

# Viscous boundary layers in high Rayleigh number convection: A new insight from 3d velocity measurements

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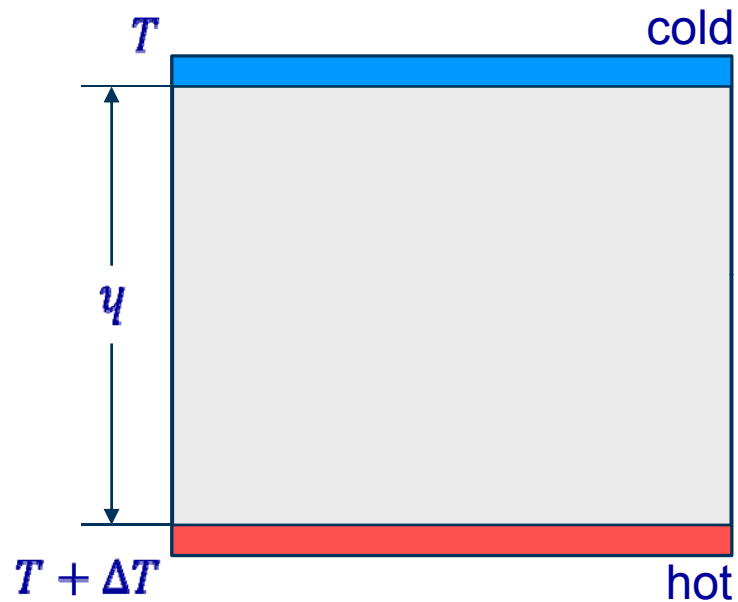


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## Outline

- **Technical news from the Barrel**
- **Present projects**
- **Viscous boundary layer measurements**

## Sketch of the RB problem



<u>Input:</u>	<u>Response:</u>
$Ra = \frac{\beta g \Delta \vartheta h^3}{\nu \kappa}$	$Nu = \frac{\dot{q}}{\dot{q}_d}$
$\Gamma = D/h$	$Re = U_\infty h/\nu$
$Pr = \nu/\kappa$	

## 1. Technical News

Two different ways to study Rayleigh Bénard convection:



### Global characteristics

- study of global quantities like heat flux, velocity, global flow structure, flow dynamics



- aims to predict scaling laws like  $Nu, Re = f(Ra, \Gamma, Pr)$

### Local details

- local details like boundary layers, local transport, turbulent dissipation



- looking for significant variations in the local flow fields, e.g transitions of the boundary layer structure

## Different philosophies to built up experiments:



### to study global characteristics

- maximum Ra numbers
- large parameter domains
- accurate measurements of the global quantities



- experiments in liquid Helium or compressed SF<sub>6</sub>
- disadvantage: limitations of local measurements

### to study local details

- large-scale experiments for high resolution
- small and (preferably) non-intrusive sensors



- experiments in air or water
- virtually unrestricted access for measurements

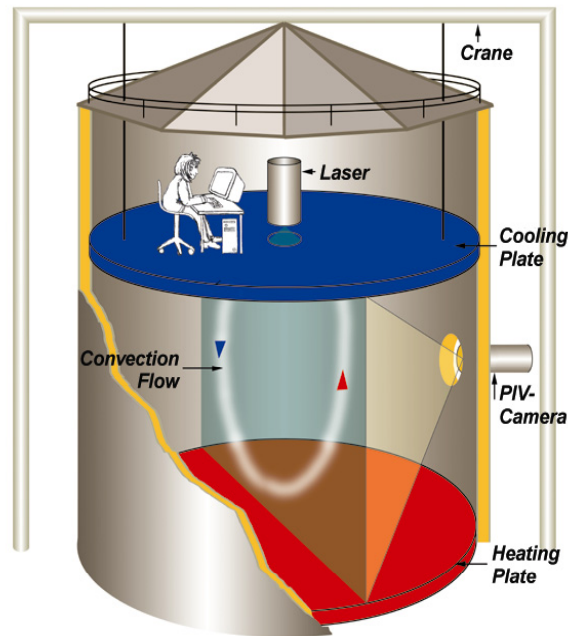
# BOI

Technical news

Present projects

Measurements

## The „Barrel of Ilmenau“ (BOI)



### Physical parameter:

$$Ra = \dots 10^{12}$$

$$\Gamma = 1.13 \dots 143$$

$$Pr = 0.7$$

$$Nu = \dots 1000$$

$$Re = \dots 250,000$$

### Technical data:

$$d = 7.15 \text{ m}$$

$$h = 0.05 \dots 6.30 \text{ m}$$

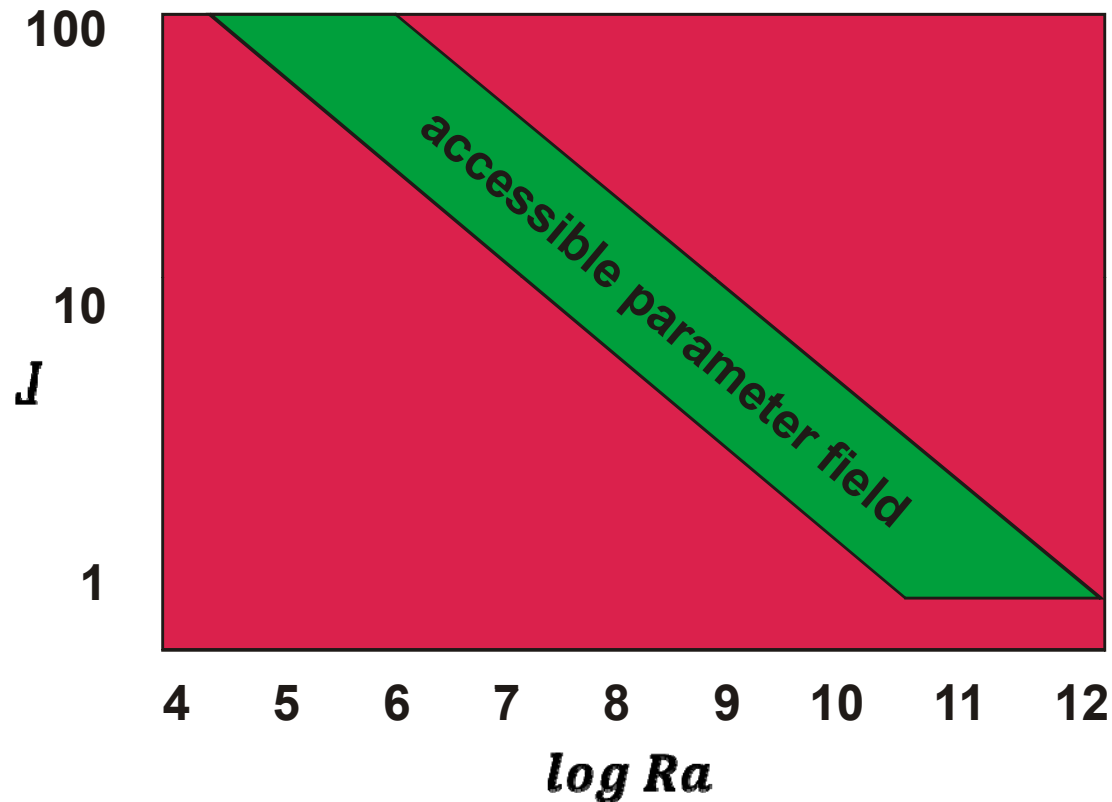
$$\Delta\vartheta = 2.5 \dots 60 \text{ K}$$

$$\dot{Q}_h = 10 \text{ kW}$$

$$\dot{Q}_c = 15 \text{ kW}$$

Even in the BOI it is of crucial interest to span a wide parameter range in  $Ra$  and  $\Gamma$

