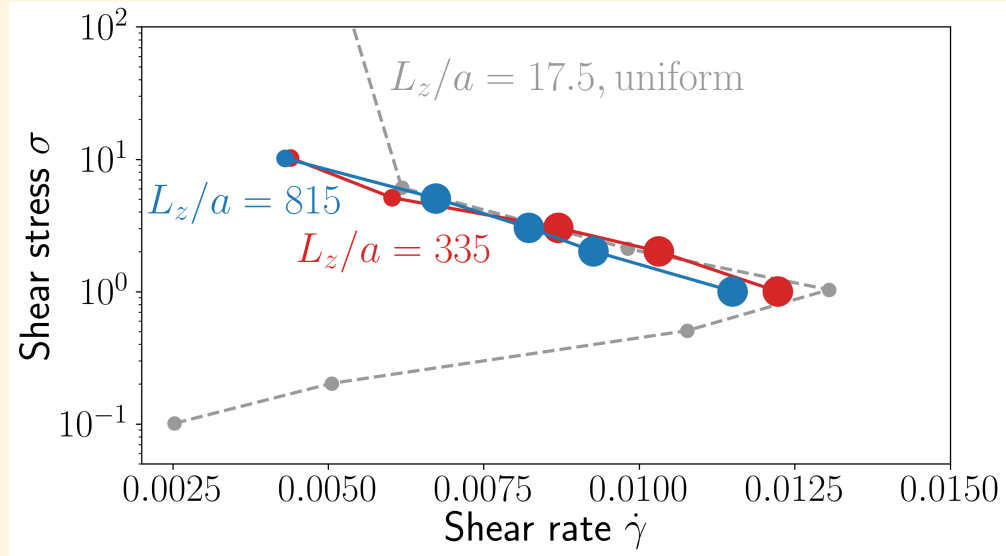
COMPARISON WITH MODEL

Simulations



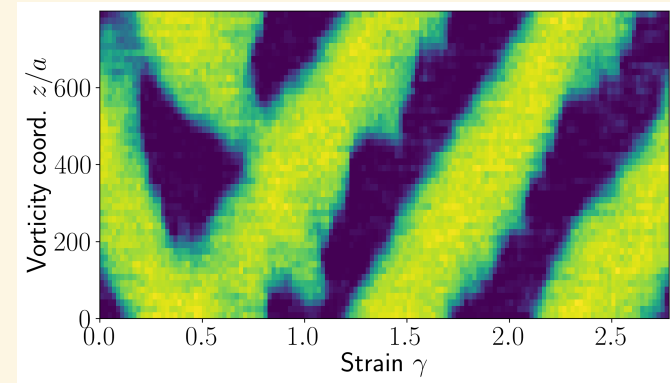
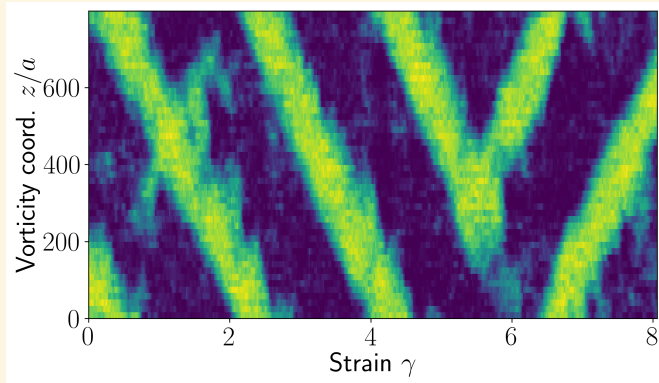
COMPARISON WITH MODEL

Simulations

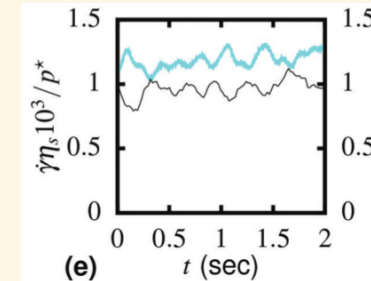
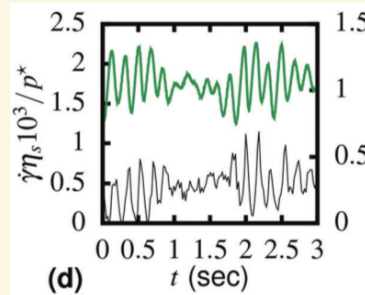
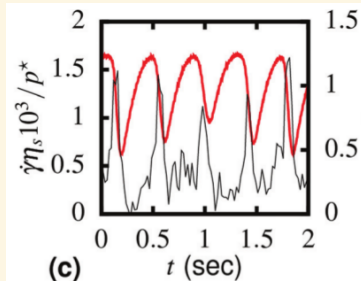


SOME OPEN QUESTIONS

- Two-band state in simulations?
- Some simulation events not captured, role of "noise"?



- Where are the rare, intermittent and chaotic regimes of experiments?



- Boundary conditions (free surface, imposed normal stress?)