Accessible parameter field of the  $D=7.15$  m cell

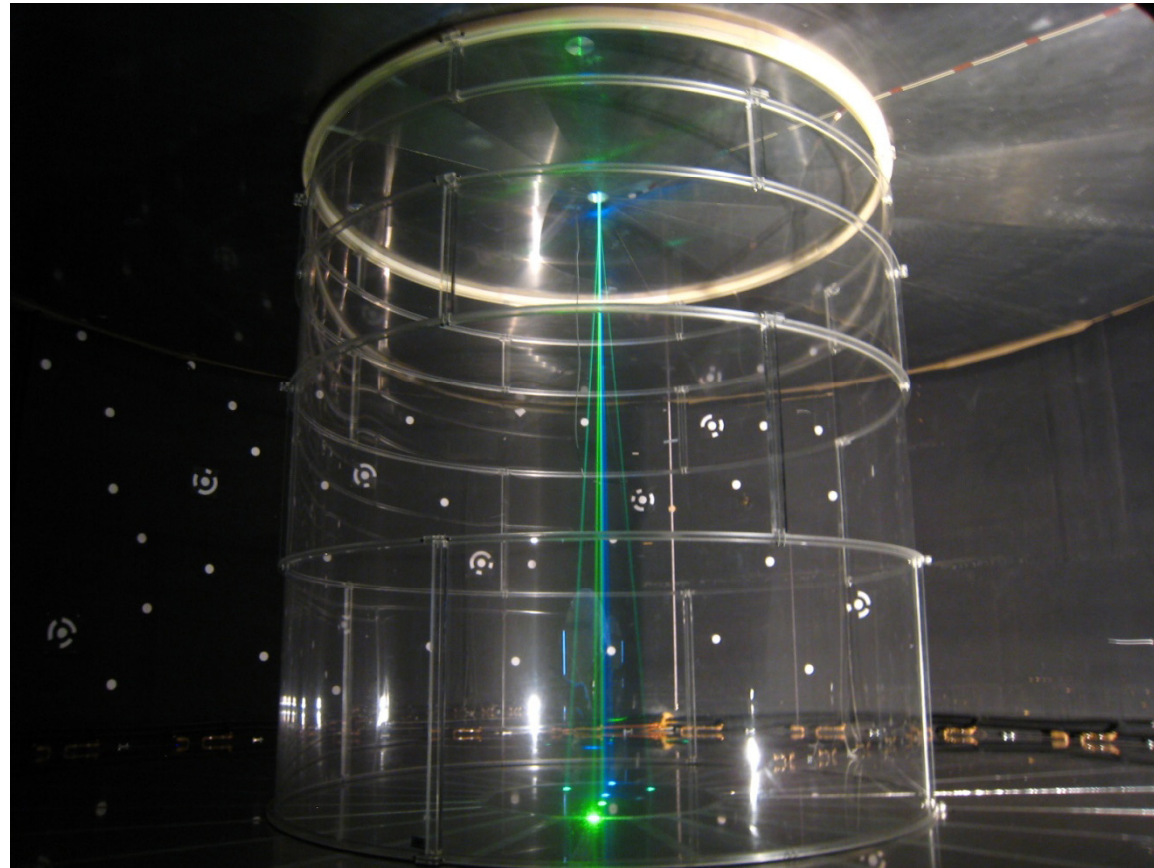


$$Ra = \frac{\beta g \Delta \vartheta h^3}{\nu \kappa}$$

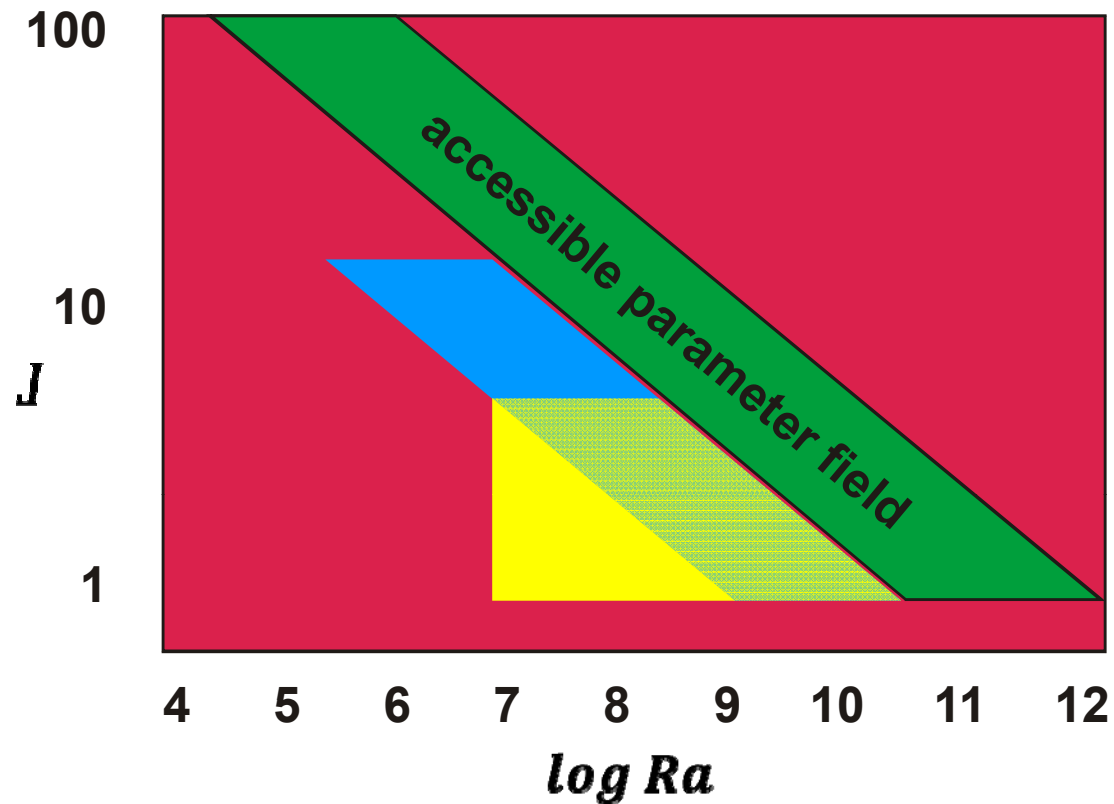
$$\Gamma = D/h$$

The domain in  $Ra$  for  $\Gamma = \text{const.}$  is limited to 1.5 decades!  
The variation in  $\Gamma$  for constant  $Ra$  is limited to a factor of 2.5!

## Smaller inset of $D=2.5$ m in the big barrel







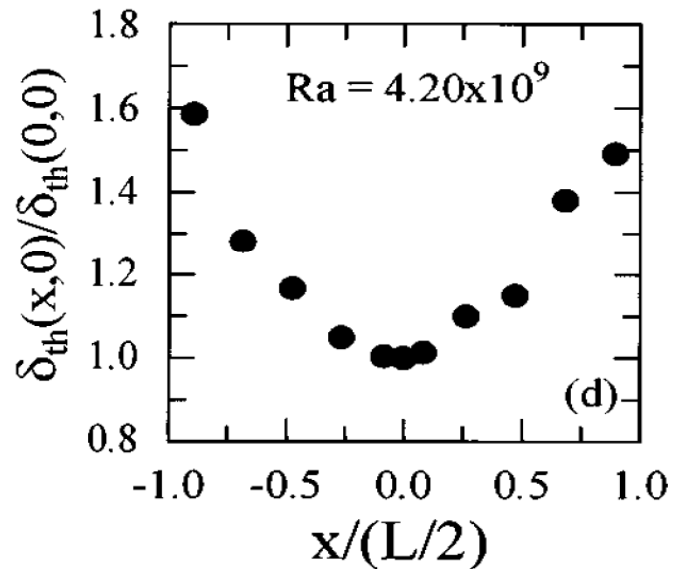
Accessible parameter field of:

- ✓  $D=7.15$  m sample (green)
- ✓  $D=2.50$  m sample (blue)
- ✓ Numerics (yellow)

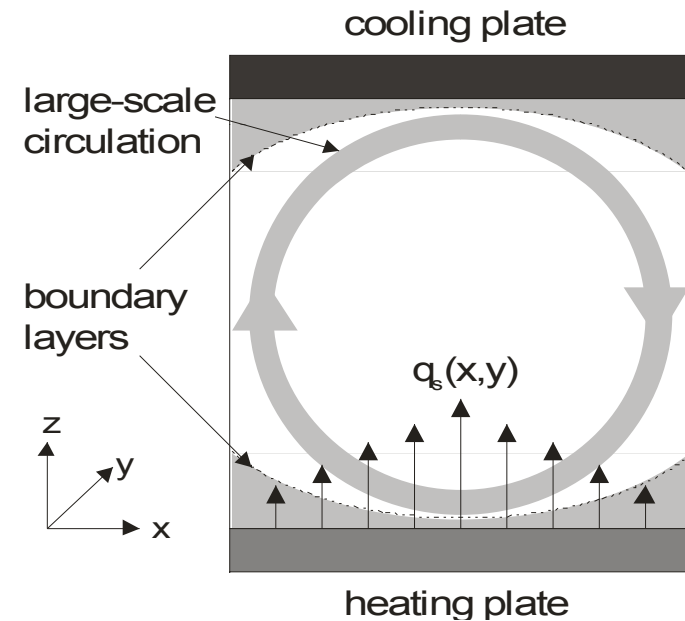
## 2. Present projects

„Local wall heat flux measurements“

Relative thickness of the thermal boundary layer at  $\Gamma=1$   
along the large-scale circulation

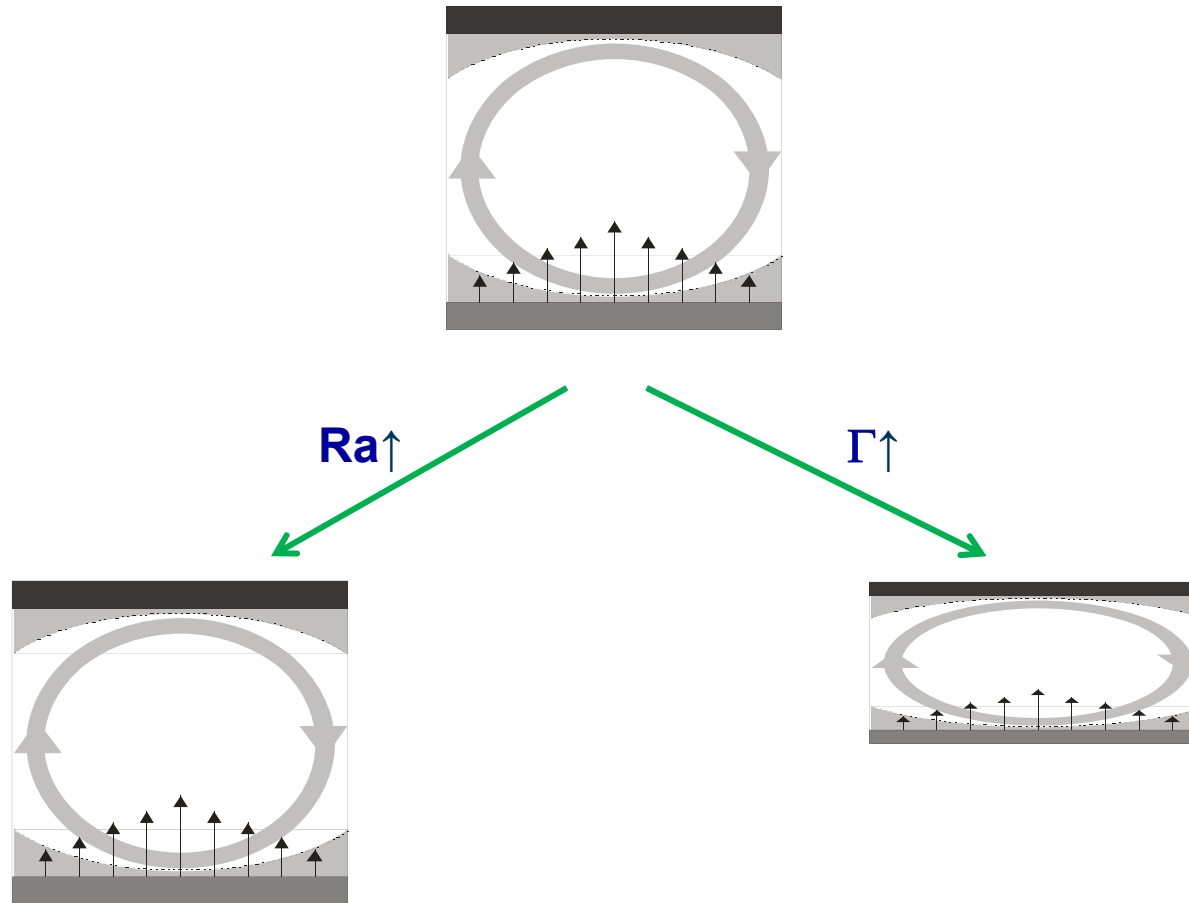


*Lui and Xia, PRE 57 (1998)*

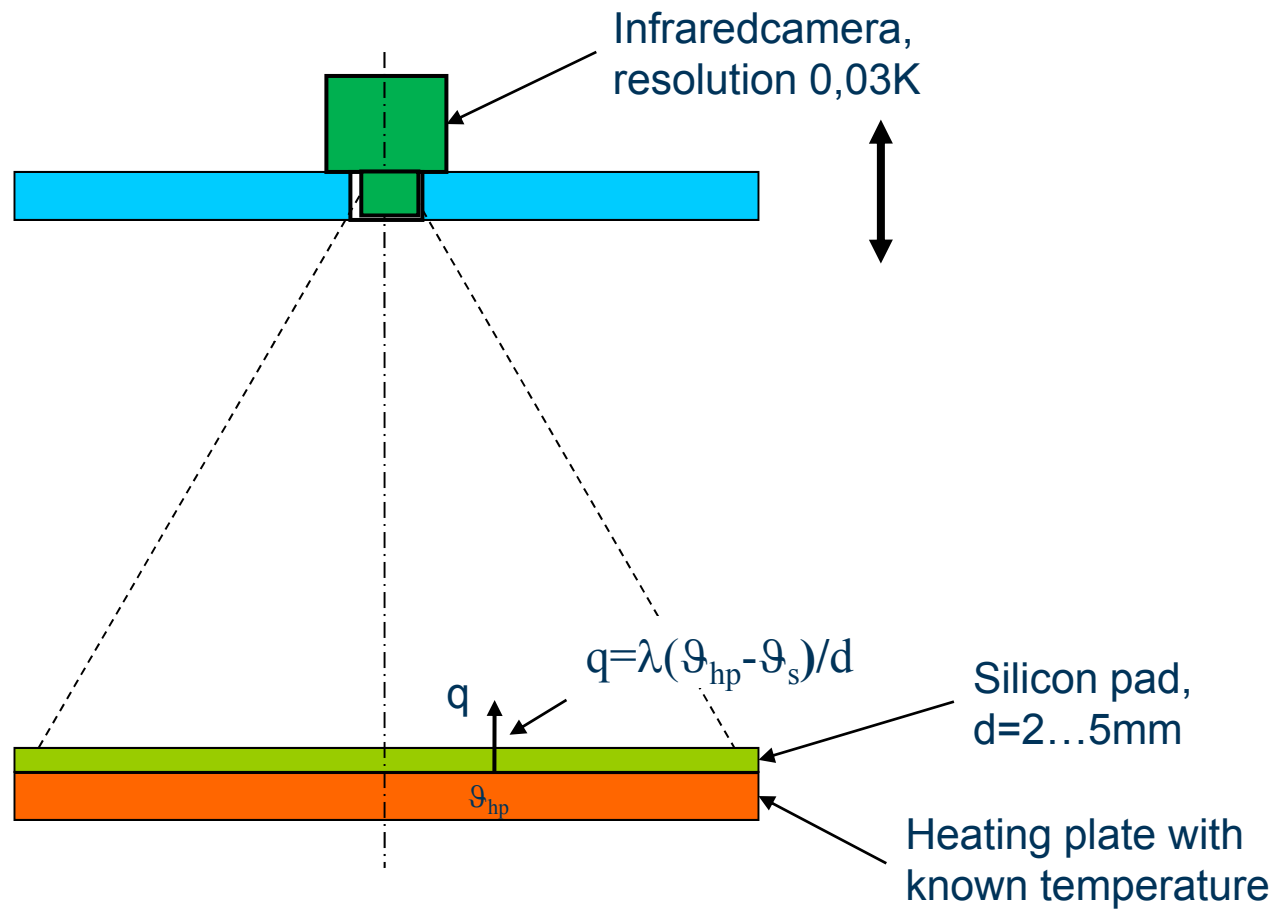


*du Puits et al., NJP 12 (2010)*

To study the effect of  $Ra$  and  $\Gamma$  on the distribution of the local wall heat flux



## Setup to measure the local wall heat flux distribution



**Some ideas to measure (more ideas are very welcome):**

## Averaged quantities

- **Distribution of the local heat flux at  $\Gamma=1$  and variable Ra**
- **Distribution of the local heat flux at fixed Ra and variable  $\Gamma$**
- **Global flow structure at variable  $\Gamma$  analyzing its footprint at the plate**
- **Critical aspect ratios for transitions between different flow modes**

## Instantaneous quantities

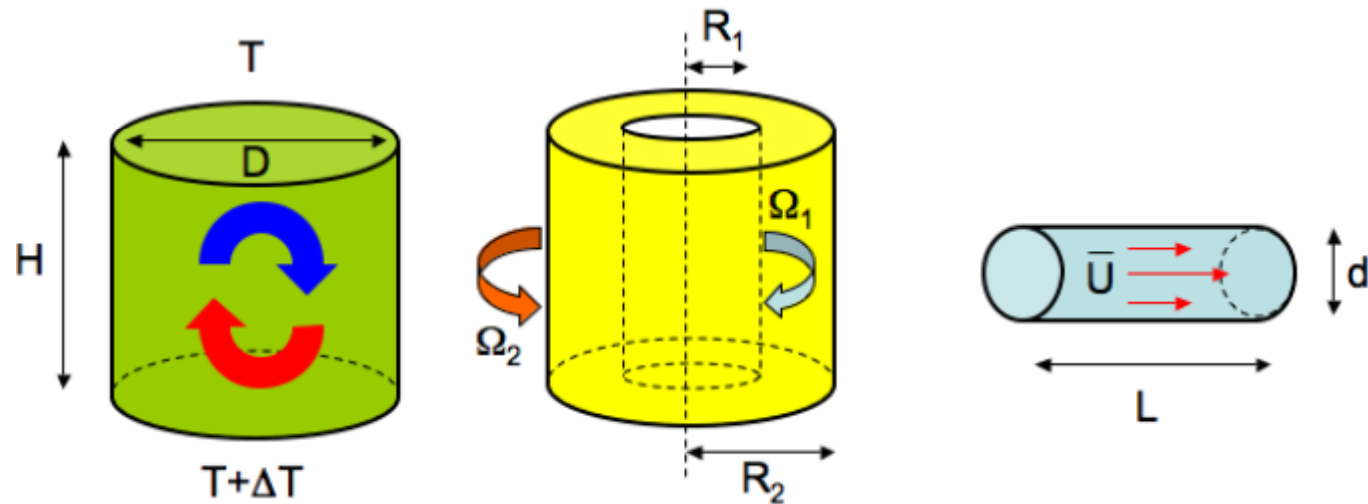
- **Evolution of the mean flow orientation**
- **Probability of different flow modes at transitional aspect ratios**

„Near wall transport and structures in turbulent RB-, TC- and pipe flow“

$$Ra = \frac{g\alpha\Delta TH^3}{\nu\kappa}$$

$$Re_{1,2} = \frac{\Omega_{1,2}R_{1,2}d}{\nu}$$

$$Re = \frac{\bar{U}d}{\nu}$$



Following the ideas of Eckhardt, Grossmann and Lohse [EPL 78 (2007)] the analogy in the turbulent transport between different systems will be studied.

Our part in this project is the experimental study of the RB system and we will focus on the the flow field inside the boundary layers.

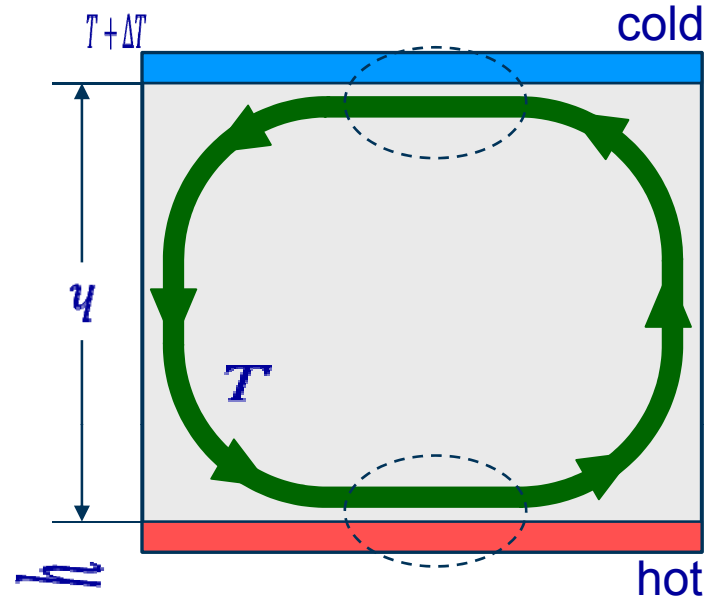
## Parameter range

- $Ra=10^9 \dots 10^{12}$
- $\Gamma=1 \dots 10$
- Various locations at the heating and the cooling plate

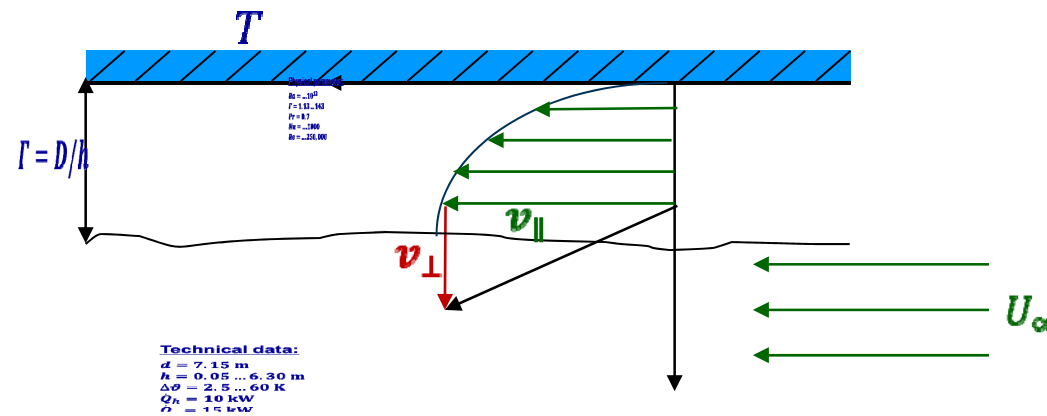
## Measurement tasks

- Temperature profiles
- 3d velocity profiles (all three velocity components)
- Simultaneous temperature and velocity measurements
- PIV, PTV measurements (which is hard since the orientation of the flow permanently varies)

## 3. Viscous boundary layer measurements



- Finite lateral extent of the cell
- creates a mean flow
- Boundary layers develop
- BI's determine the heat transport





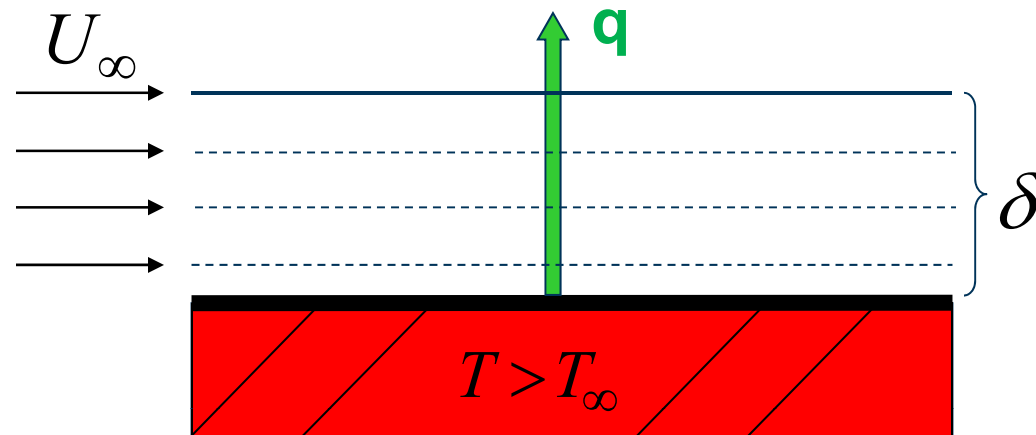
## „What is the nature of the heat transport throughout the boundary layers?“

$$q = -\lambda \frac{\partial T}{\partial z} + \rho c_p \langle w' T' \rangle$$

Diffusion

Advection

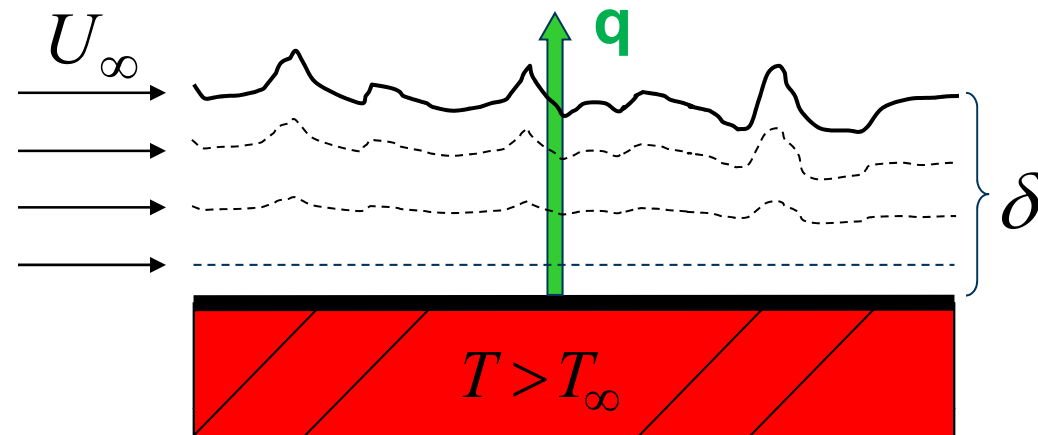
## Scenario 1: Laminar boundary layer (acc. Prandtl/Blasius)



- Stationary, two-dimensional flow, small fluctuations might be allowed
- Wall-normal velocity component small compared with that parallel to the wall
- Basically parallel stream lines (as shown in the sketch)
- Diffusive heat transport according Fourier's law

$$q = -\lambda \frac{\partial T}{\partial z} \quad \longrightarrow \quad T \sim -z$$

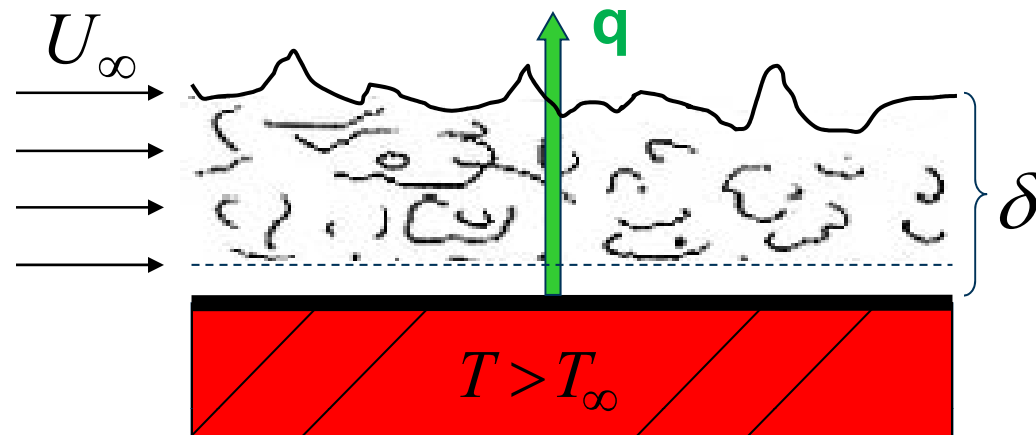
## Scenario 2: Laminar boundary layer with fluctuations



- **Fluctuating but still two-dimensional flow,  $u', v', w' < U_\infty$**
- **Basically parallel stream lines (as shown in the sketch)**
- **Diffusive + advective heat transport**

$$q = -\lambda \frac{\partial \bar{T}}{\partial z} + \rho c_p \langle w' T' \rangle \quad \text{with} \quad \left| -\lambda \frac{\partial \bar{T}}{\partial z} \right| \geq |\rho c_p \langle w' T' \rangle|$$

### Scenario 3: Fully turbulent boundary layer



- Fully turbulent boundary layer,  $u', v', w' \approx U_\infty$
- Only a thin viscous sublayer survives
- Mainly advective heat transport

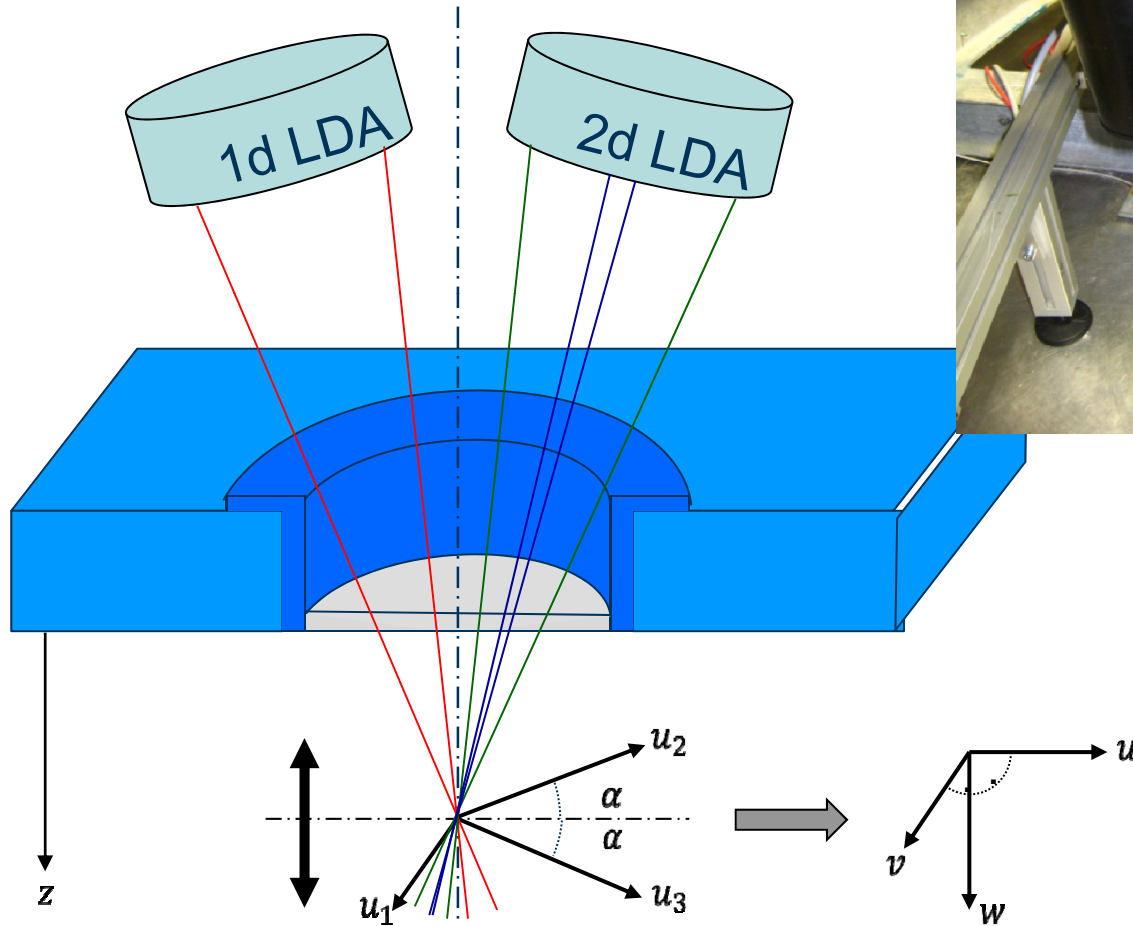
$$q = -\lambda \frac{\partial T}{\partial z} + \rho c_p \langle w' T' \rangle \quad \text{with} \quad \left| -\lambda \frac{\partial T}{\partial z} \right| \ll |\rho c_p \langle w' T' \rangle|$$

## Measurement setup

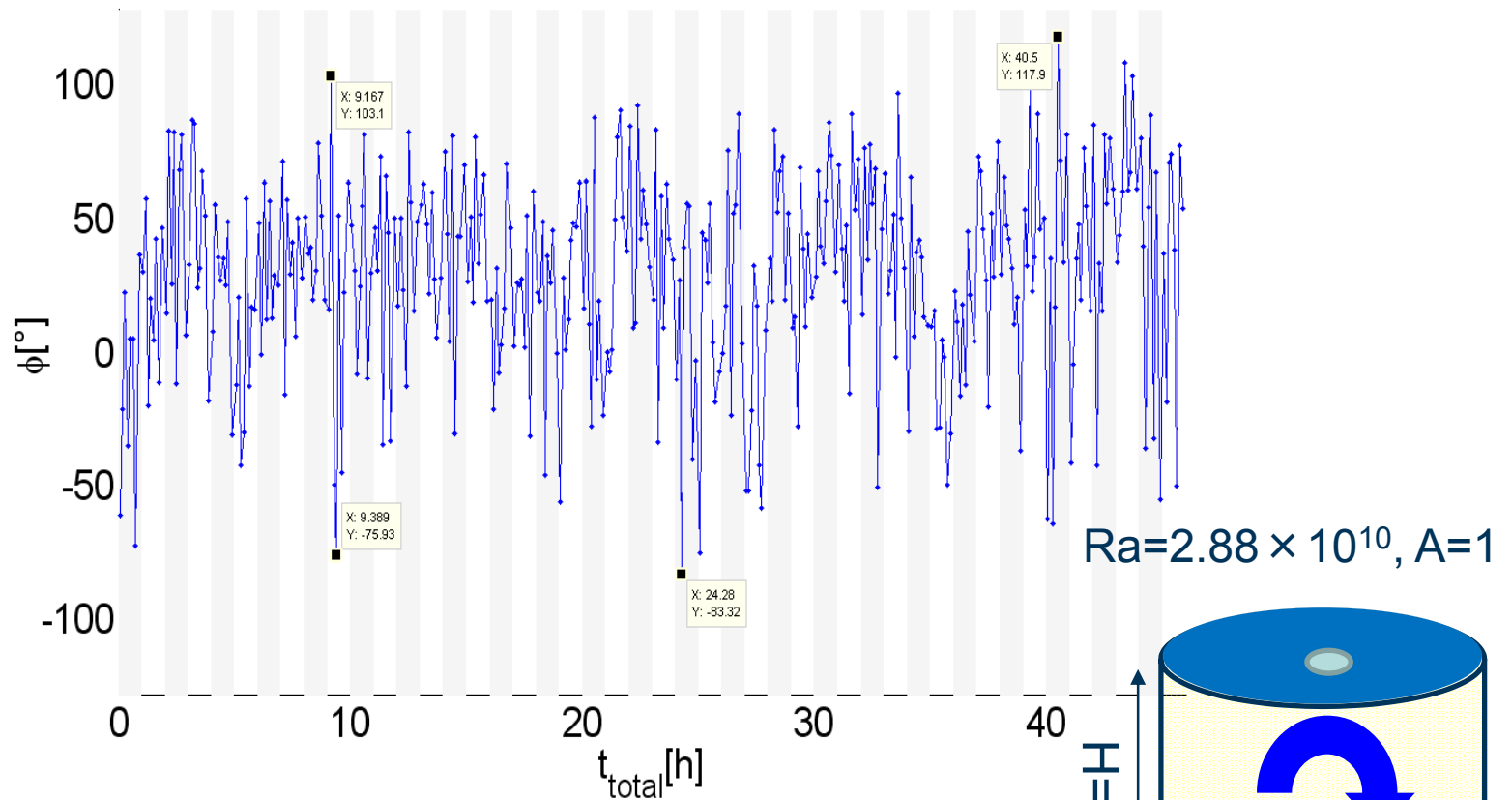
Technical news

Present projects

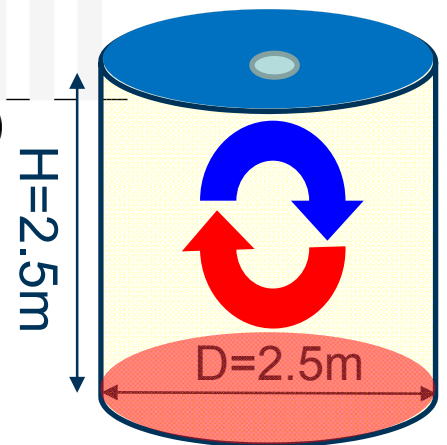
Measurements



## Orientation of the large-scale circulation



- Plot the instantaneous angle of the LSC
- Oscillations by  $\pm 90^\circ$  around the mean angle



## Mean horizontal velocity profile

$$Ra = 3.4 \times 10^9$$

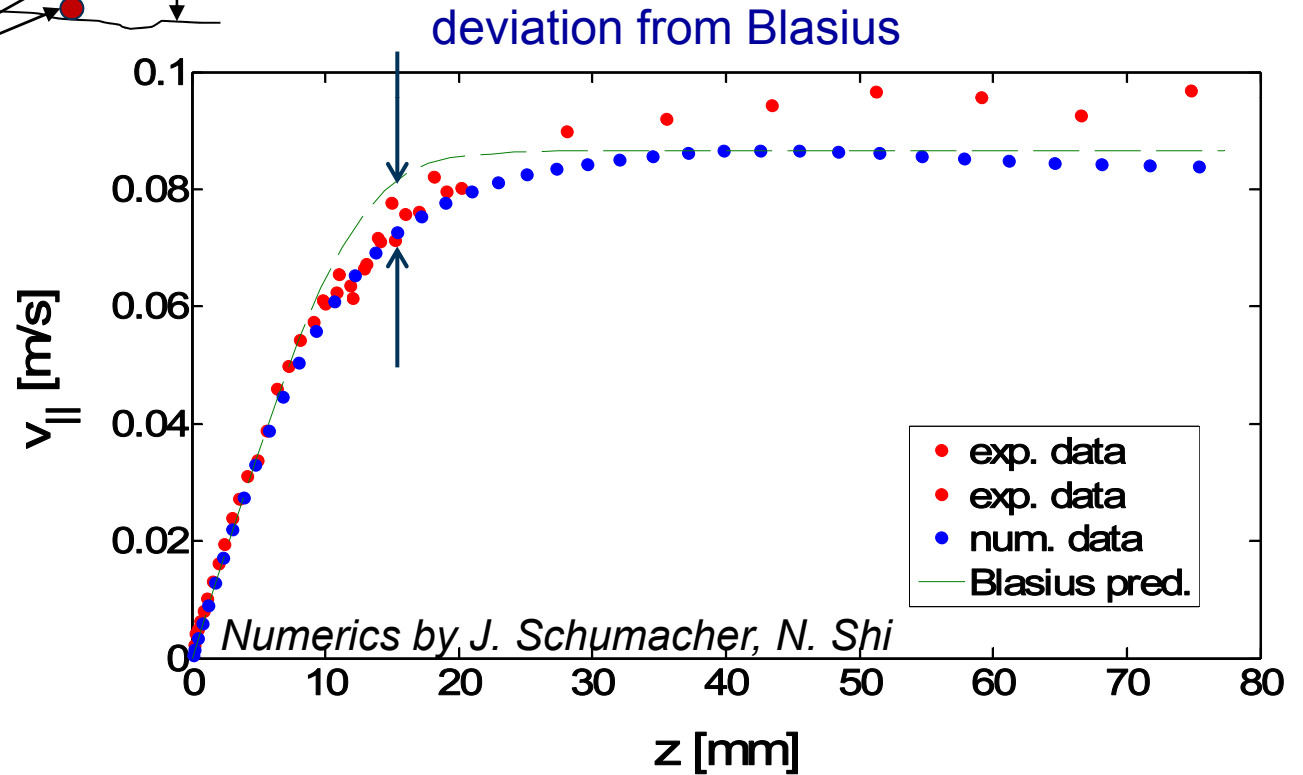
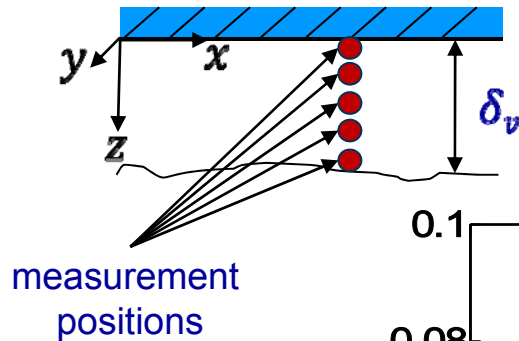
$$\Gamma = 1, Pr = 0.7$$

$$v_{\parallel} = \sqrt{u^2 + v^2}$$

$$w$$

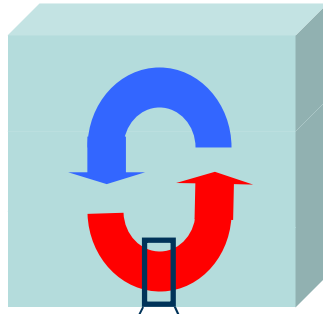
- wall-parallel velocity

- wall-normal velocity



## Dynamic space transformation of the profiles

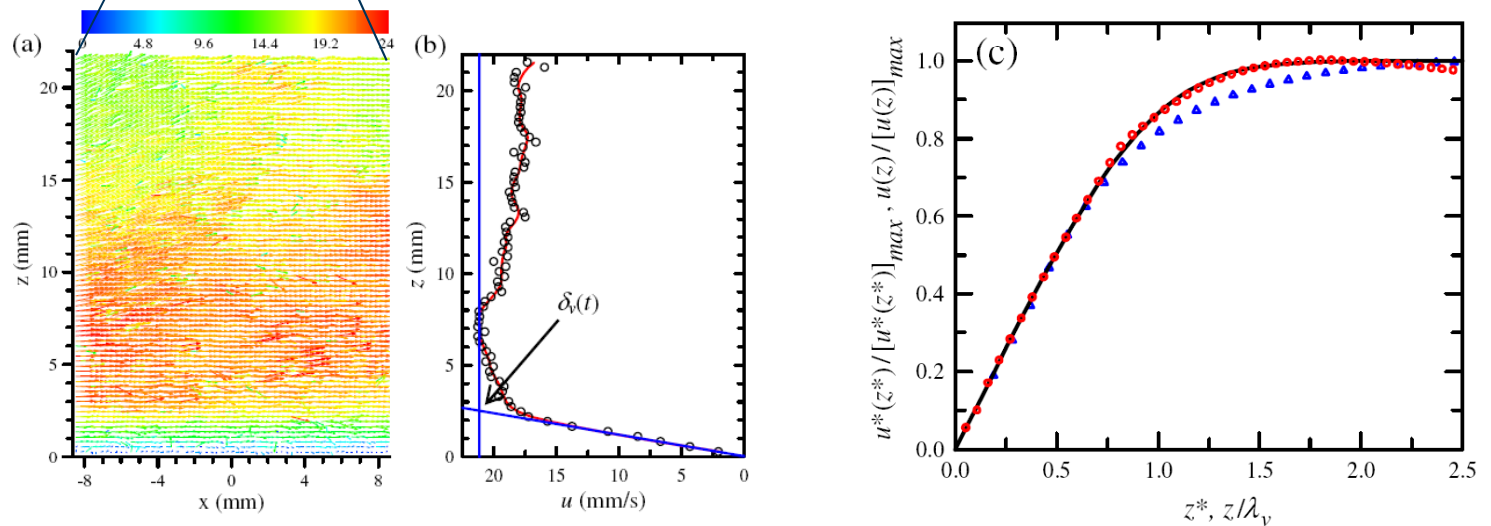
Zhou and Xia, PRL 104 (2010)



1. Instantaneous velocity field
2. Instantaneous thickness  $\delta_v(t)$  of the bl
3. Rescaling of  $z$  with respect to  $\delta_v(t)$



The transformed profile  $u^*(z^*)$  perfectly fits the Blasius prediction



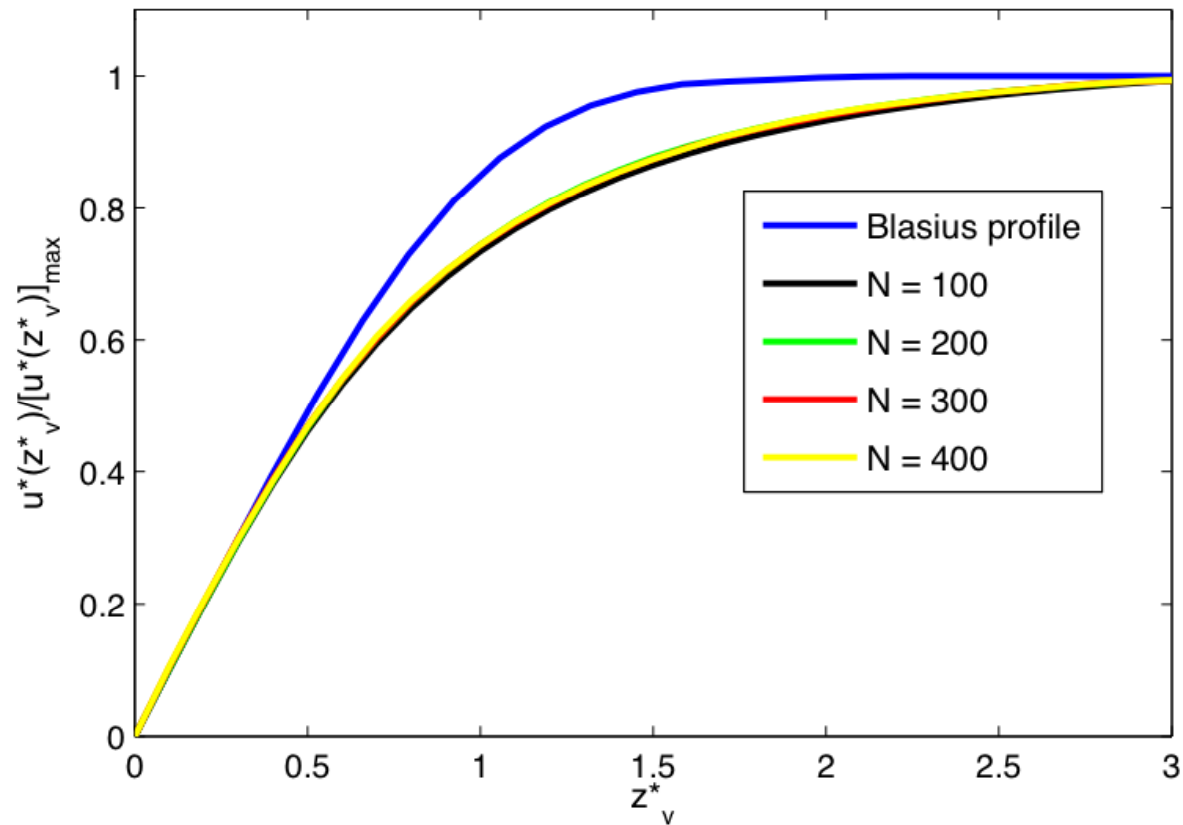


## Dynamic space transformation of the profiles

*Shi, Emran and Schumacher, APS meeting (2010)*

$$Ra = 3 \times 10^9$$

$$\Gamma = 1, Pr = 0.7$$



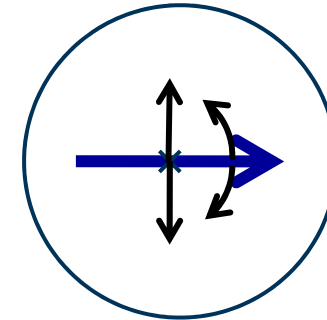
There are two fundamental differences:

## Rectangular cell

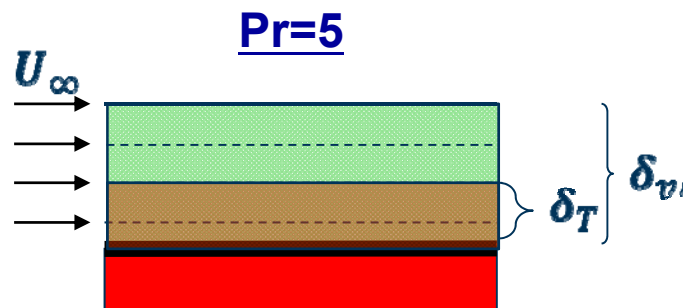


- Fixed orientation of the LSC

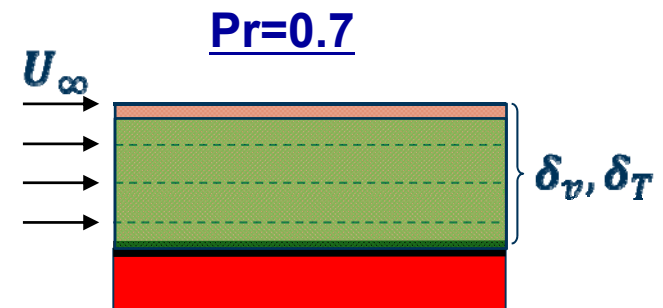
## Cylindrical cell



- One more degree of freedom for the LSC
- More dynamics!



- $\delta_T < \delta_v$



- $\delta_v$  and  $\delta_T$  are of the same order

## Mean velocity profiles

$$Ra = 2.9 \times 10^{10}$$

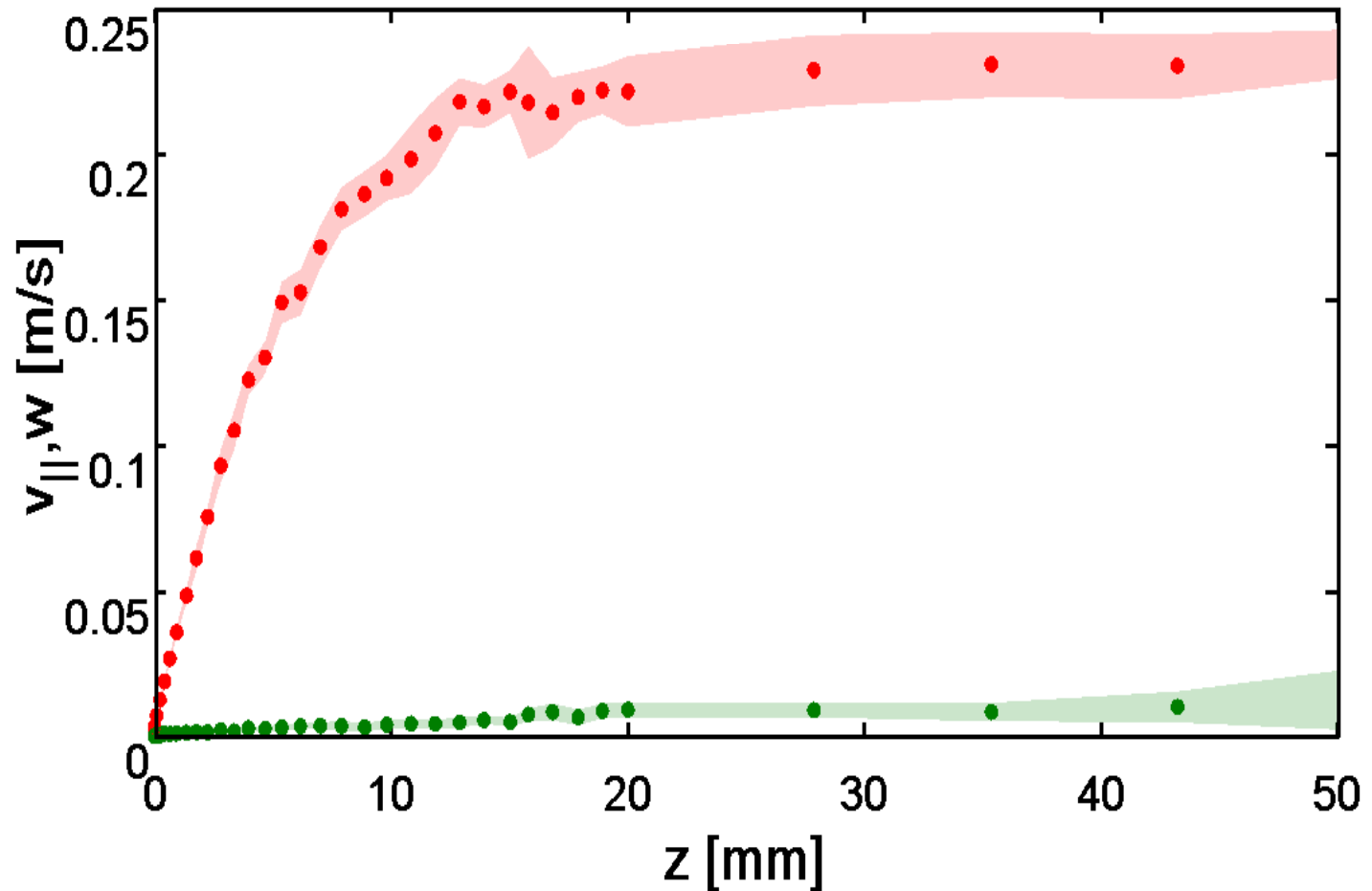
$$\Gamma = 1, Pr = 0.7$$

$$v_{\parallel} = \sqrt{u^2 + v^2}$$

$$w$$

- wall-parallel velocity

- wall-normal velocity



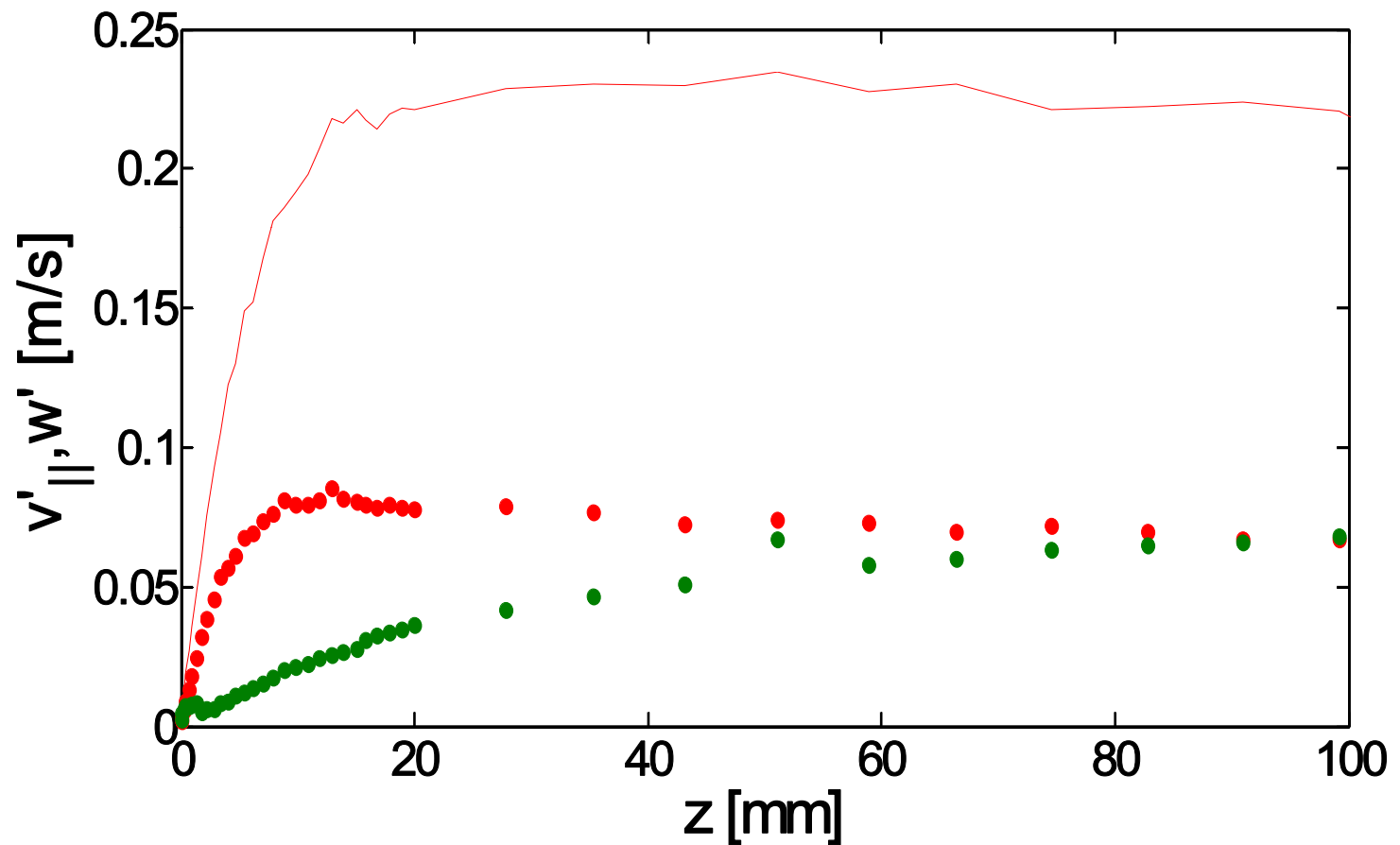
## Fluctuations

$$Ra = 2.9 \times 10^{10}$$

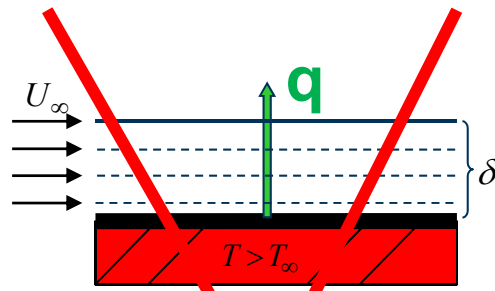
$$\Gamma = 1, Pr = 0.7$$

$v'_{\parallel}$  - standard deviation of  $v_{\parallel}$

$w'$  - standard deviation of  $w$

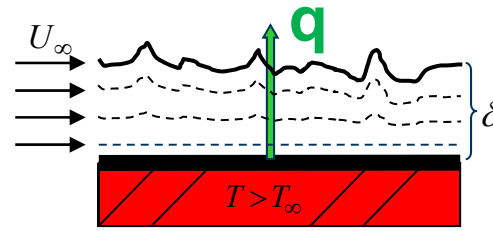


Which of the models for the boundary layer is the right one?



~~laminar bl~~

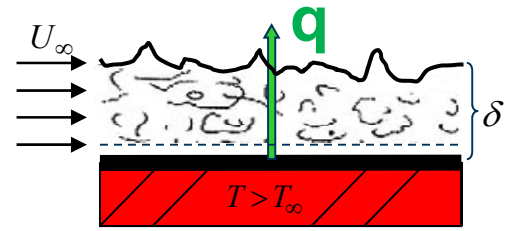
~~$$q = -\lambda \frac{\partial T}{\partial z}$$~~



laminar bl with  
fluctuations

$$q = -\lambda \frac{\partial T}{\partial z} + \rho c_p \langle w' T' \rangle$$

$$\left| -\lambda \frac{\partial T}{\partial z} \right| \geq \left| \rho c_p \langle w' T' \rangle \right|$$



turbulent bl

$$\left| -\lambda \frac{\partial T}{\partial z} \right| \ll \left| \rho c_p \langle w' T' \rangle \right|$$

Have we already reached the ultimate state?

BOI

THANK YOU!